

STRUCTURAL OPTIMIZATION: FROM CONTINUUM AND GROUND STRUCTURES TO ADDITIVE MANUFACTURING

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LCCV – UFAL
2014

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ZEGARD T, PAULINO GH (2013). "TRUSS LAYOUT OPTIMIZATION WITHIN A CONTINUUM." STRUCTURAL AND MULTIDISCIPLINARY OPTIMIZATION, 48(1):1-16.

3. LATERAL BRACING SYSTEMS

ZEGARD T, BAKER WF, MAZUREK A, PAULINO GH (2014). "GEOMETRICAL ASPECTS OF LATERAL BRACING SYSTEMS: WHERE SHOULD THE OPTIMAL BRACING POINT BE?" JOURNAL OF STRUCTURAL ENGINEERING, 140(8):04014063

4. 2D GROUND STRUCTURES

ZEGARD T, PAULINO GH (2014). "GRAND – GROUND STRUCTURE BASED TOPOLOGY OPTIMIZATION ON ARBITRARY 2D DOMAINS USING MATLAB." STRUCTURAL AND MULTIDISCIPLINARY OPTIMIZATION, JUNE.

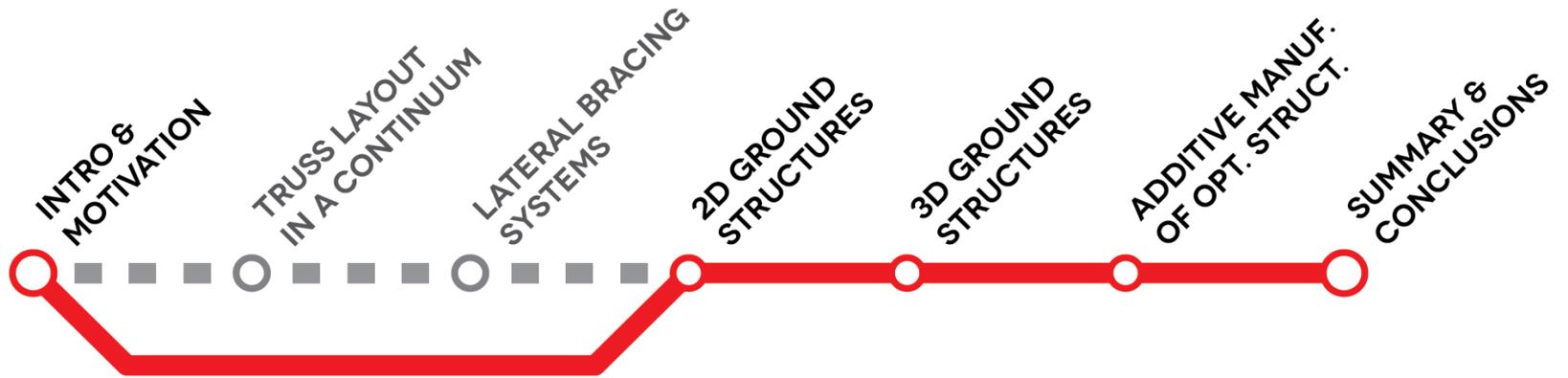
5. 3D GROUND STRUCTURES

ZEGARD T, PAULINO GH (XXXX). "GRAND3 – GROUND STRUCTURE BASED TOPOLOGY OPTIMIZATION ON ARBITRARY 3D DOMAINS USING MATLAB." STRUCTURAL AND MULTIDISCIPLINARY OPTIMIZATION, IN PREPARATION.

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7. SUMMARY & CONCLUSIONS

ROADMAP



ROADMAP

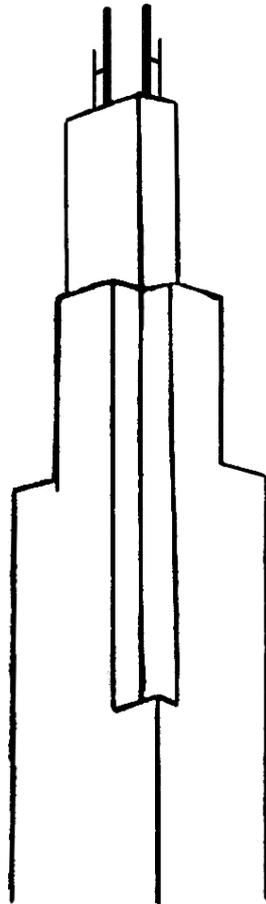


1) INTRO & MOTIVATION

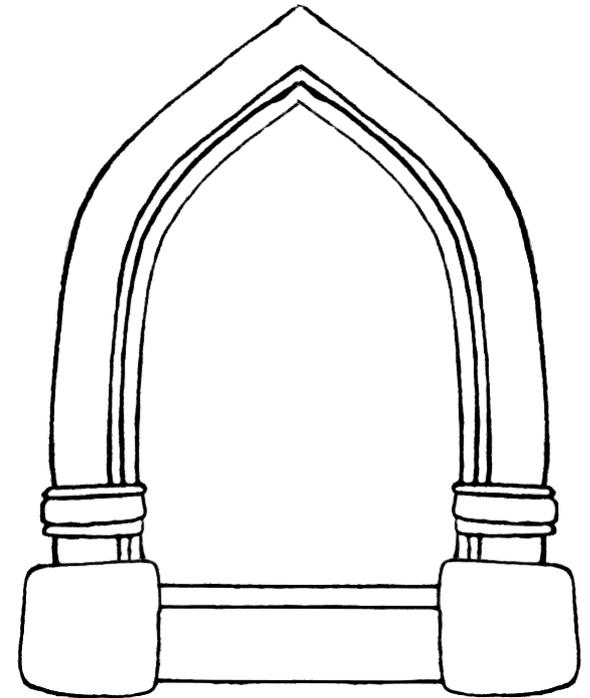
- WHY USE STRUCTURAL OPTIMIZATION?



LIMITED
RESOURCES



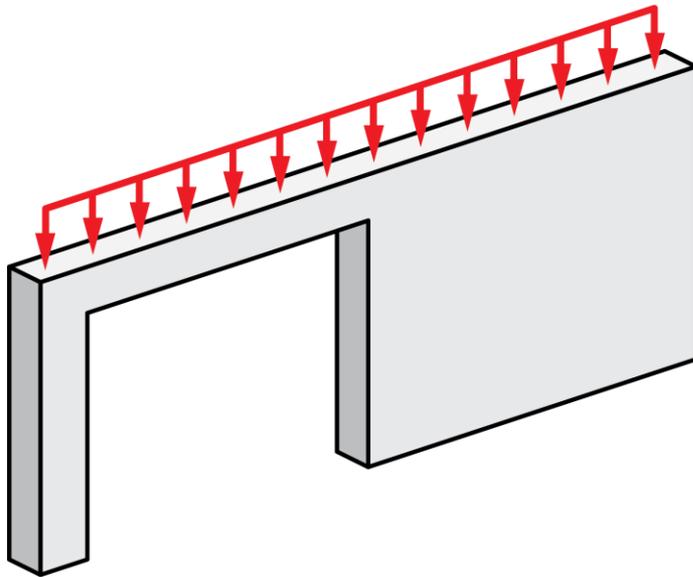
EXTREME STRUCTURES



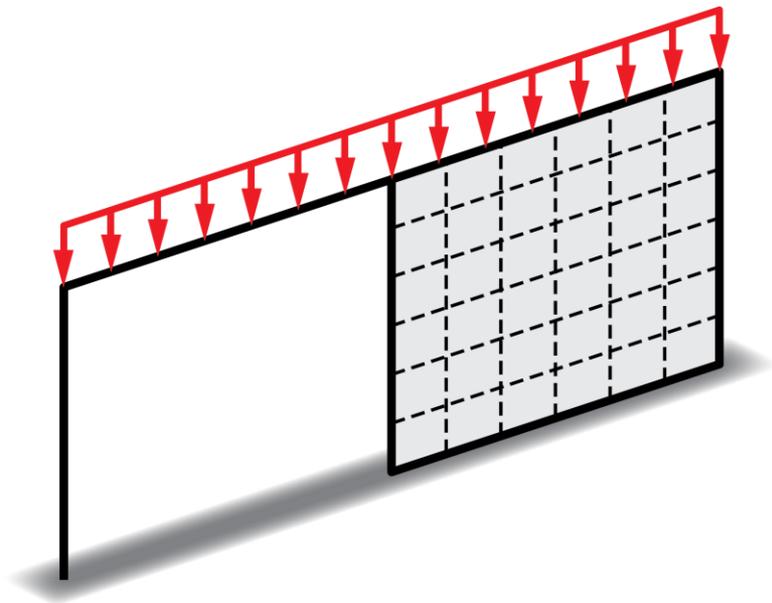
FUNCTIONAL

1) INTRO & MOTIVATION

- WHY DISCRETE—CONTINUUM?
 - LIMITED MODELING CAPABILITY
 - REASONABLE SIMPLIFICATIONS OF REALITY



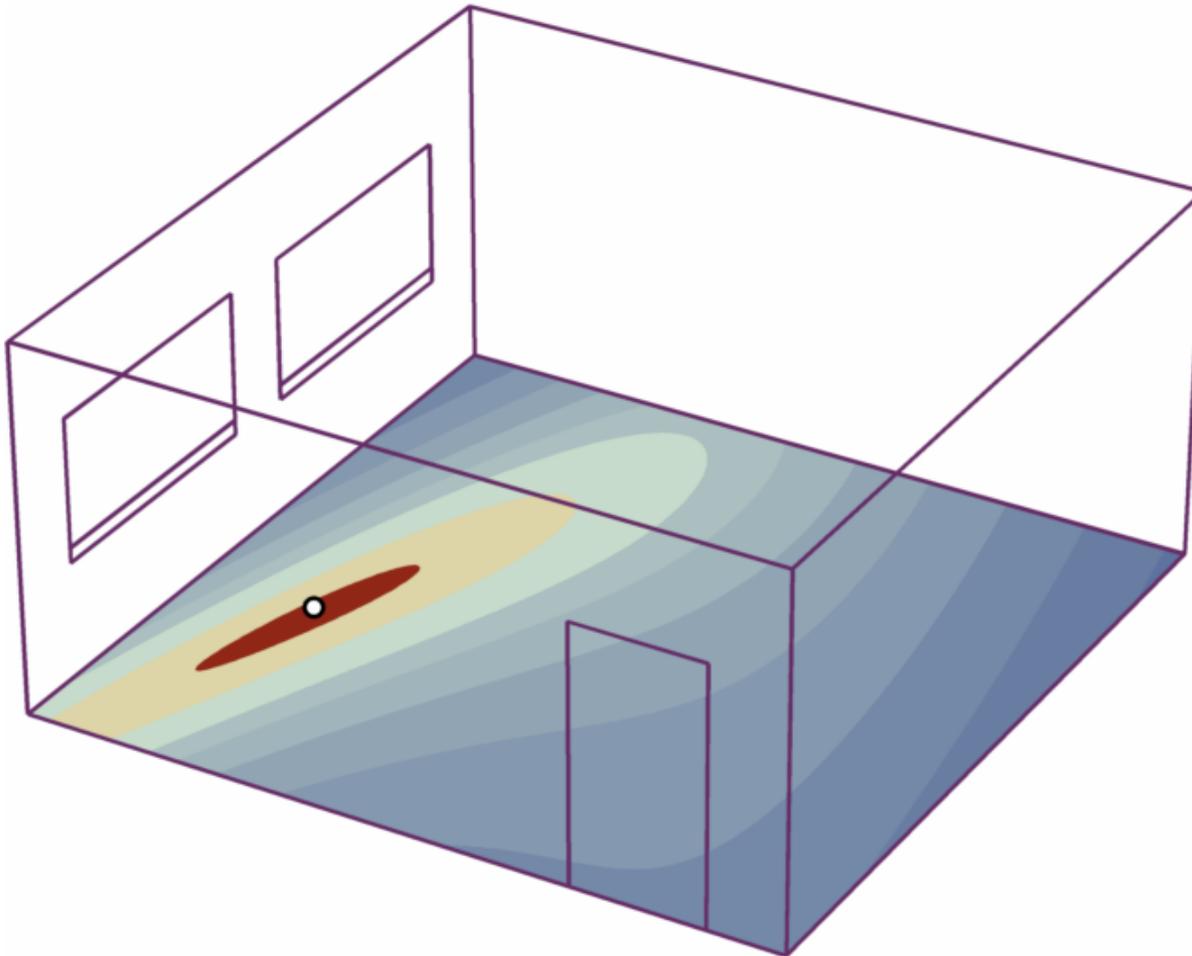
REAL FRAME



SIMPLIFIED FRAME MODEL

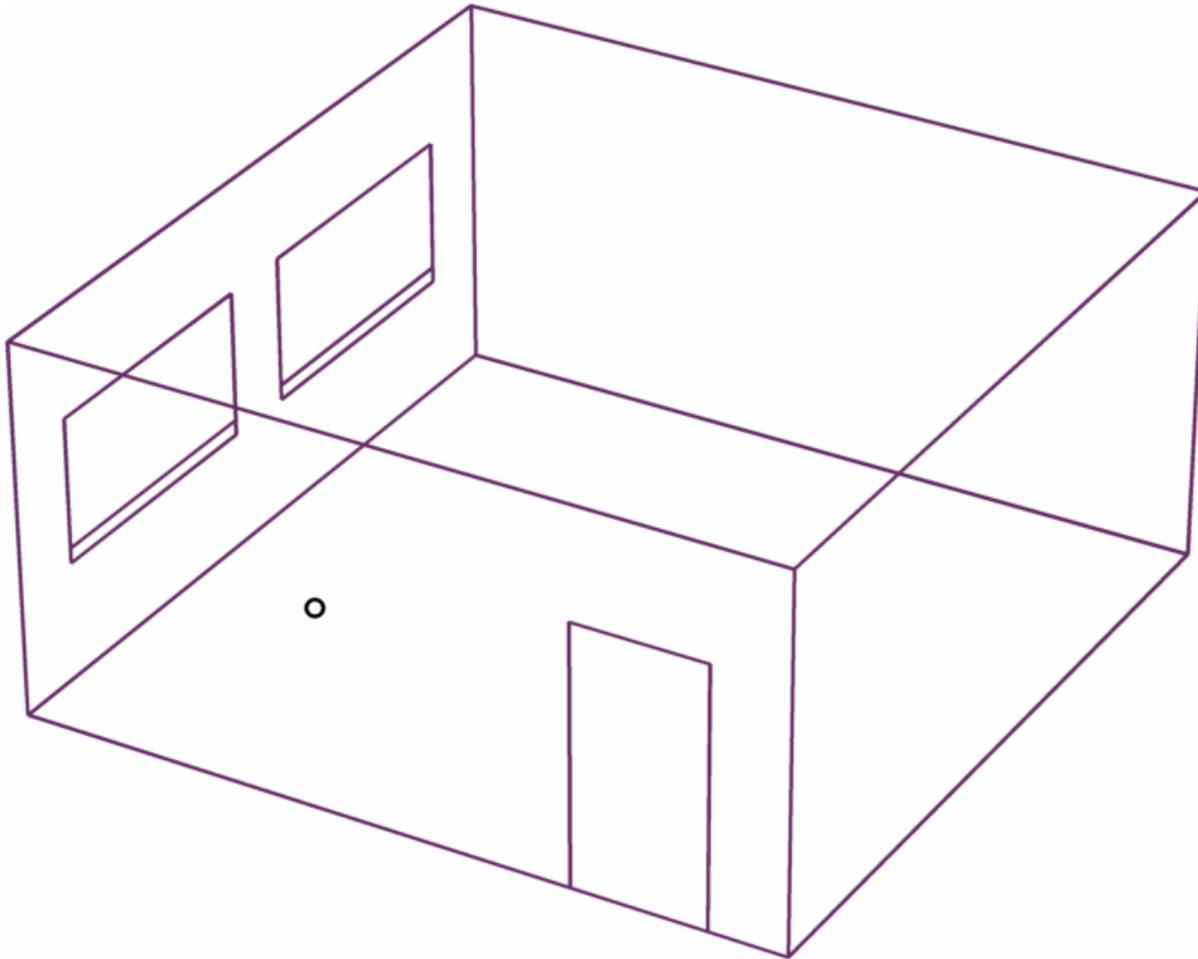
1) INTRO & MOTIVATION

- GRADIENT VS. NON-GRADIENT



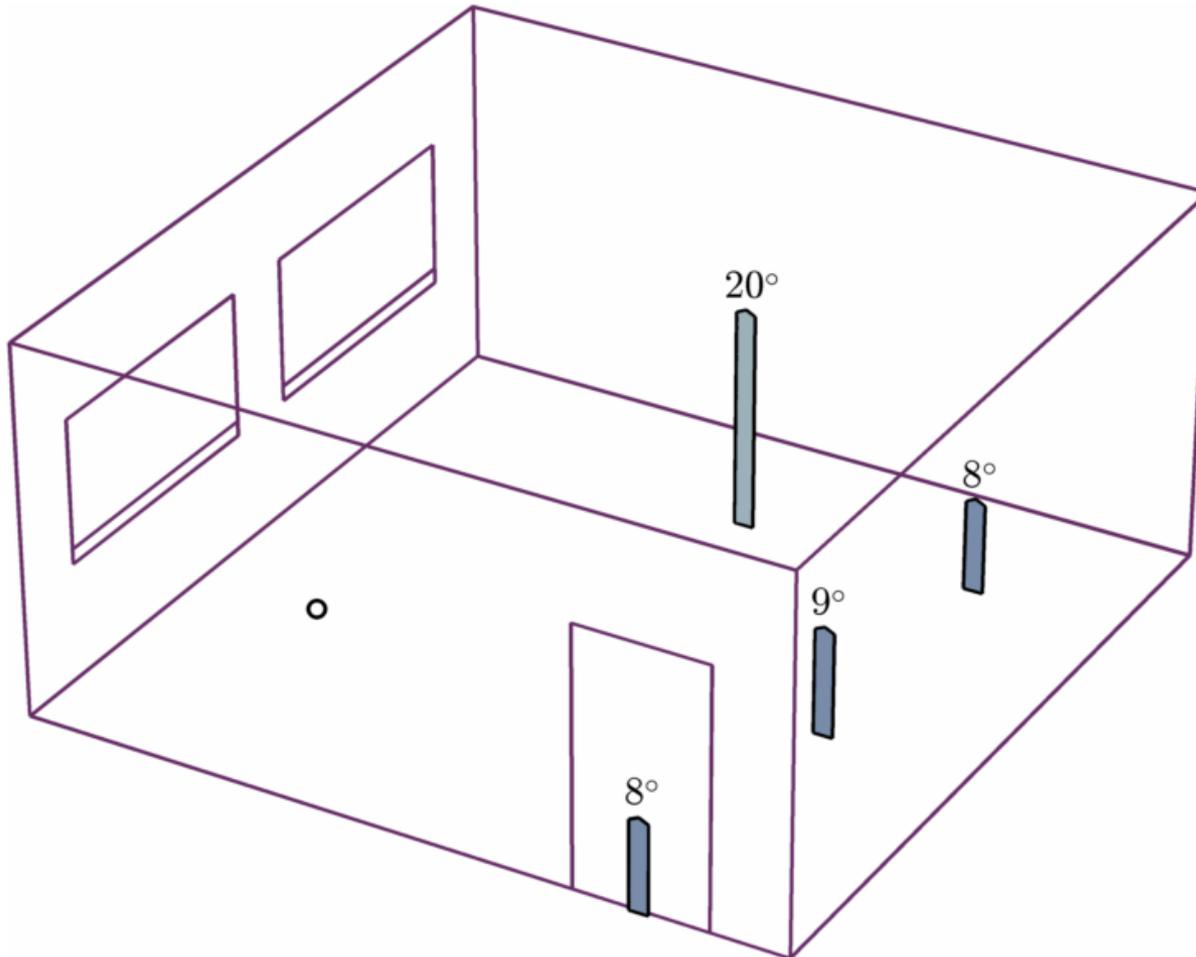
1) INTRO & MOTIVATION

- GRADIENT VS. NON-GRADIENT



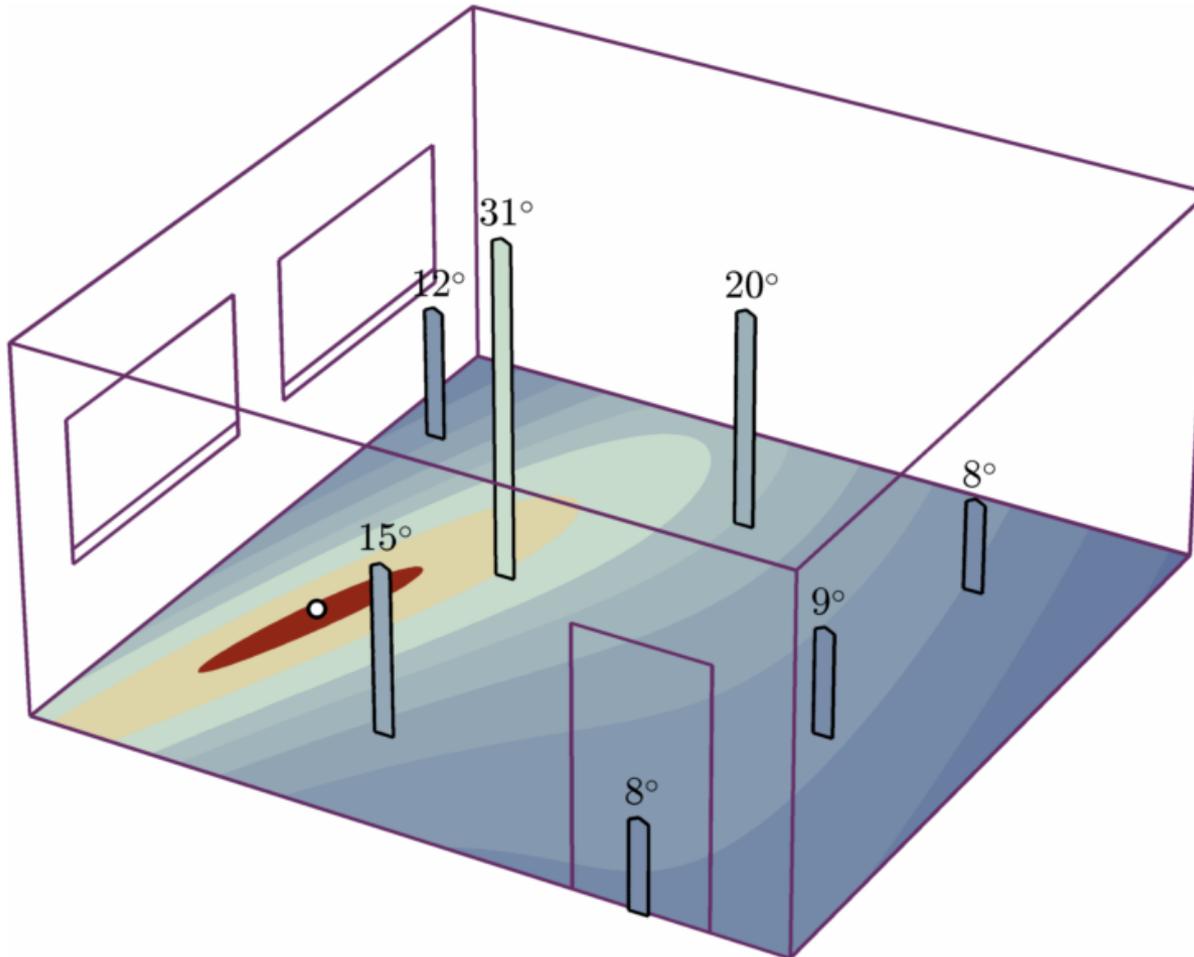
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- GRADIENT VS. NON-GRADIENT



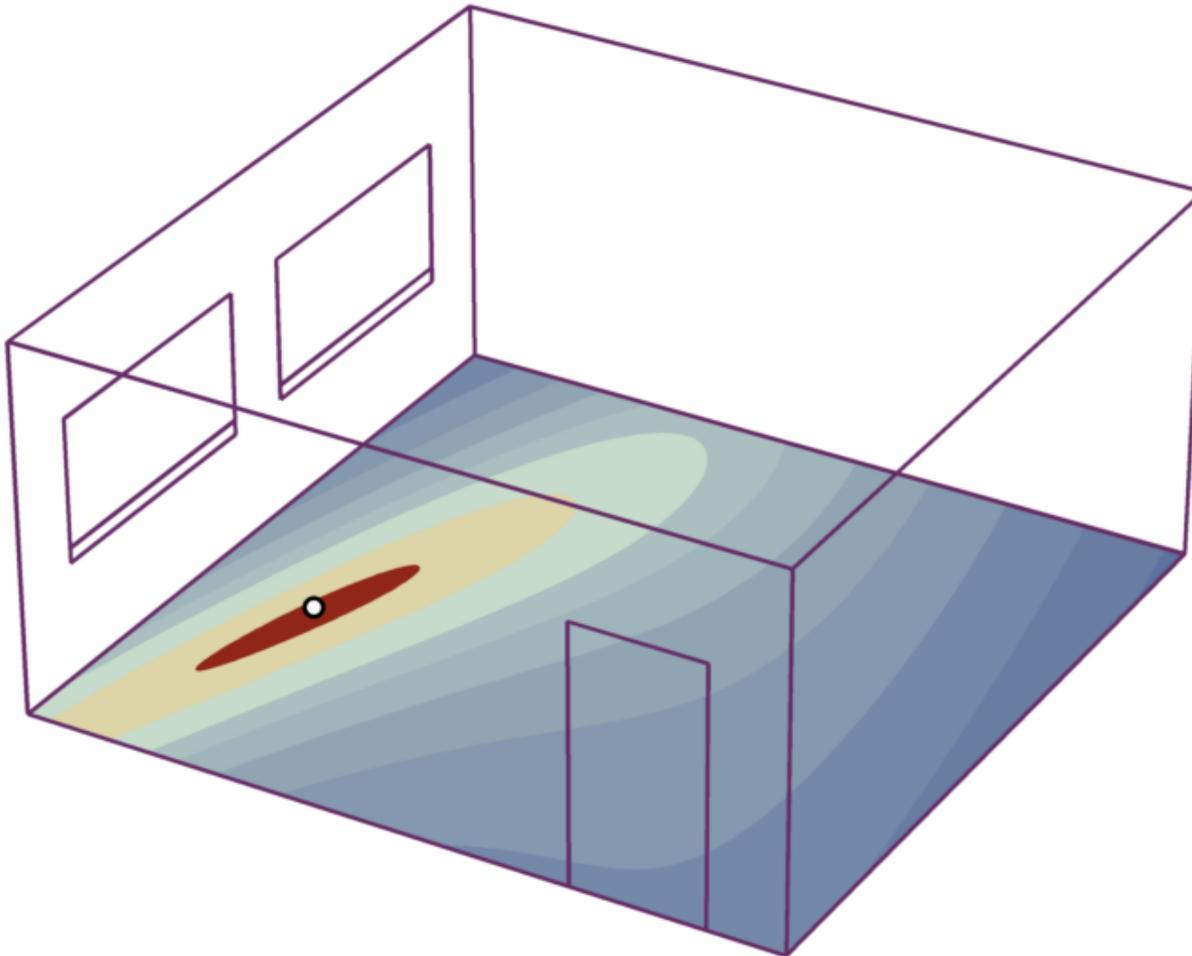
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- GRADIENT VS. NON-GRADIENT



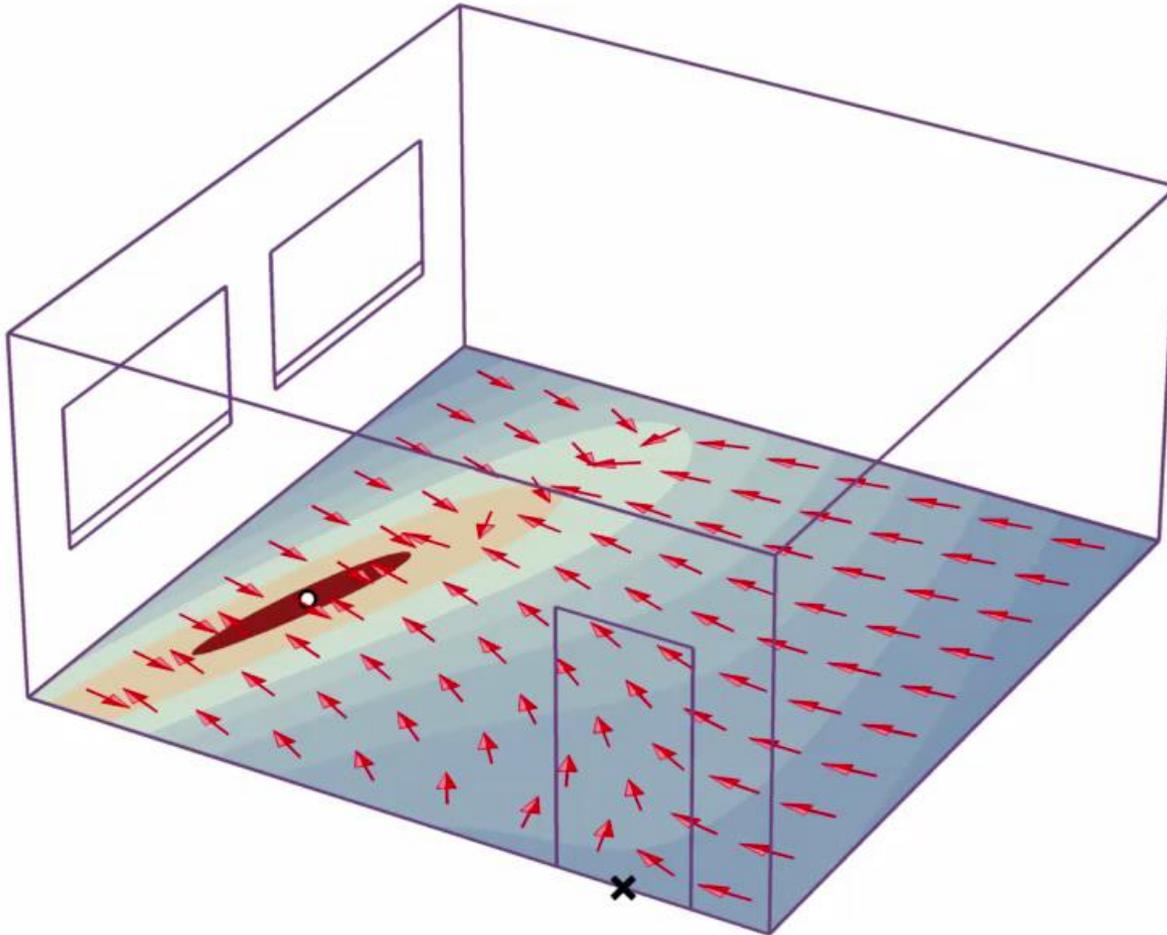
1) INTRO & MOTIVATION

- GRADIENT VS. NON-GRADIENT



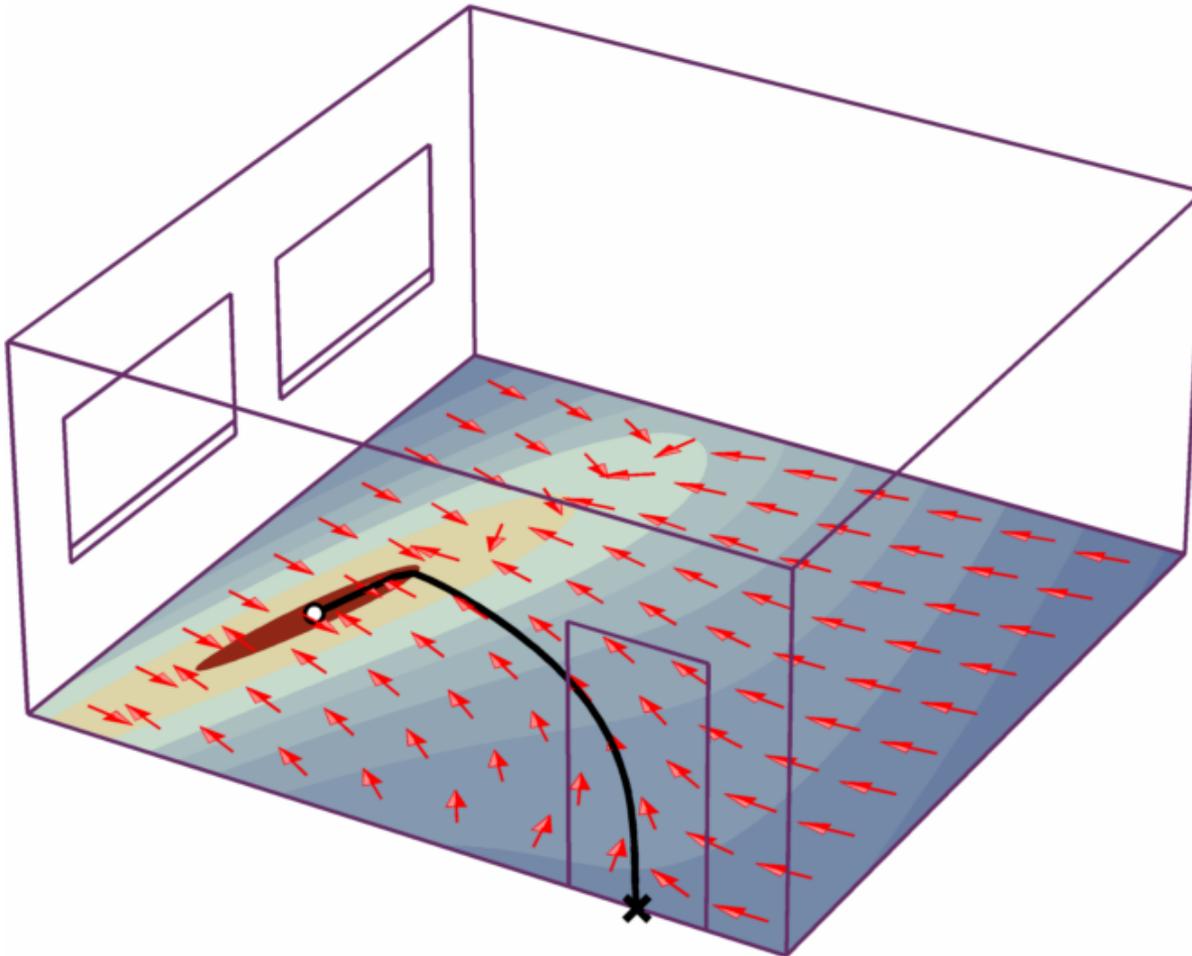
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- GRADIENT VS. NON-GRADIENT



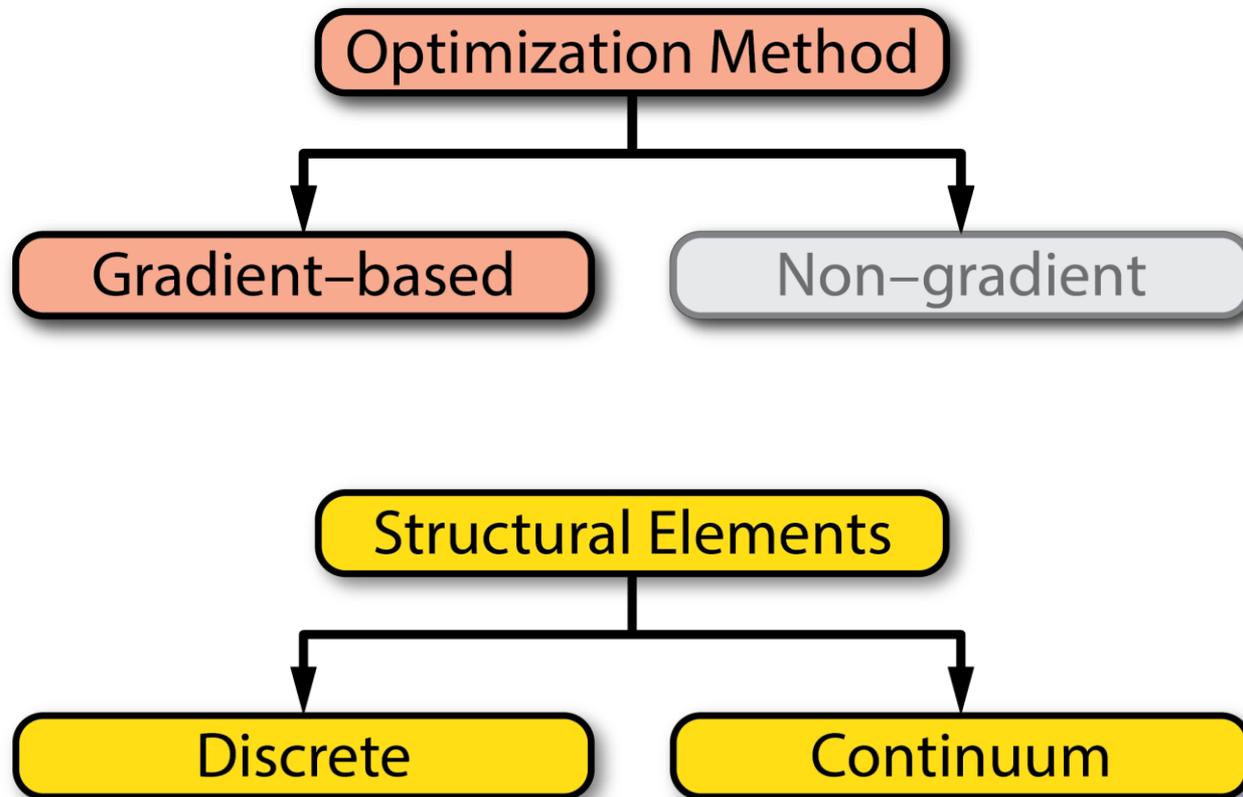
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- GRADIENT VS. NON-GRADIENT



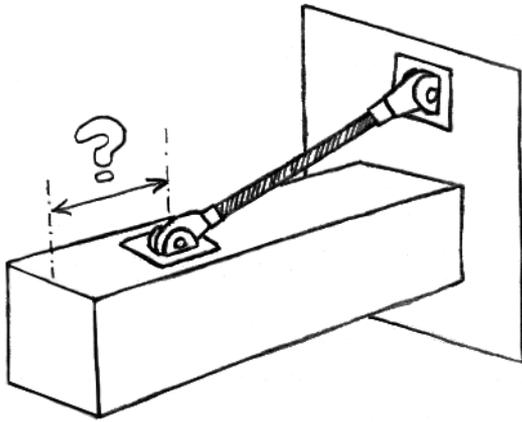
1) INTRO & MOTIVATION

- STRUCTURAL OPTIMIZATION METHODS

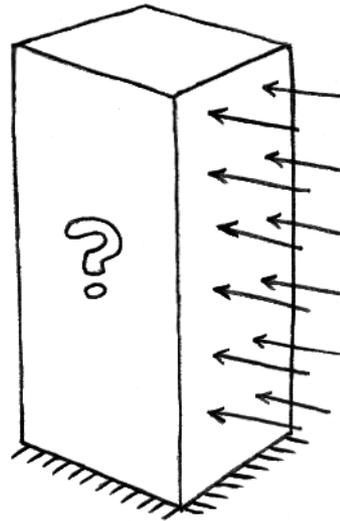


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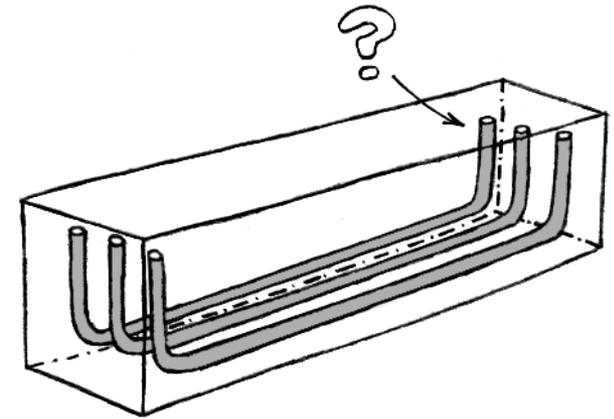
- POTENTIAL APPLICATIONS



ANCHOR POINT
LOCATION



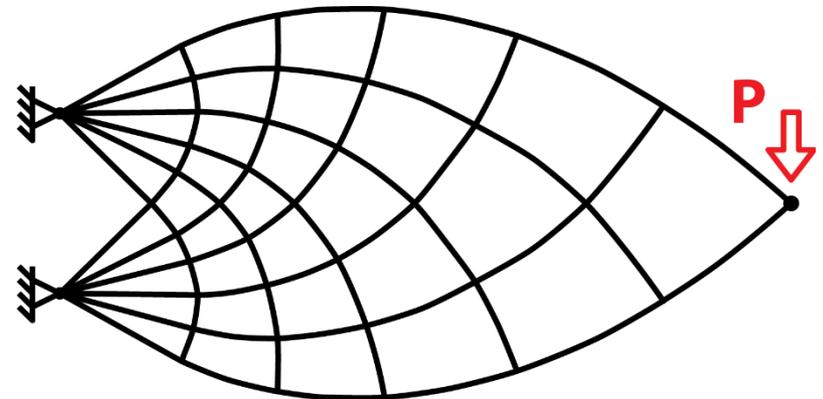
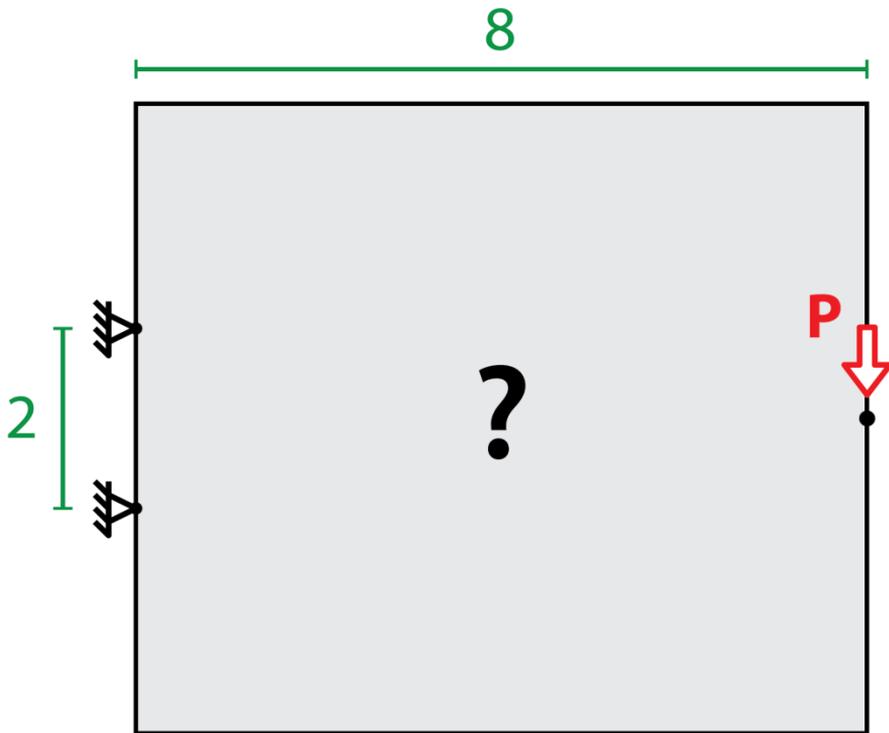
LATERAL BRACING
SYSTEM



REINFORCEMENT
LAYOUT

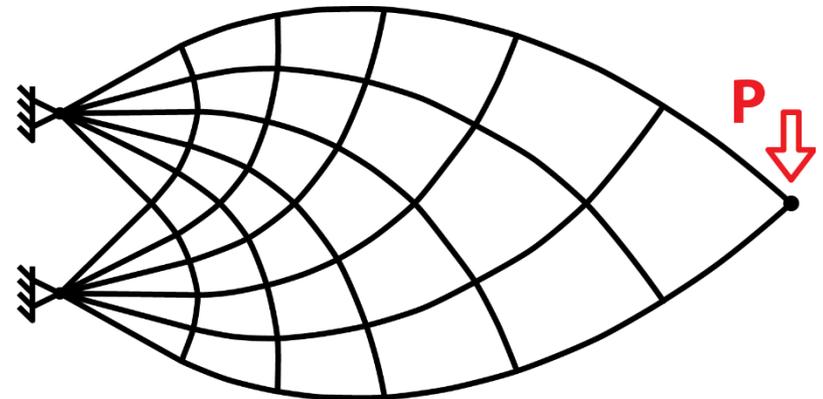
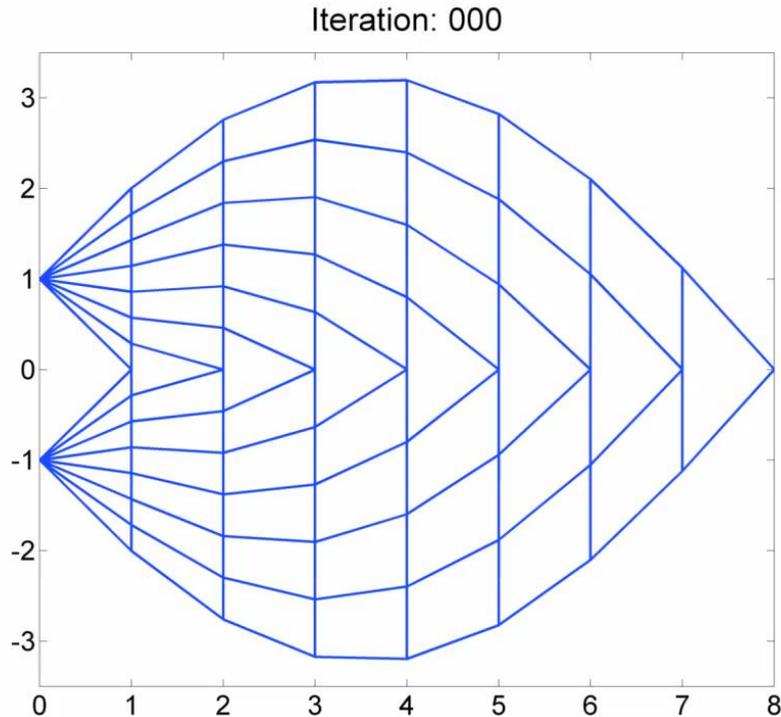
4) GROUND STRUCTURES IN 2D

- TRUSS LAYOUT OPTIMIZATION IS HIGHLY NONLINEAR: GEOMETRY AND SIZING



4) GROUND STRUCTURES IN 2D

- TRUSS LAYOUT OPTIMIZATION IS HIGHLY NONLINEAR: GEOMETRY AND SIZING



4) GROUND STRUCTURES IN 2D

- MAIN IDEA:
CONVERT A GEOMETRY AND SIZE OPTIMIZATION TO A SIZING-ONLY PROBLEM

- PLASTIC FORMULATION:

$$\begin{aligned} \min_{\mathbf{a}} \quad & V = \mathbf{l}^T \mathbf{a} \\ \text{s.t.} \quad & \mathbf{B}^T \mathbf{n} = \mathbf{f} \\ & -\sigma_C \leq \sigma_i \leq \sigma_T \quad \text{if } a_i > 0 \\ & a_i \geq 0 \quad i = 1, 2, \dots, N_b \end{aligned}$$

4) GROUND STRUCTURES IN 2D

$$\begin{array}{ll} \min_{\mathbf{a}} & V = \mathbf{l}^T \mathbf{a} \\ \text{s.t.} & \mathbf{B}^T \mathbf{n} = \mathbf{f} \\ & -\sigma_C \leq \sigma_i \leq \sigma_T \quad \text{if } a_i > 0 \\ & a_i \geq 0 \quad i = 1, 2, \dots, N_b \end{array} \quad \left. \vphantom{\begin{array}{l} \\ \\ \\ \end{array}} \right\} \text{VANISHING CONSTRAINT}$$

- MULTIPLYING THE INEQUALITY BY CROSS-SECTIONAL AREA

$$\begin{array}{ll} \min_{\mathbf{a}} & V = \mathbf{l}^T \mathbf{a} \\ \text{s.t.} & \mathbf{B}^T \mathbf{n} = \mathbf{f} \\ & -\sigma_C a_i \leq n_i \leq \sigma_T a_i \end{array}$$

4) GROUND STRUCTURES IN 2D

$$\begin{aligned} \min_{\mathbf{a}} \quad & V = \mathbf{l}^T \mathbf{a} \\ \text{s.t.} \quad & \mathbf{B}^T \mathbf{n} = \mathbf{f} \\ & -\sigma_C a_i \leq n_i \leq \sigma_T a_i \end{aligned}$$

- INTRODUCING SLACK VARIABLES

$$\left. \begin{aligned} n_i + 2 \frac{\sigma_0}{\sigma_C} s_i^- &= \sigma_T a_i \\ -n_i + 2 \frac{\sigma_0}{\sigma_T} s_i^+ &= \sigma_C a_i \\ \sigma_0 &= (\sigma_T + \sigma_C) / 2 \end{aligned} \right\}$$

$$\begin{aligned} a_i &= \frac{s_i^+}{\sigma_T} + \frac{s_i^-}{\sigma_C} \\ n_i &= s_i^+ - s_i^- \end{aligned}$$

$$\begin{aligned} \min_{\mathbf{s}^+, \mathbf{s}^-} \quad & V = \mathbf{l}^T \left(\frac{\mathbf{s}^+}{\sigma_T} + \frac{\mathbf{s}^-}{\sigma_C} \right) \\ \text{s.t.} \quad & \mathbf{B}^T (\mathbf{s}^+ - \mathbf{s}^-) = \mathbf{f} \\ & s_i^+, s_i^- \geq 0 \end{aligned}$$

4) GROUND STRUCTURES IN 2D

- REMARKS

- DESIGN VARIABLES DOUBLED: s^+ AND s^-
- NO MORE VANISHING CONSTRAINT
- DIFFERENT LIMITS IN TENSION AND COMPRESSION
- LINEAR PROGRAM

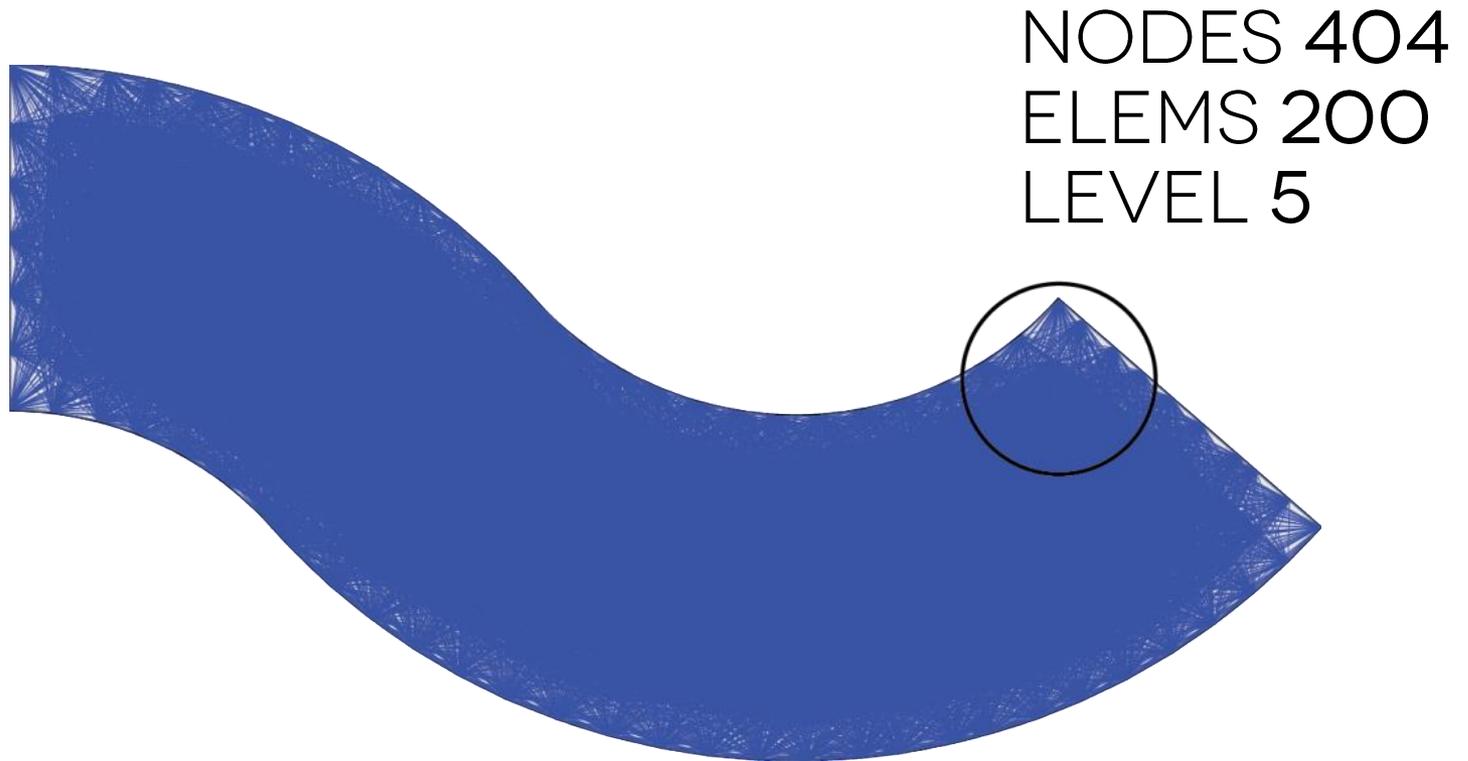
KARMAKAR N (1984) "A NEW POLYNOMIAL-TIME ALGORITHM FOR LINEAR PROGRAMMING." COMBINATORICA, 4(4):373-395.

WRIGHT MH (2004) "THE INTERIOR-POINT REVOLUTION IN OPTIMIZATION: HISTORY, RECENT DEVELOPMENTS, AND LASTING CONSEQUENCES." BULLETIN OF THE AMERICAN MATHEMATICAL SOCIETY, 42(1):39-56.

$$\begin{aligned} \min_{\mathbf{s}^+, \mathbf{s}^-} \quad & V = \mathbf{1}^T \left(\frac{\mathbf{s}^+}{\sigma_T} + \frac{\mathbf{s}^-}{\sigma_C} \right) \\ \text{s.t.} \quad & \mathbf{B}^T (\mathbf{s}^+ - \mathbf{s}^-) = \mathbf{f} \\ & s_i^+, s_i^- \geq 0 \end{aligned}$$

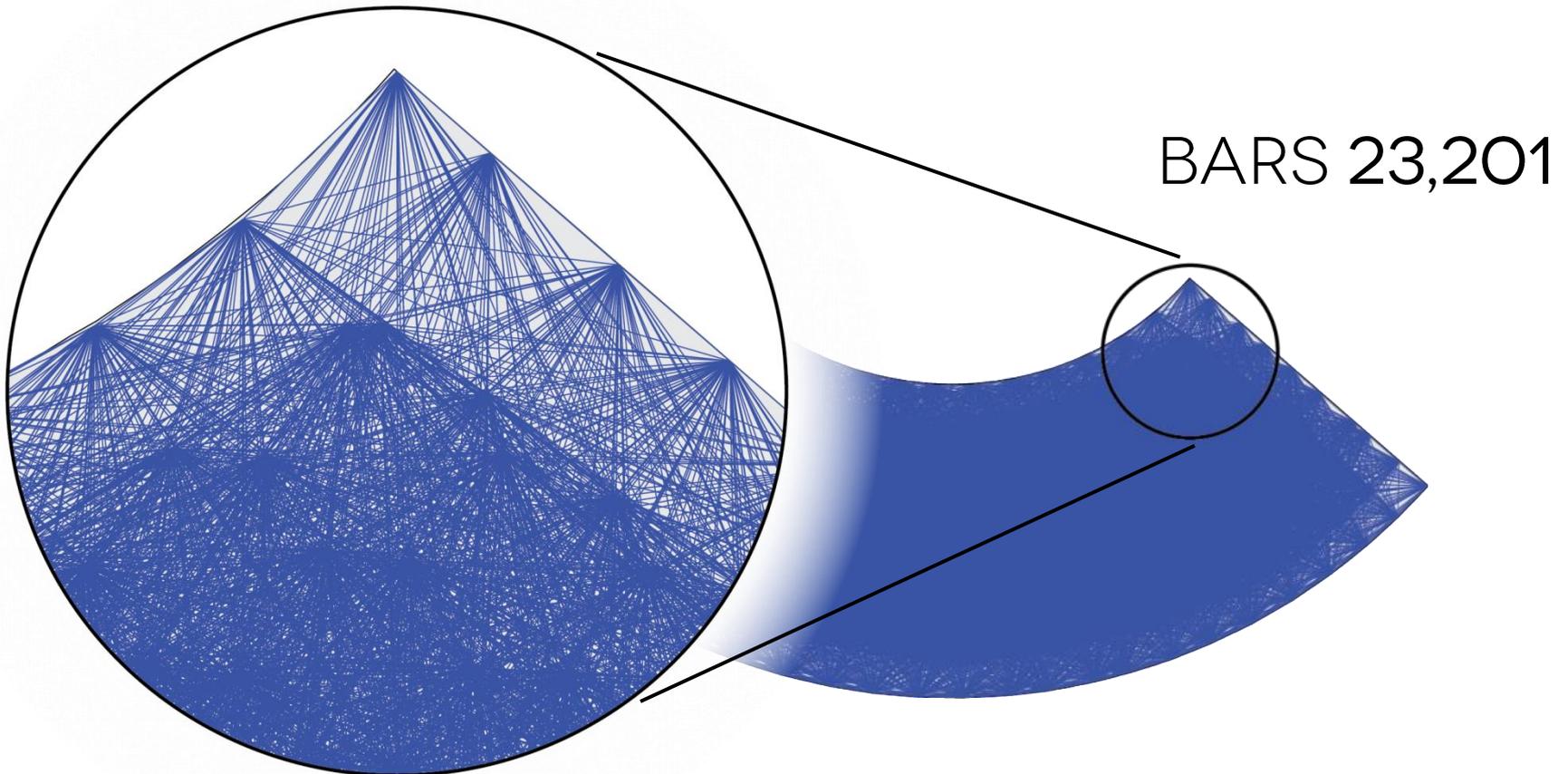
4) GROUND STRUCTURES IN 2D

- SIZING OF A HIGHLY INTERCONNECTED AND REDUNDANT TRUSS



4) GROUND STRUCTURES IN 2D

- SIZING OF A HIGHLY INTERCONNECTED AND REDUNDANT TRUSS



4) GROUND STRUCTURES IN 2D

- UNIQUE SOLUTION — NO COLLINEAR BARS

GIVEN $\sigma_T = 1$ AND $P = 1$

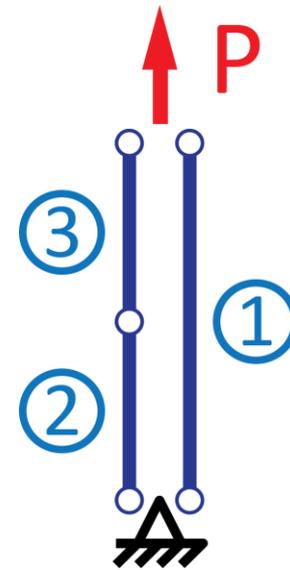
$$a_1 = 1.0$$



$$a_1 = 1.0 \quad a_2 = a_3 = 0.0$$

$$a_1 = 0.0 \quad a_2 = a_3 = 1.0$$

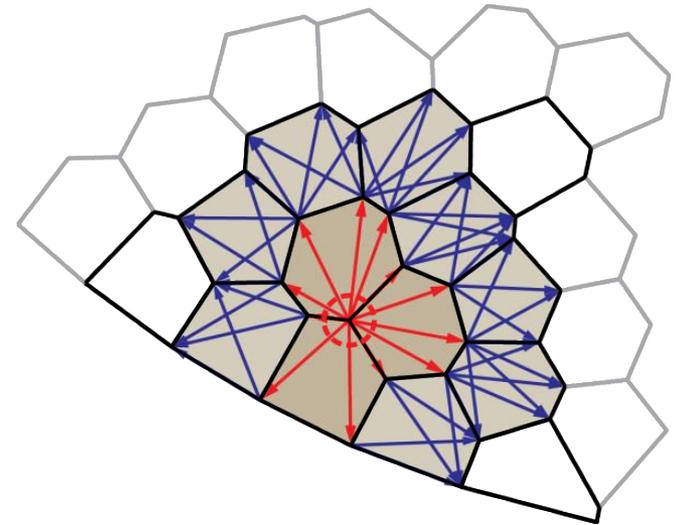
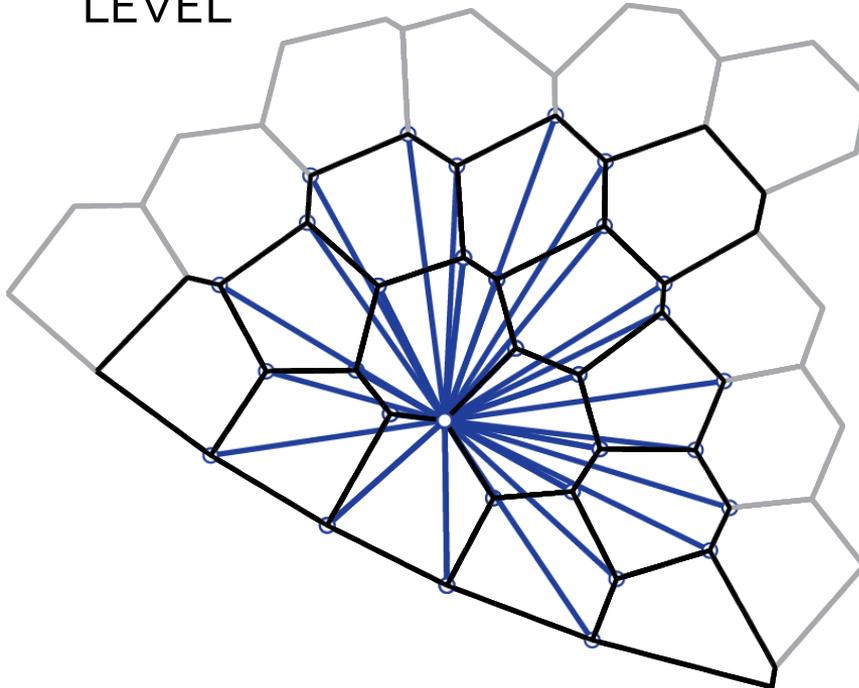
$$a_1 = 0.5 \quad a_2 = a_3 = 0.5$$



4) GROUND STRUCTURES IN 2D

- HIGHLY INTERCONNECTED TRUSS
– CONNECTIVITY GENERATION

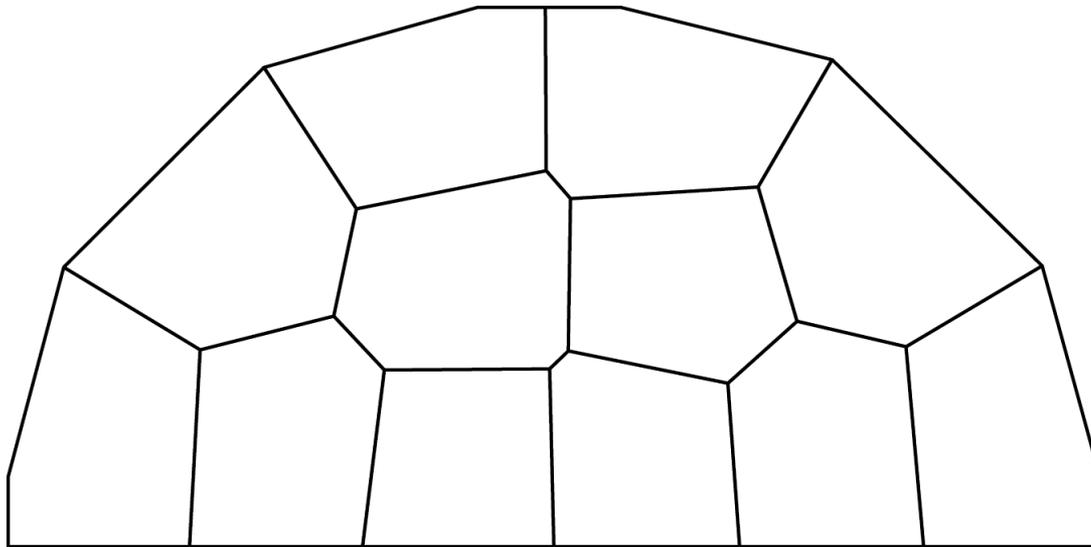
TRUSS MEMBERS
AT THIS CONNECTION
LEVEL



CONNECTION LEVEL: ~~DNR~~

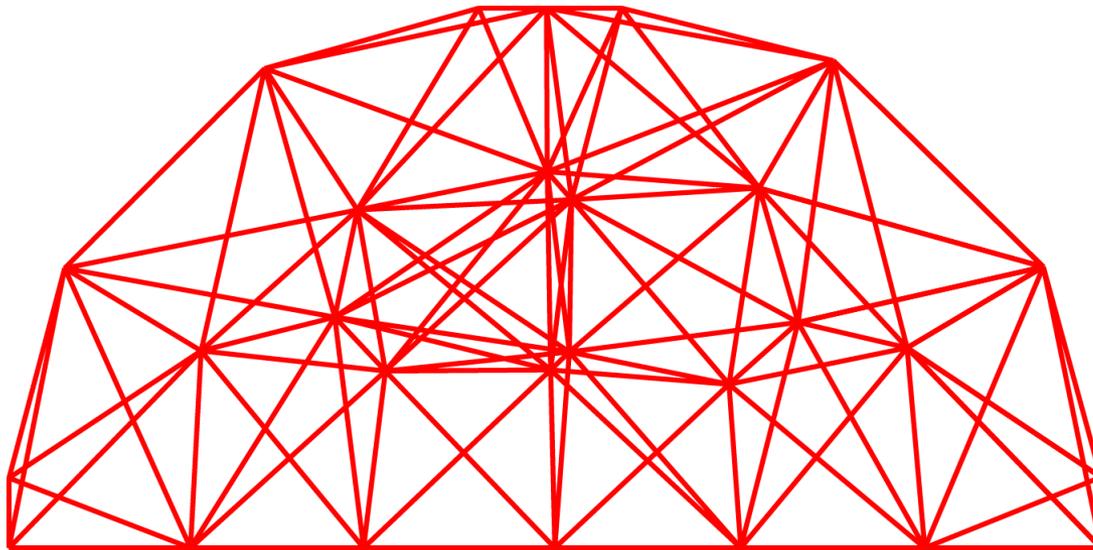
4) GROUND STRUCTURES IN 2D

- EXAMPLE
 - BASE MESH



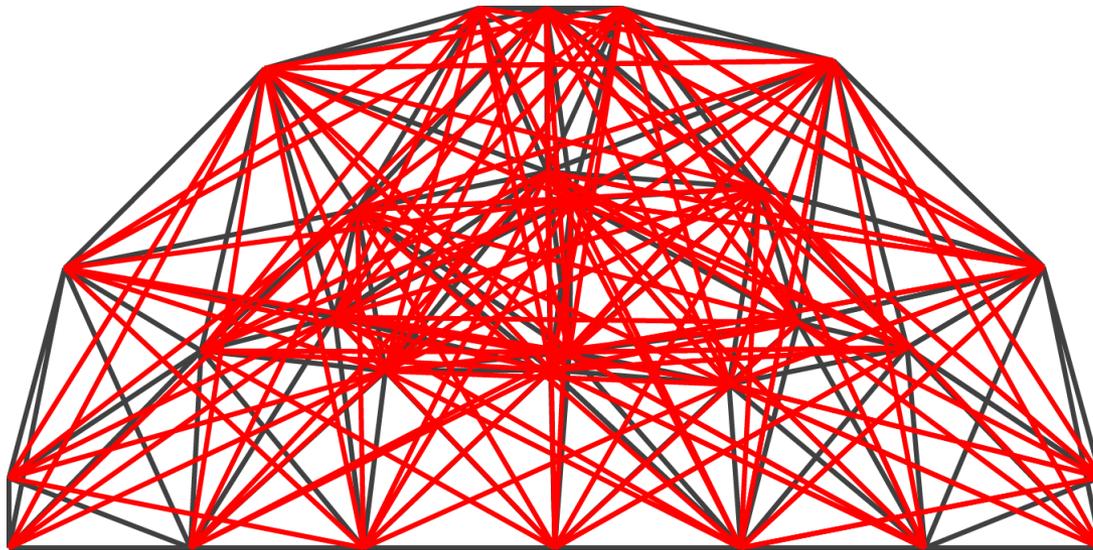
GROUND STRUCTURE METHOD

- EXAMPLE
 - CONNECTIVITY: LEVEL 1



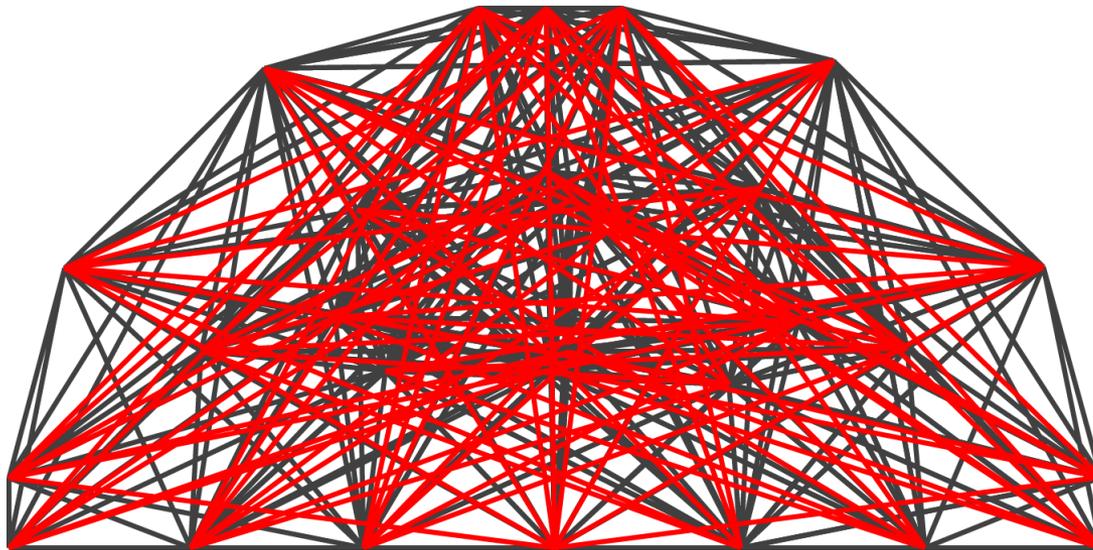
4) GROUND STRUCTURES IN 2D

- EXAMPLE
 - CONNECTIVITY: LEVEL 2



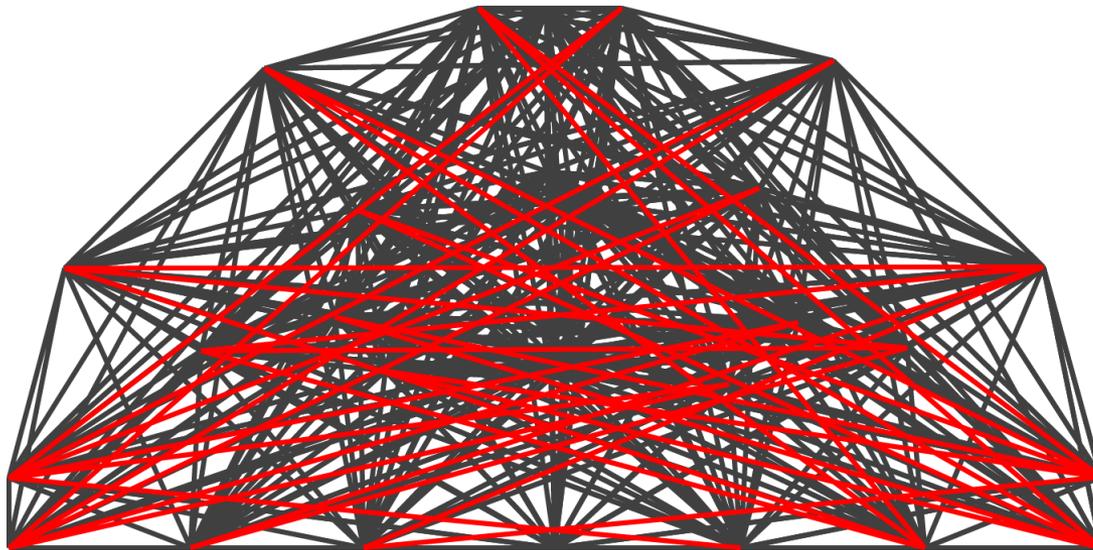
4) GROUND STRUCTURES IN 2D

- EXAMPLE
 - CONNECTIVITY: LEVEL 3



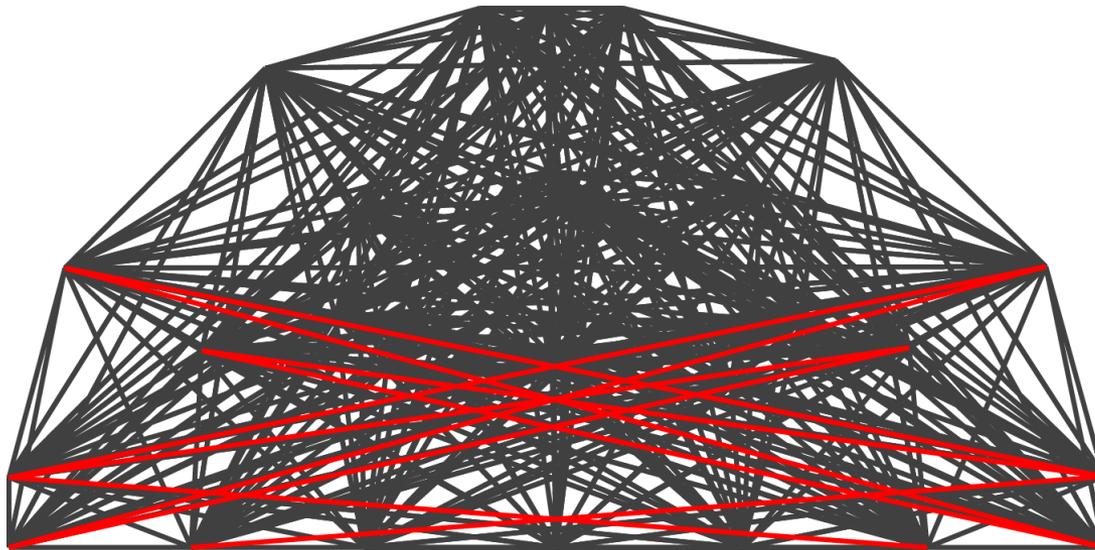
4) GROUND STRUCTURES IN 2D

- EXAMPLE
 - CONNECTIVITY: LEVEL 4



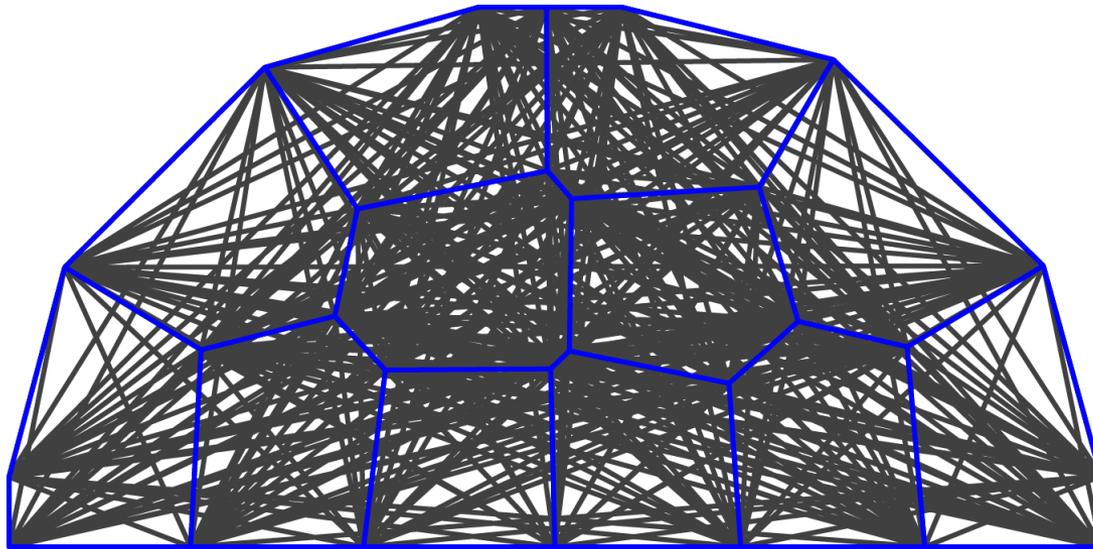
4) GROUND STRUCTURES IN 2D

- EXAMPLE
 - CONNECTIVITY: LEVEL 5



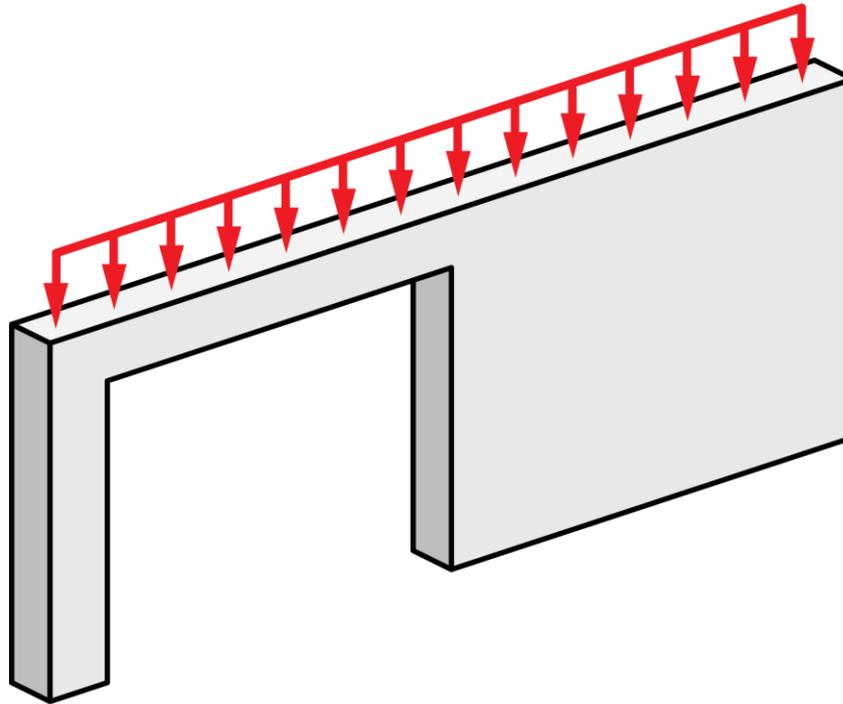
4) GROUND STRUCTURES IN 2D

- EXAMPLE
 - CONNECTIVITY: LEVEL 5



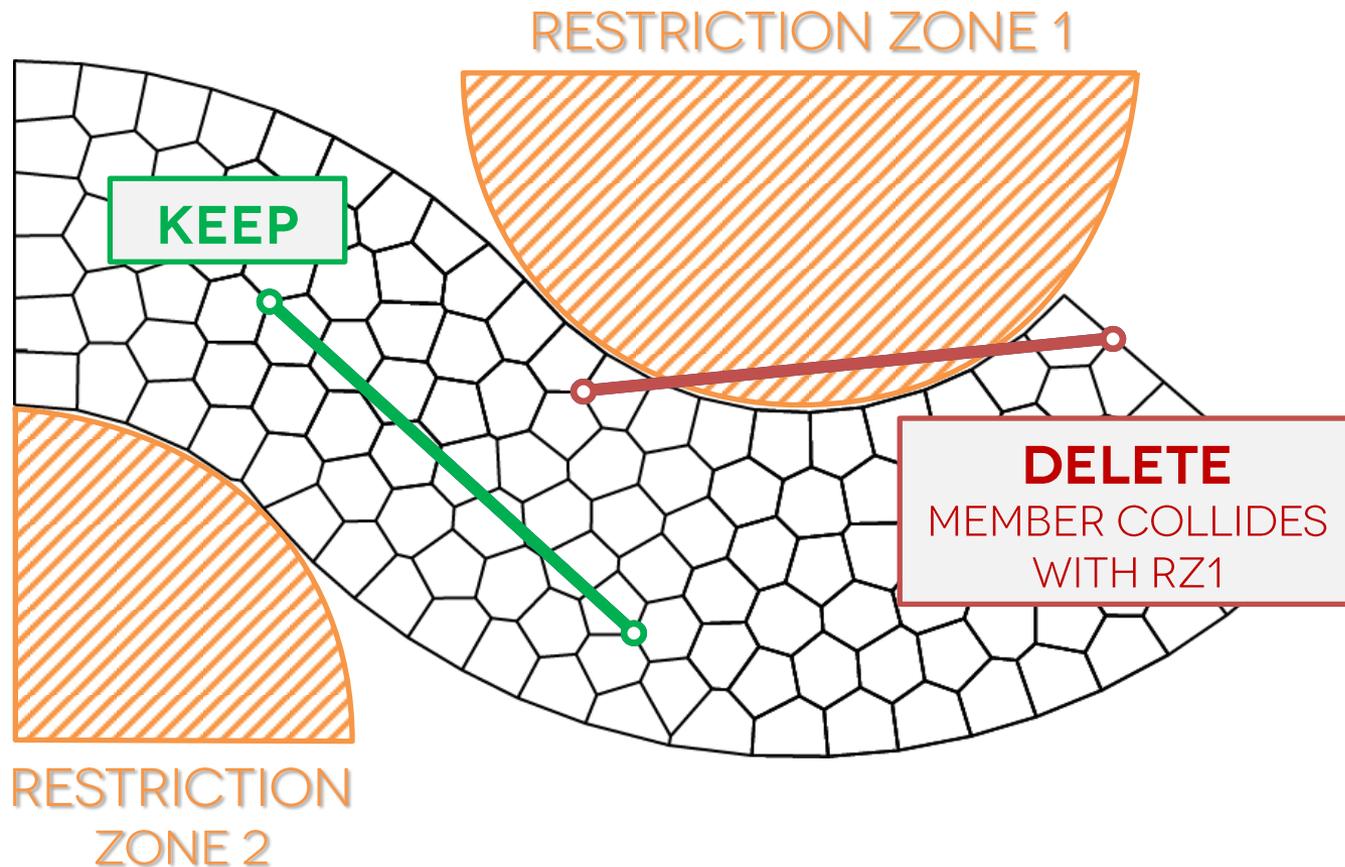
4) GROUND STRUCTURES IN 2D

- THERE CANNOT BE BARS **EVERYWHERE**
 - DEFINE ZONES WHERE NO BARS CAN BE



4) GROUND STRUCTURES IN 2D

- INTERSECTION TESTS FROM VIDEO-GAME AND COMPUTER GRAPHICS INDUSTRY

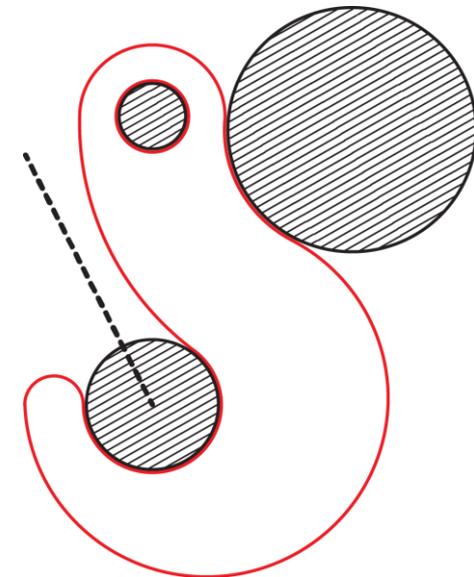
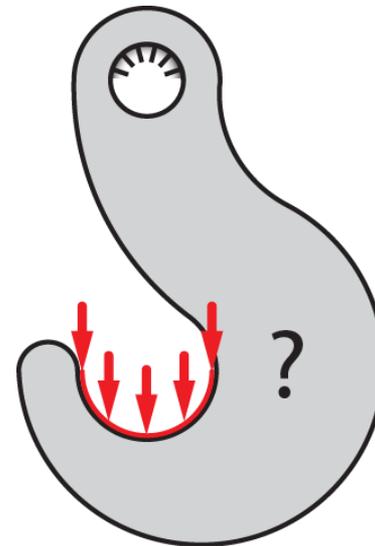


4) GROUND STRUCTURES IN 2D

- RESTRICTION ZONE PRIMITIVES
 - CIRCLE
 - SEGMENT (LINE)
 - RECTANGLE
 - POLYGON

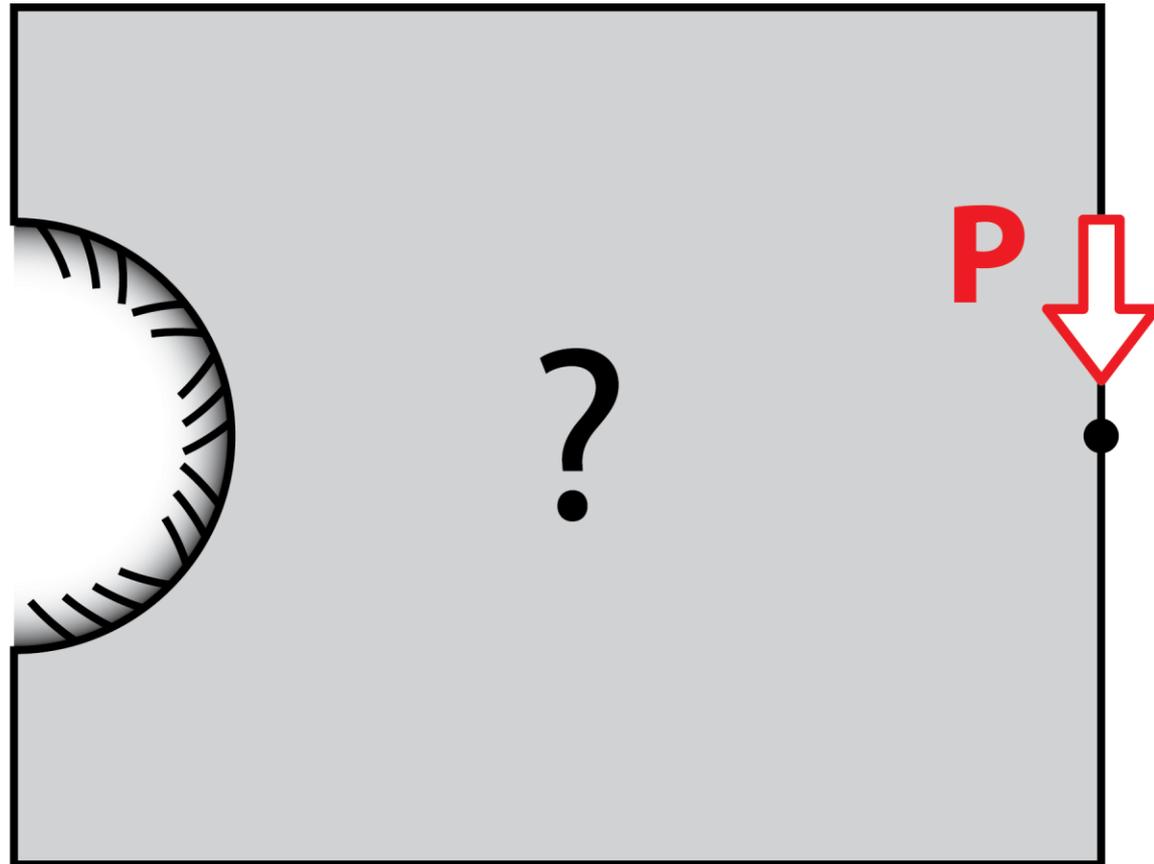
3 CIRCLES
+
1 SEGMENT

- CAN BE COMBINED...



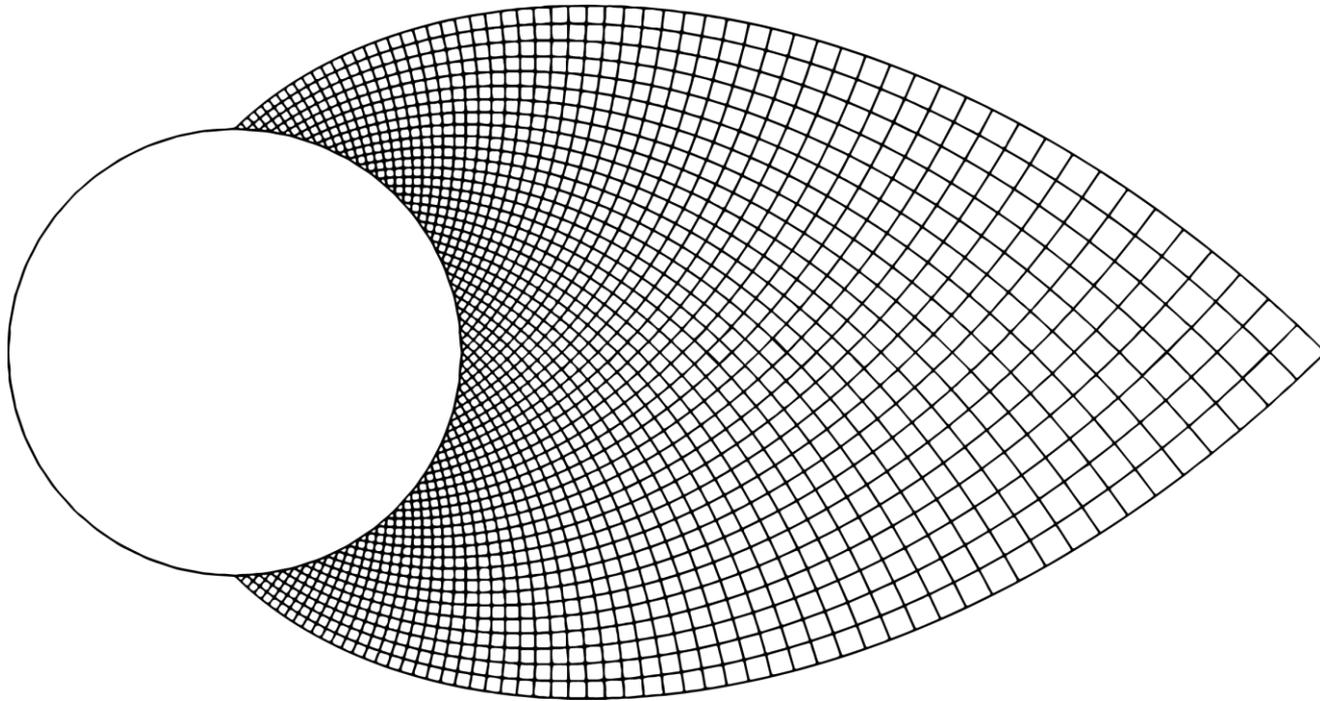
4) GROUND STRUCTURES IN 2D

- MICHELL CANTILEVER



4) GROUND STRUCTURES IN 2D

- MICHELL CANTILEVER

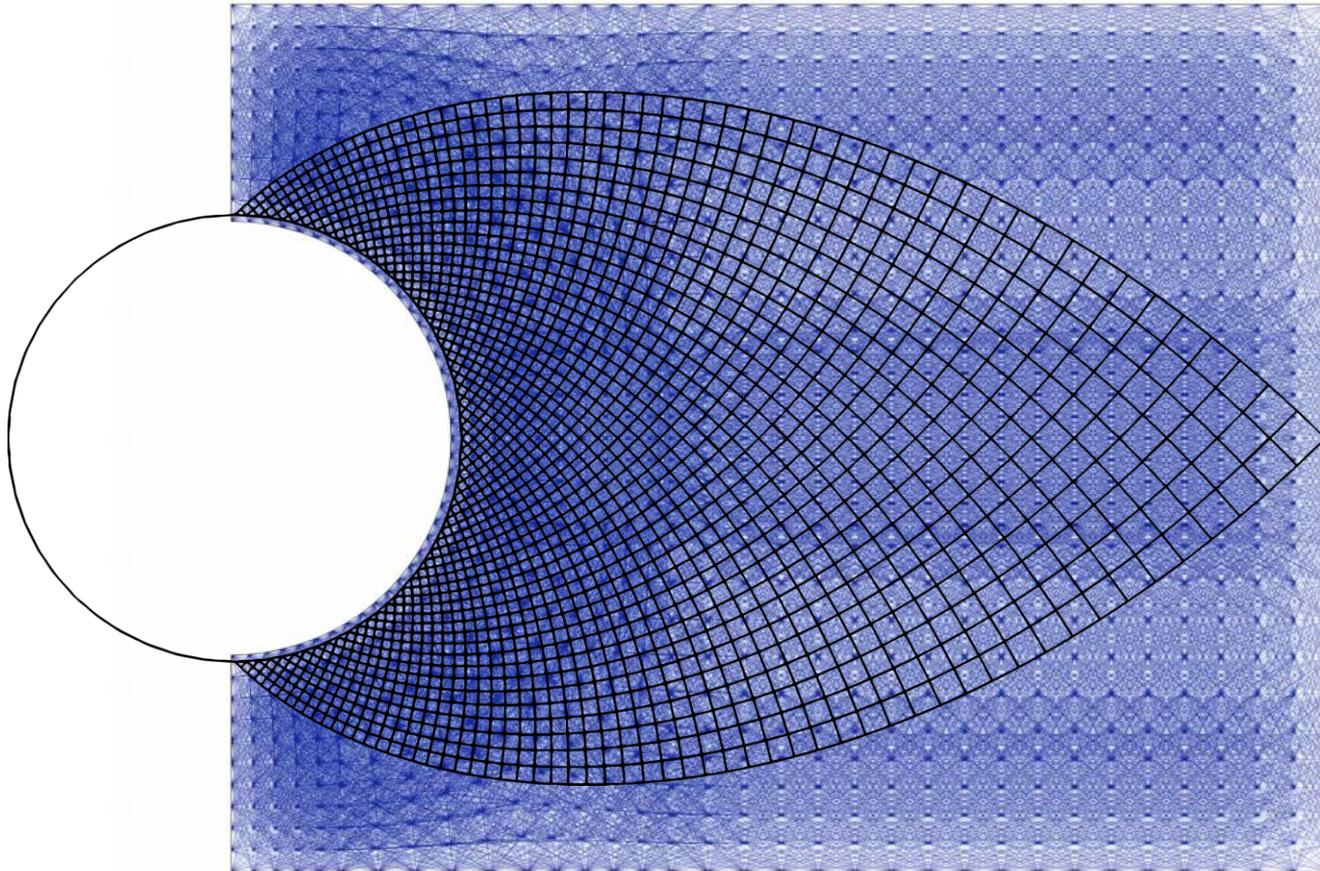


4) GROUND STRUCTURES IN 2D

- MICHELL CANTILEVER

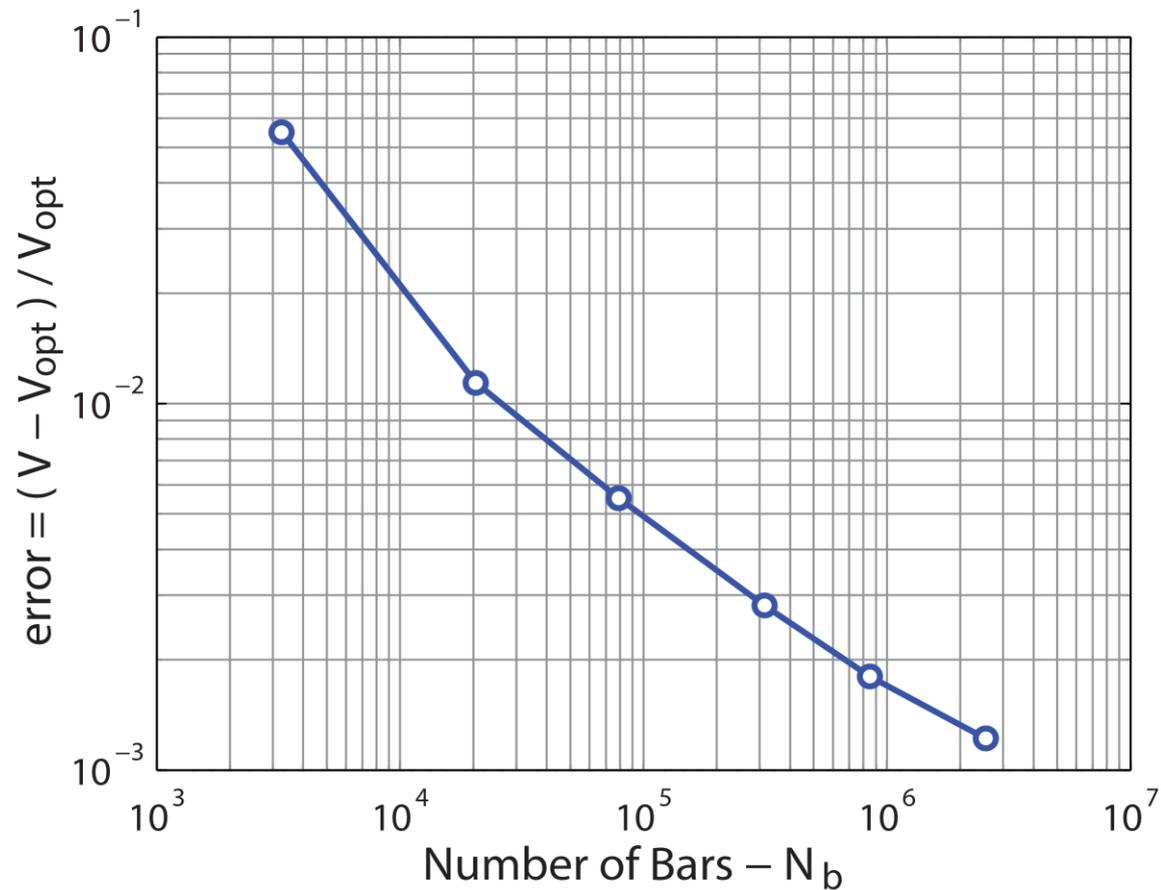
28,256 BARS

Iteration 00



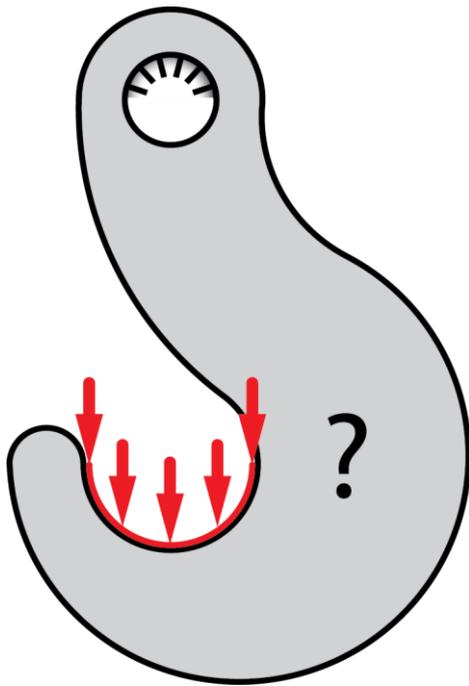
4) GROUND STRUCTURES IN 2D

- MICHELL CANTILEVER

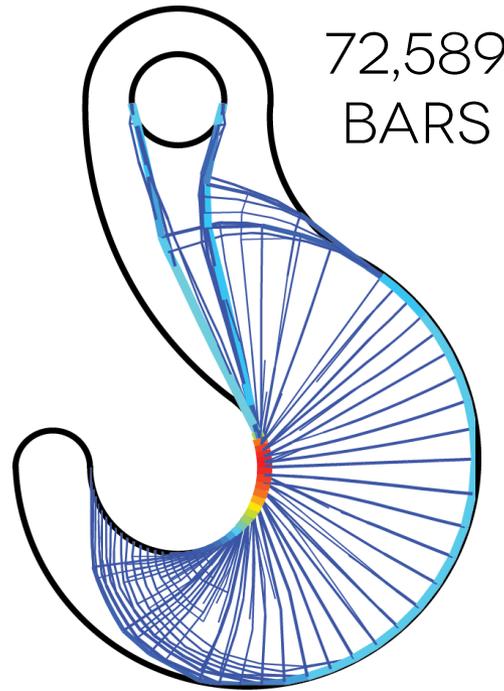


4) GROUND STRUCTURES IN 2D

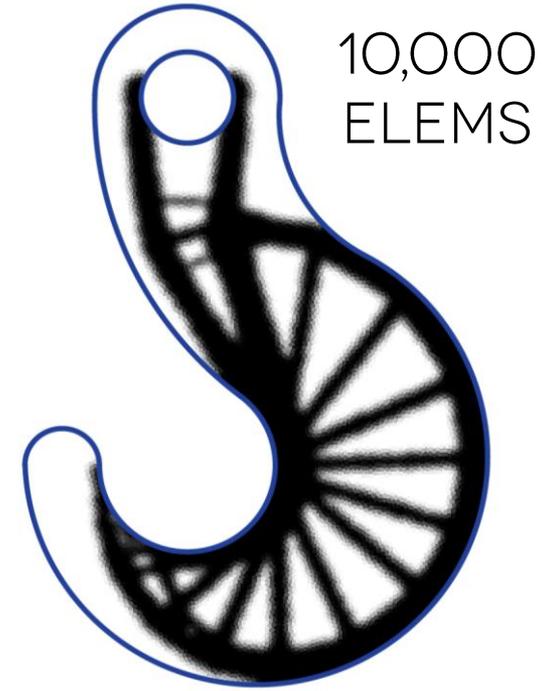
- HOOK PROBLEM



DOMAIN & BCs



GROUND
STRUCTURES

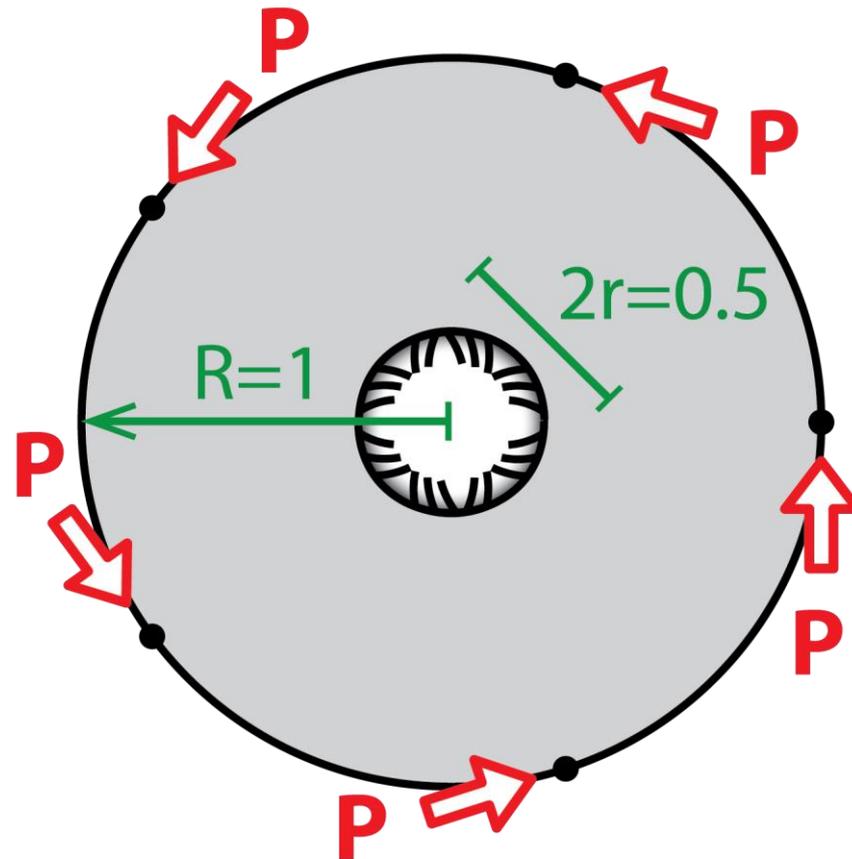


DENSITY-BASED
METHOD \diamond

\diamond TALISCHI C, PAULINO GH, PEREIRA A, MENEZES IFM (2012), "POLYTOP: A MATLAB IMPLEMENTATION OF A GENERAL TOPOLOGY OPTIMIZATION FRAMEWORK USING UNSTRUCTURED POLYGONAL FINITE ELEMENT MESHES", STRUCT. MULTIDISC. OPTIM. 45(3), 329-357

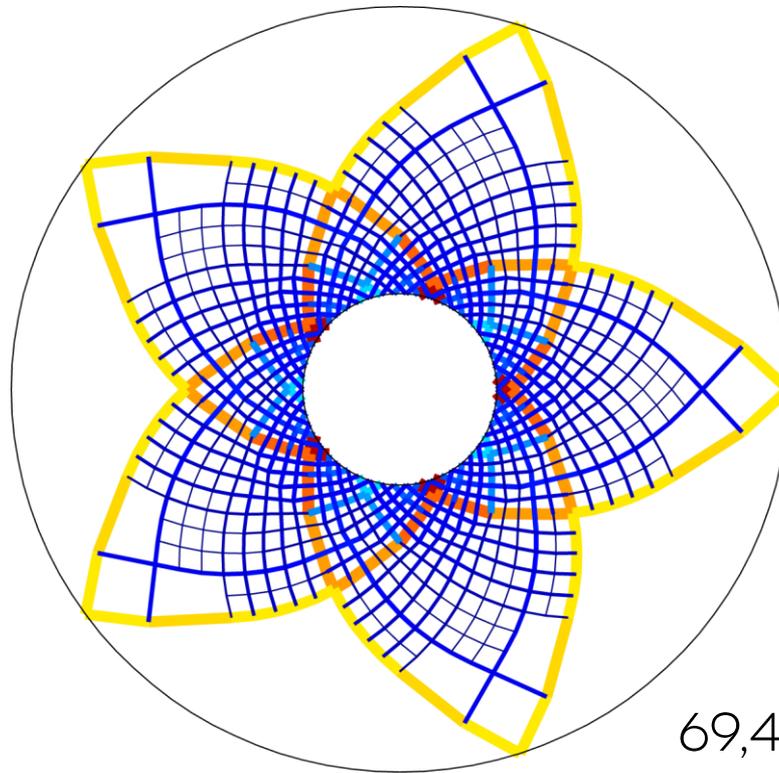
4) GROUND STRUCTURES IN 2D

- FLOWER PROBLEM



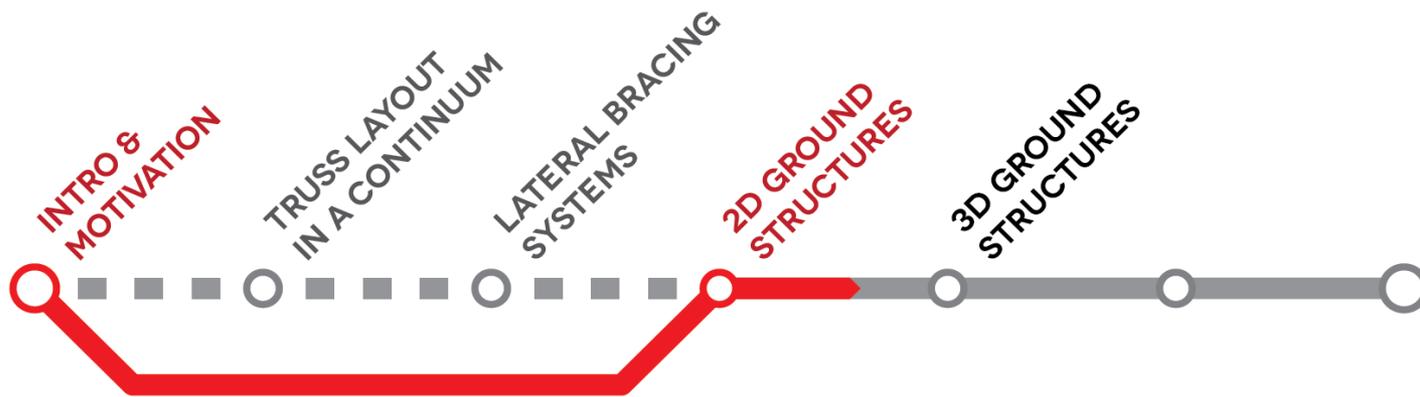
4) GROUND STRUCTURES IN 2D

- FLOWER PROBLEM



69,400 BARS

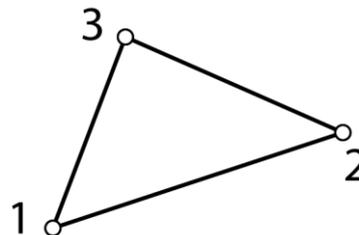
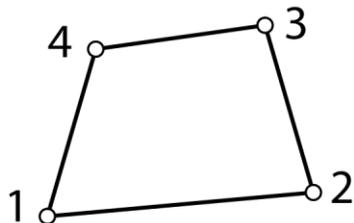
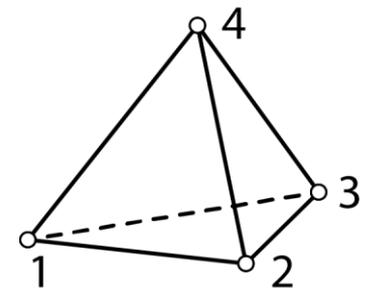
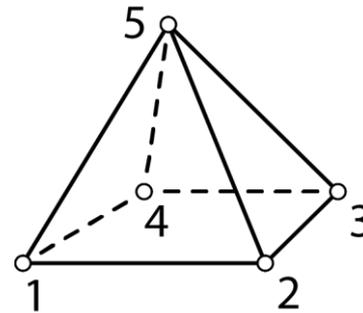
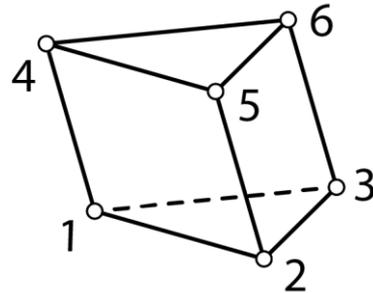
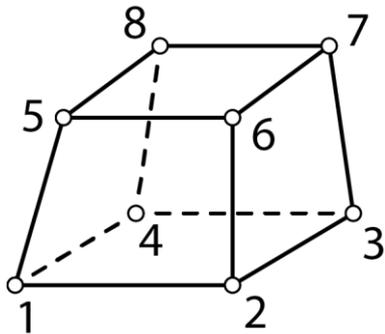
ROADMAP



5) GROUND STRUCTURES IN 3D

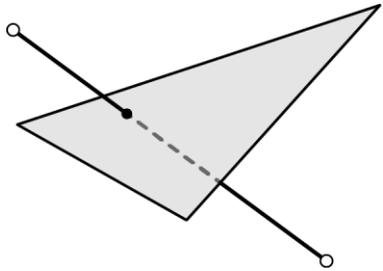
- BASE-MESH DEFINITION

- GROUND STRUCTURE ALGORITHM SUPPORTS ANY CONVEX POLYTOPE
- IMPLEMENTATION IS RESTRICTED TO 7 ELEMENTS: MESH GENERATION AND PLOTTING PURPOSES

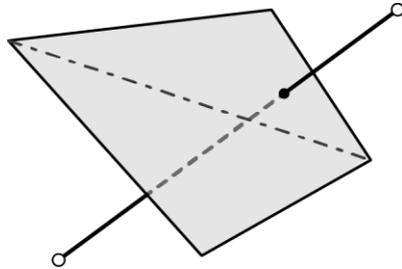


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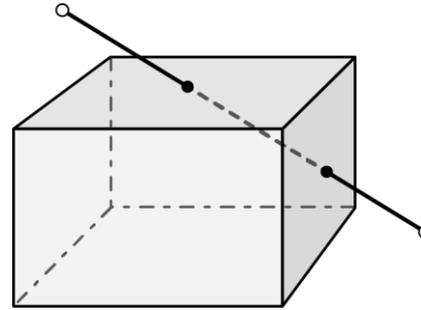
- RESTRICTION PRIMITIVES:



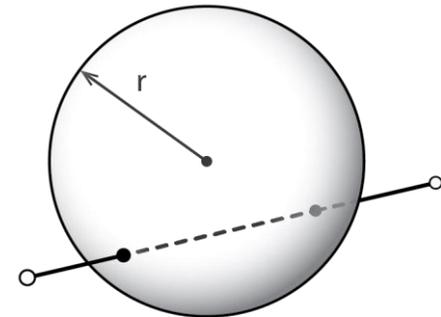
TRIANGLE



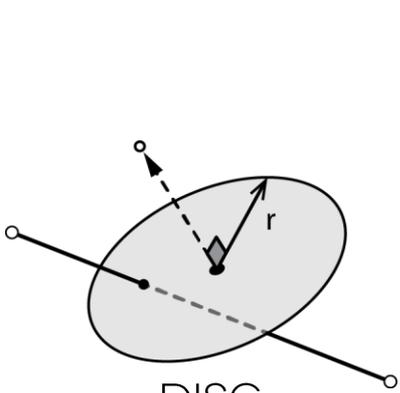
QUAD



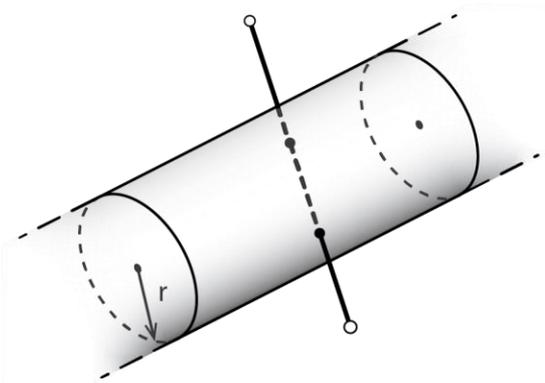
BOX



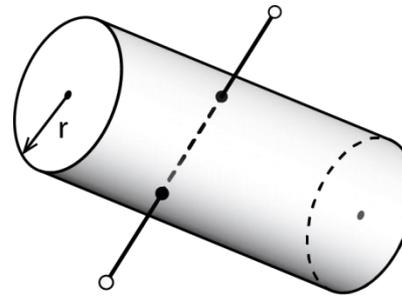
SPHERE



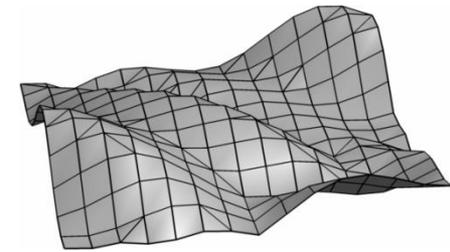
DISC



CYLINDER



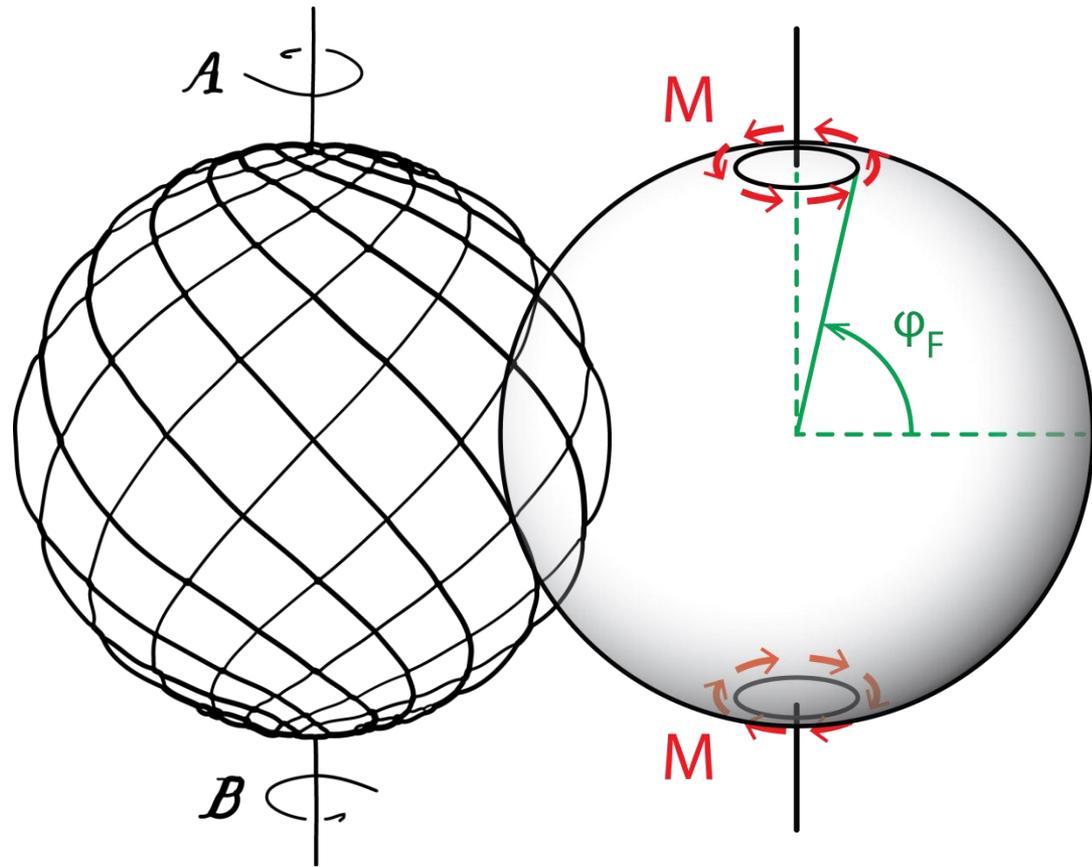
ROD



SURFACE

5) GROUND STRUCTURES IN 3D

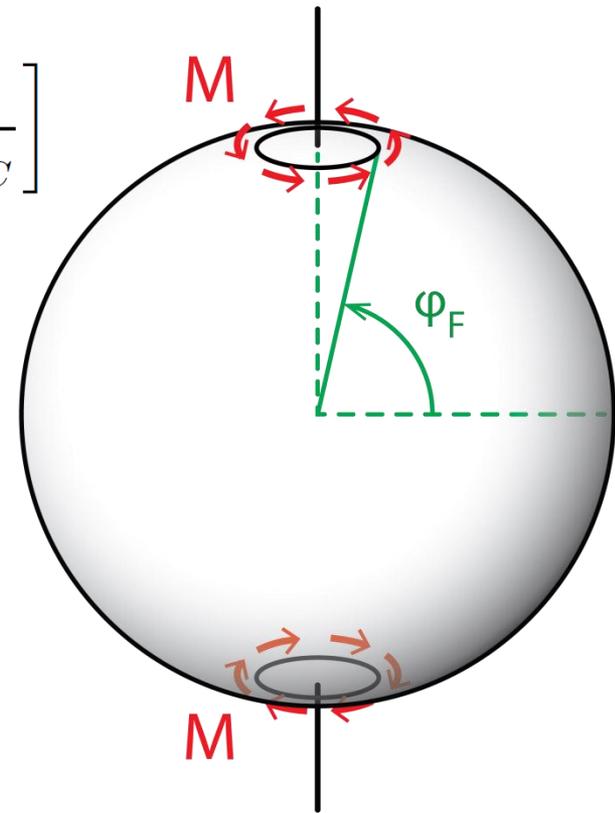
- TORSION BALL PROBLEM



5) GROUND STRUCTURES IN 3D

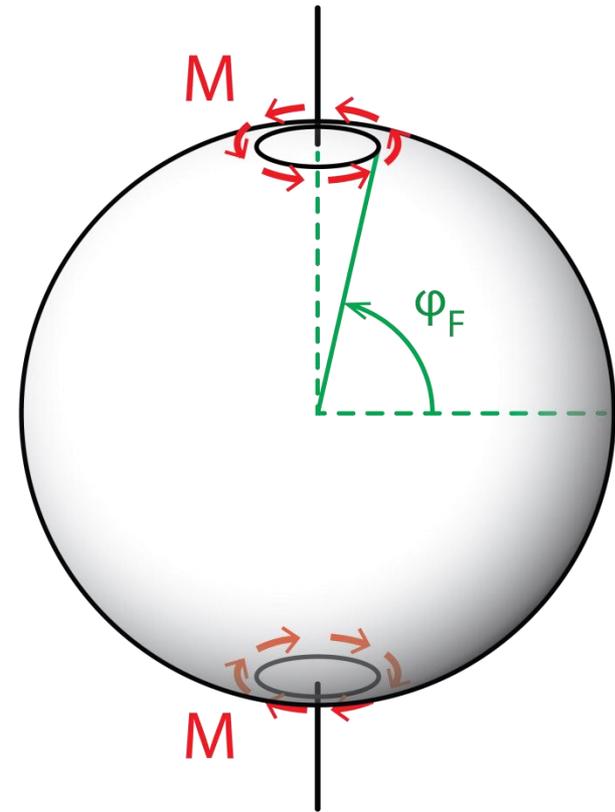
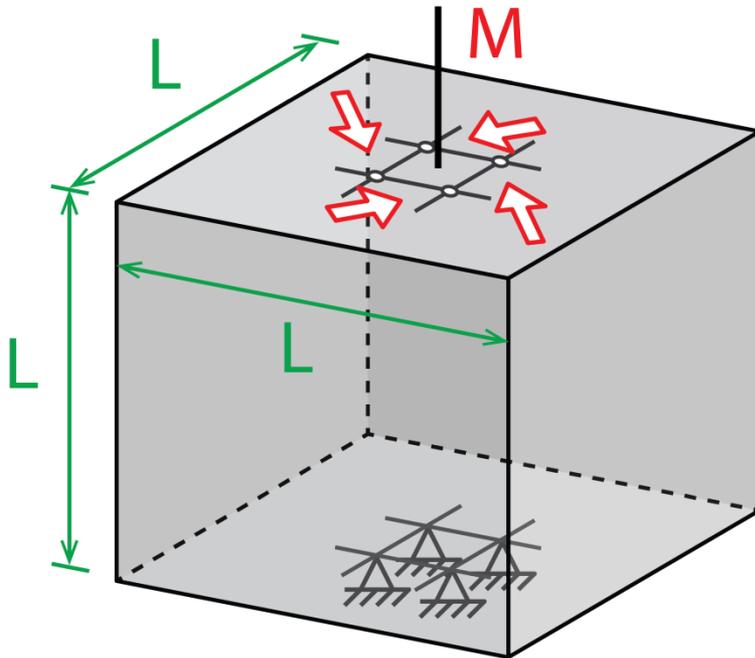
- TORSION BALL PROBLEM

$$V_{opt} = 2M \log \left(\tan \left\{ \frac{\pi}{4} + \frac{\phi_F}{2} \right\} \right) \left[\frac{1}{\sigma_T} + \frac{1}{\sigma_C} \right]$$



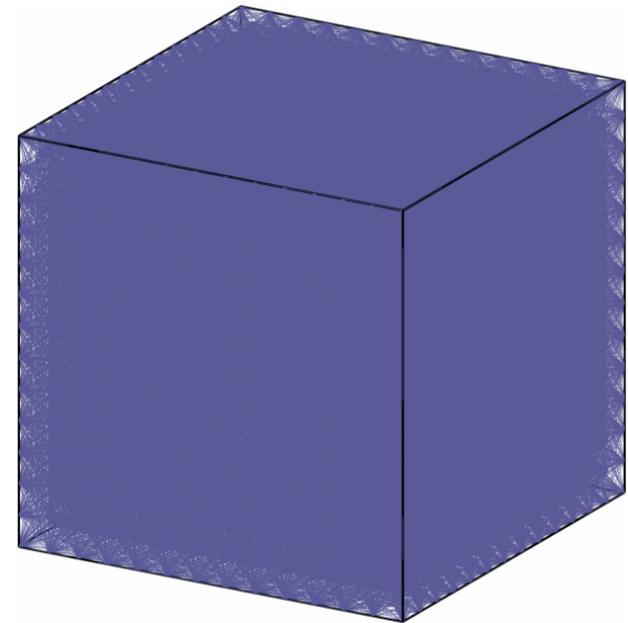
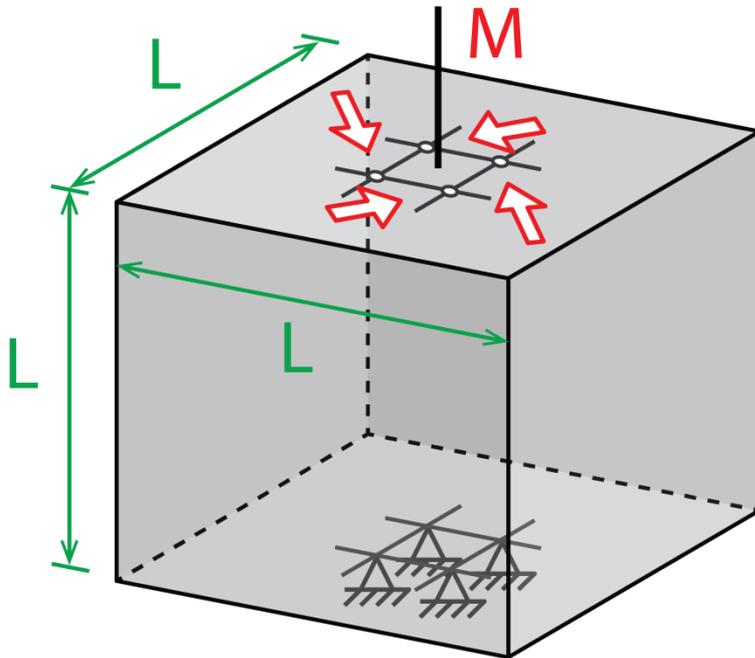
5) GROUND STRUCTURES IN 3D

- TORSION BALL PROBLEM



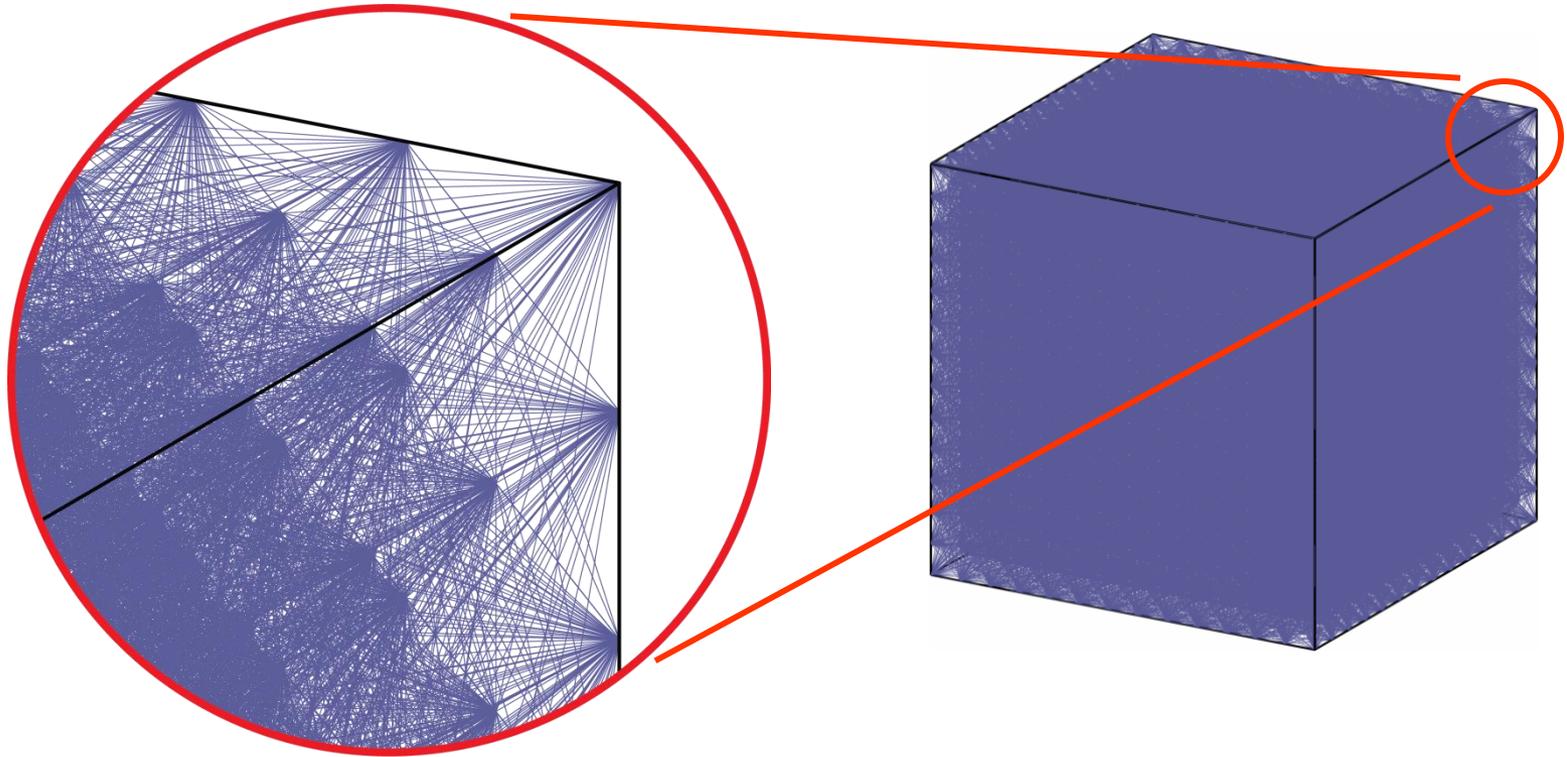
5) GROUND STRUCTURES IN 3D

- TORSION BALL PROBLEM



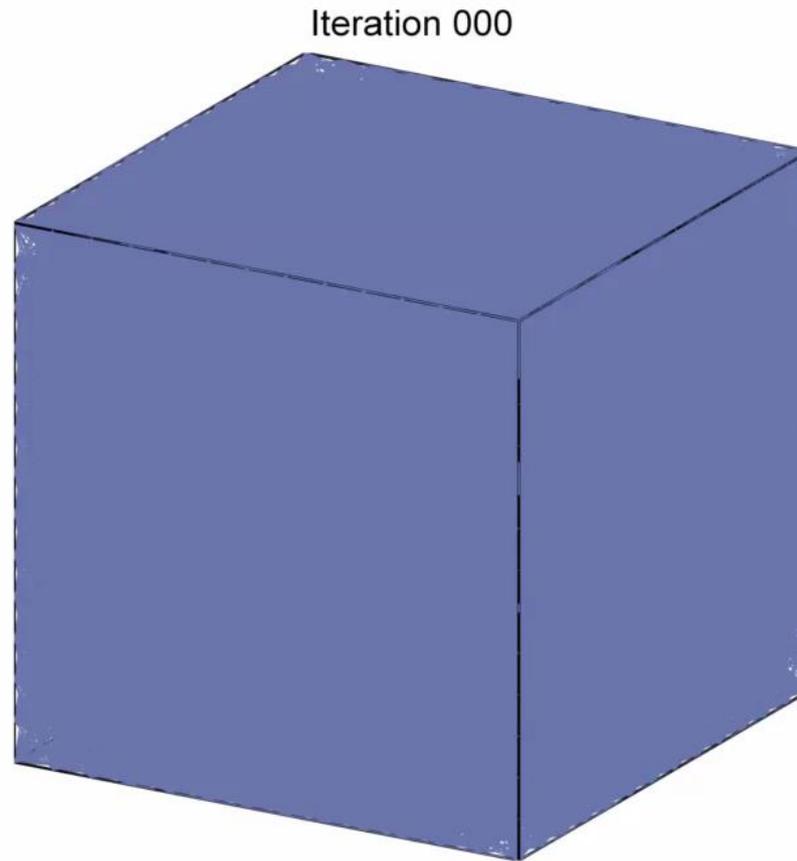
5) GROUND STRUCTURES IN 3D

- TORSION BALL PROBLEM



5) GROUND STRUCTURES IN 3D

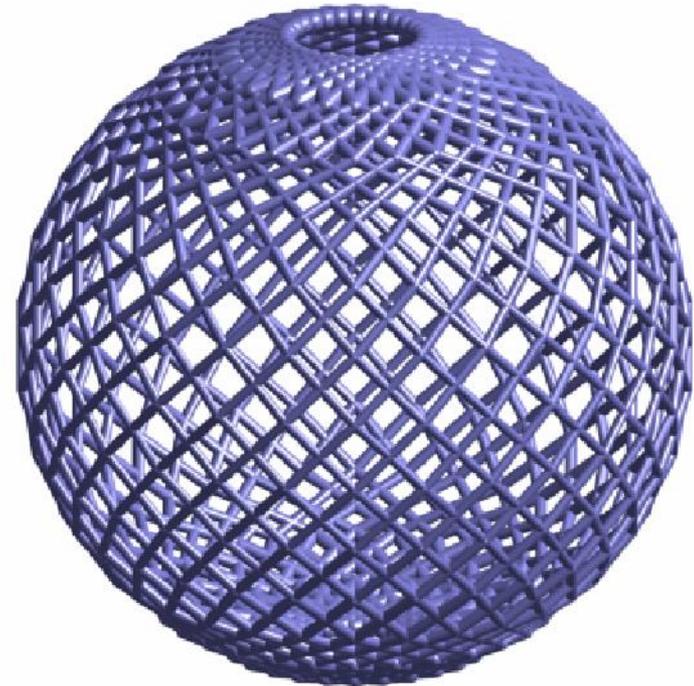
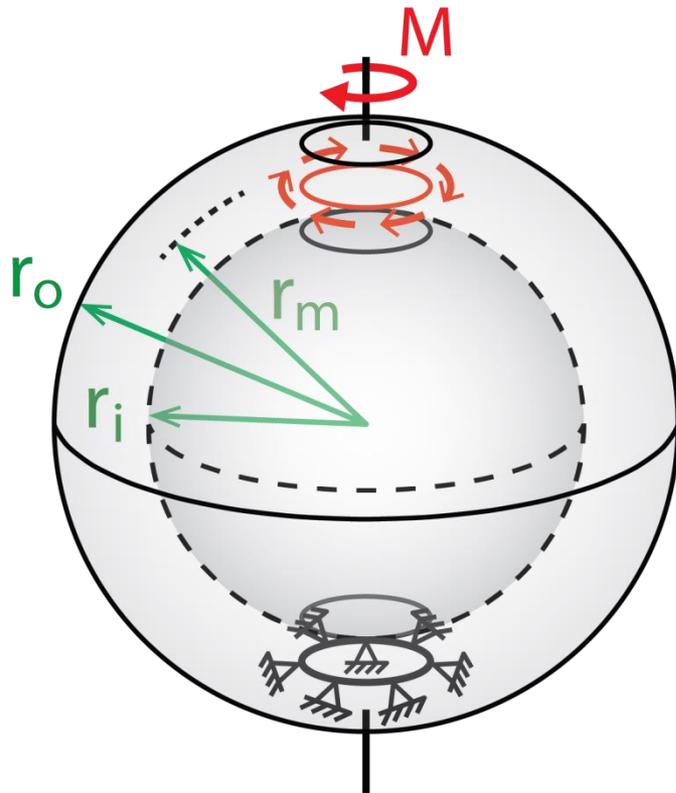
- TORSION BALL PROBLEM



268,636 BARS

5) GROUND STRUCTURES IN 3D

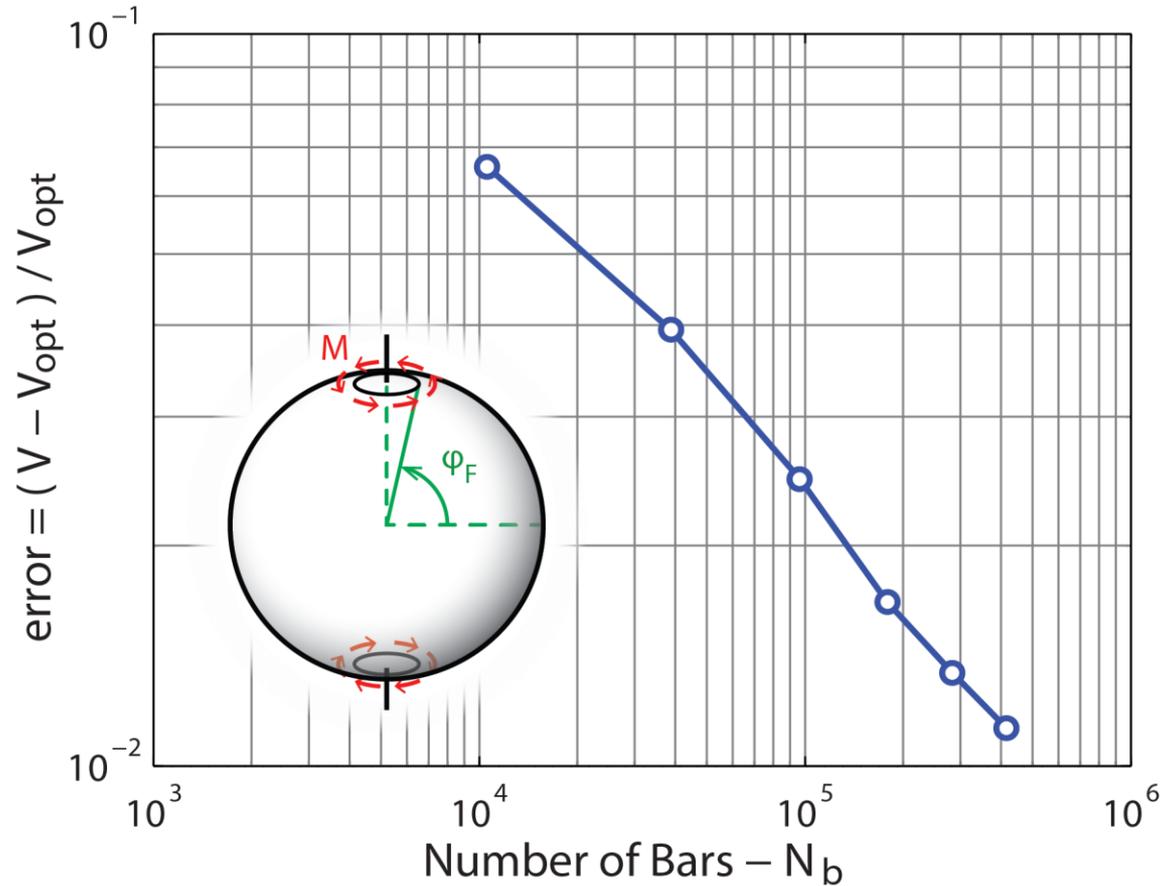
- TORSION BALL
IMPROVING THE BASE MESH: SPHERICAL COORDINATES



5) GROUND STRUCTURES IN 3D

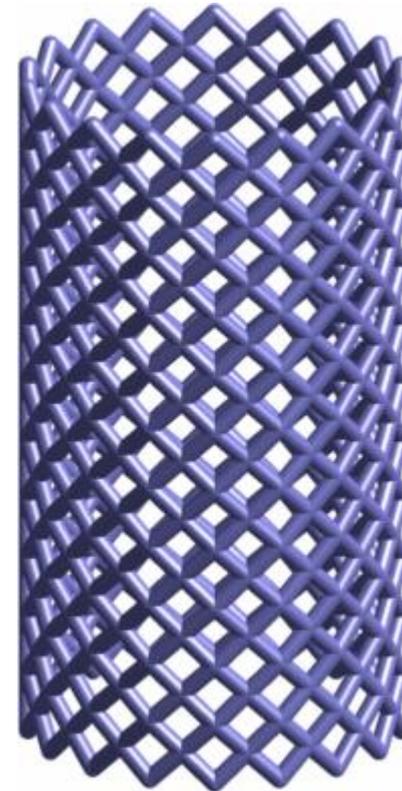
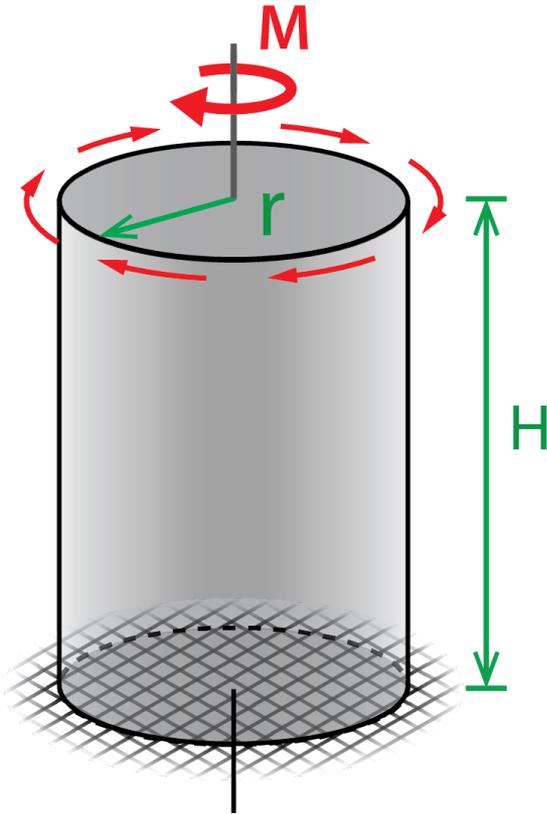
- TORSION BALL

IMPROVING THE BASE MESH: SPHERICAL COORDINATES



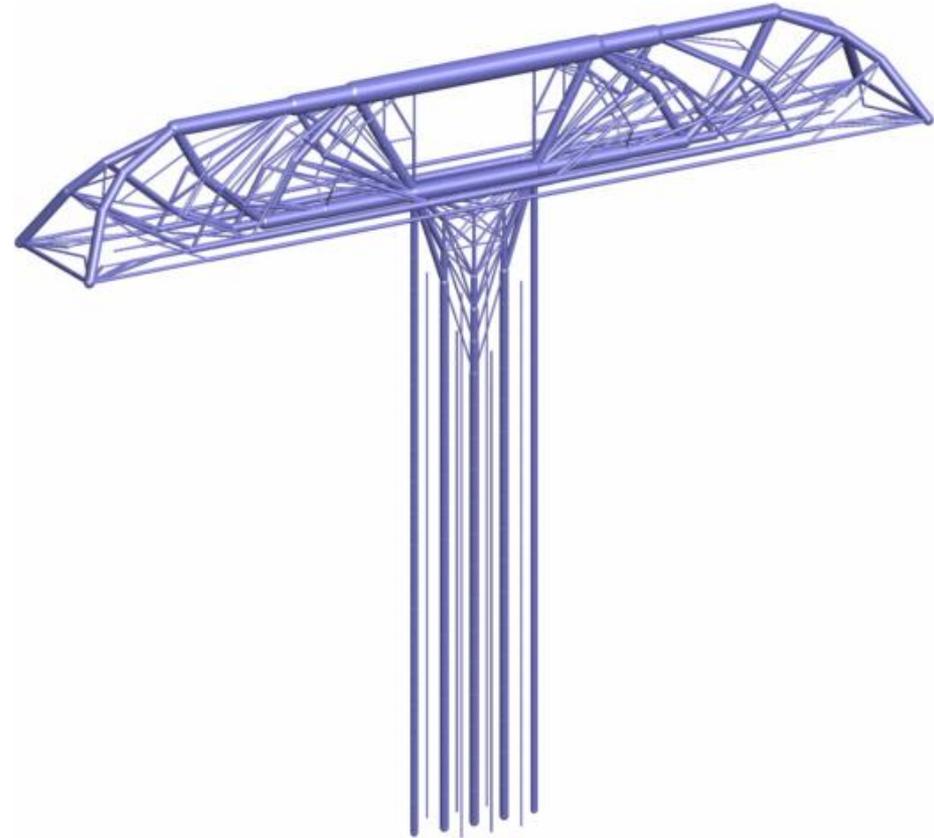
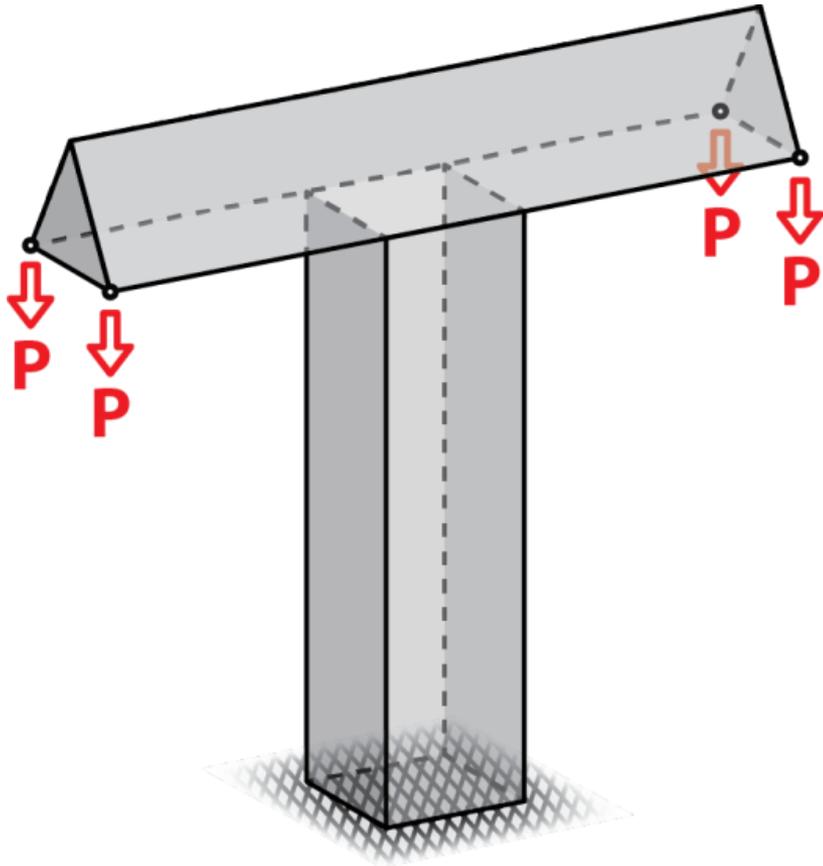
5) GROUND STRUCTURES IN 3D

- OTHER KNOWN SOLUTIONS?



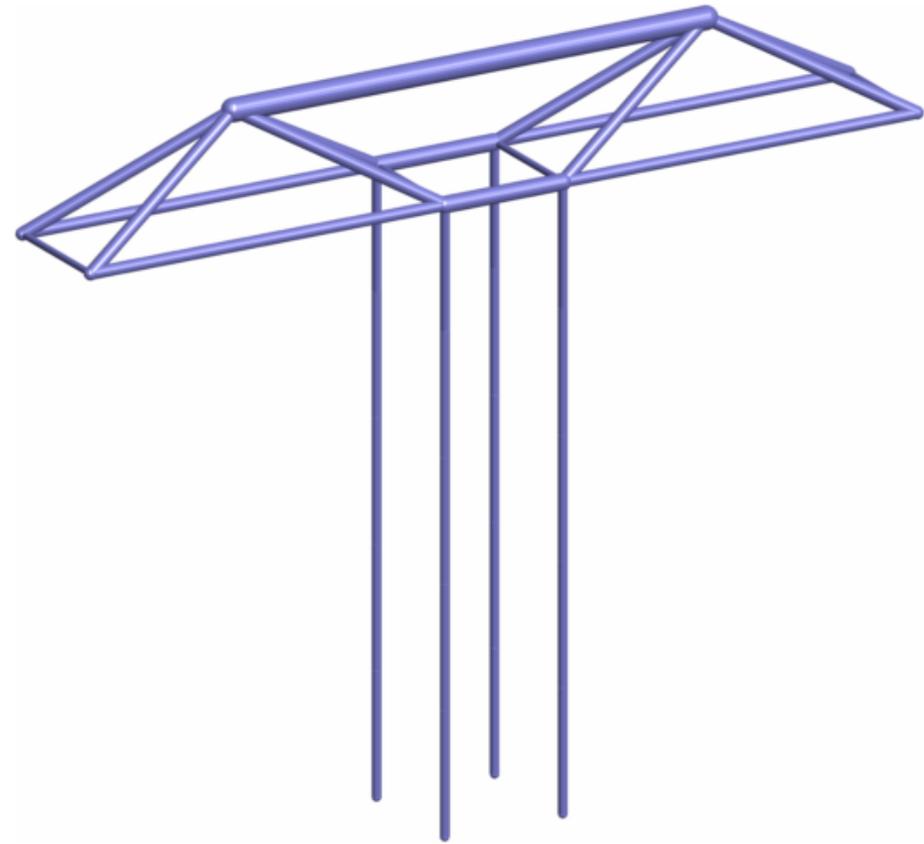
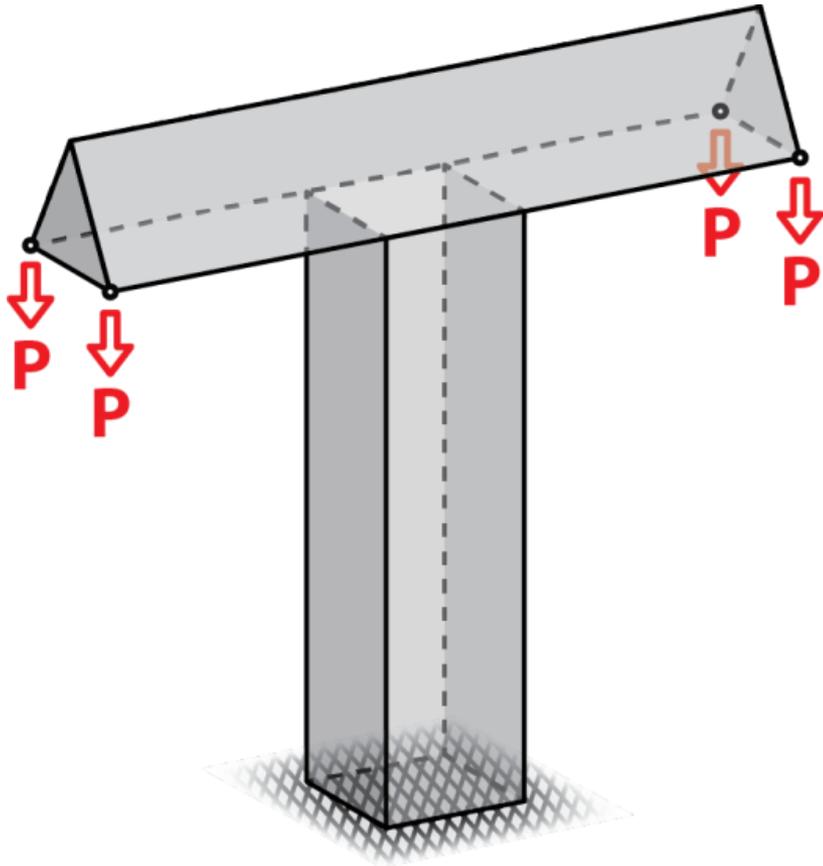
5) GROUND STRUCTURES IN 3D

- MORE APPLIED PROBLEMS?



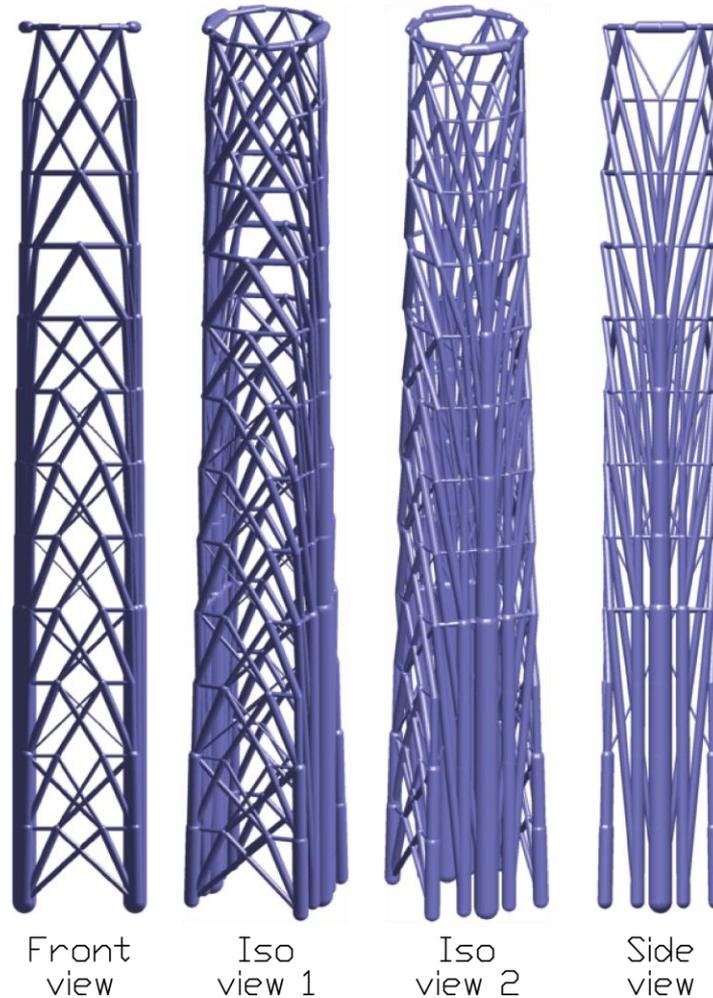
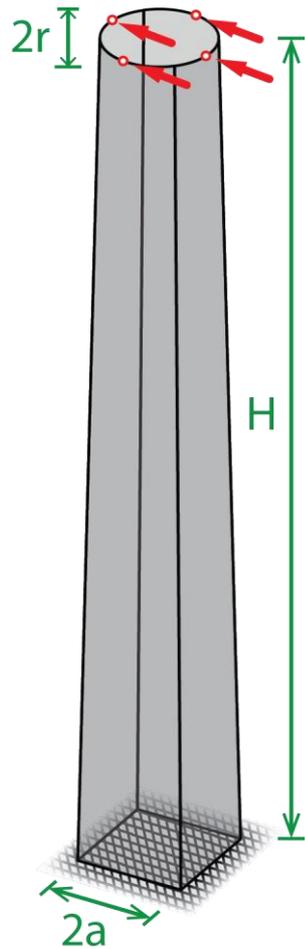
5) GROUND STRUCTURES IN 3D

- MORE APPLIED PROBLEMS?



5) GROUND STRUCTURES IN 3D

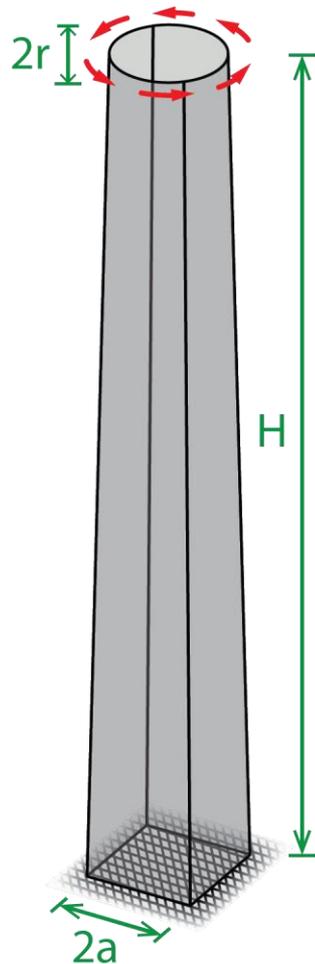
- MORE APPLIED PROBLEMS?



4,100
BARS

5) GROUND STRUCTURES IN 3D

- MORE APPLIED PROBLEMS?



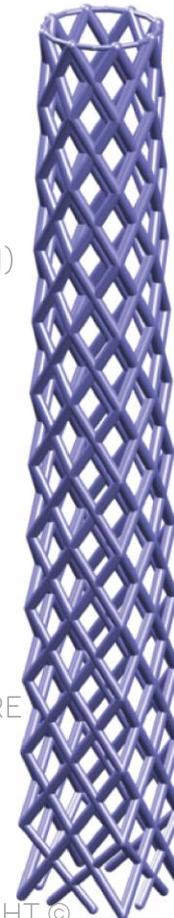
LLP (SOM)

MERRILL
&

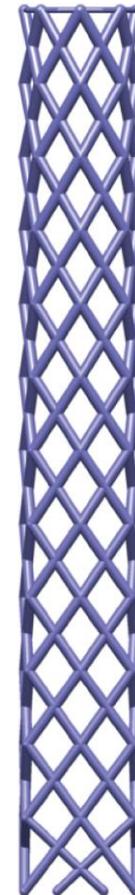
OWINGS
,

SKIDMORE

COPYRIGHT ©



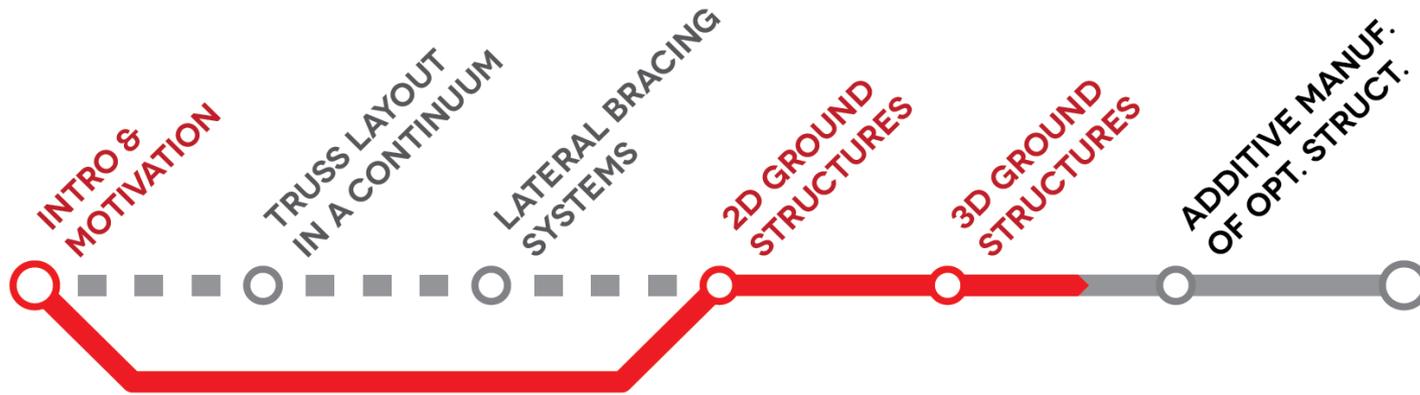
Iso
view



Front
view

4,100
BARS

ROADMAP



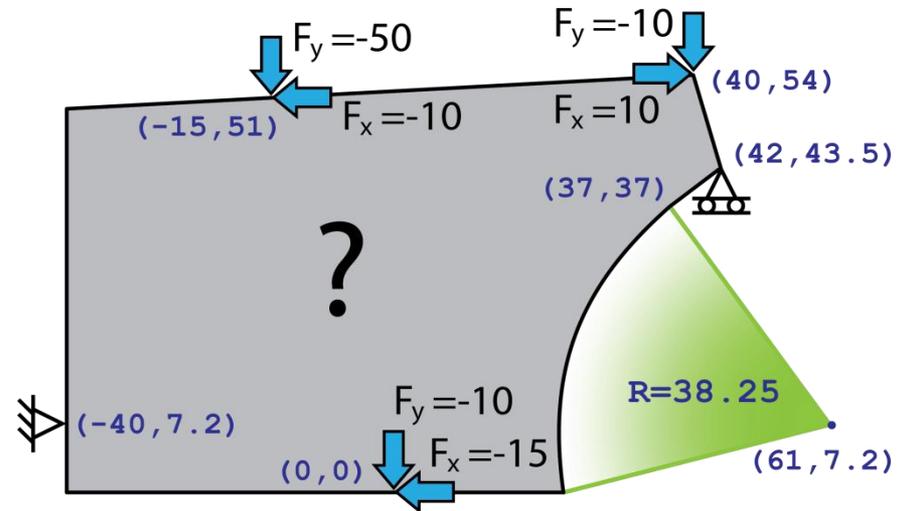
6) ADDITIVE MANUF. OF OPT. STRUCTS.

- INTRODUCTION TO DENSITY-BASED TOPOLOGY OPTIMIZATION



[HTTP://WWW.CANNONDALE.COM](http://www.cannondale.com)

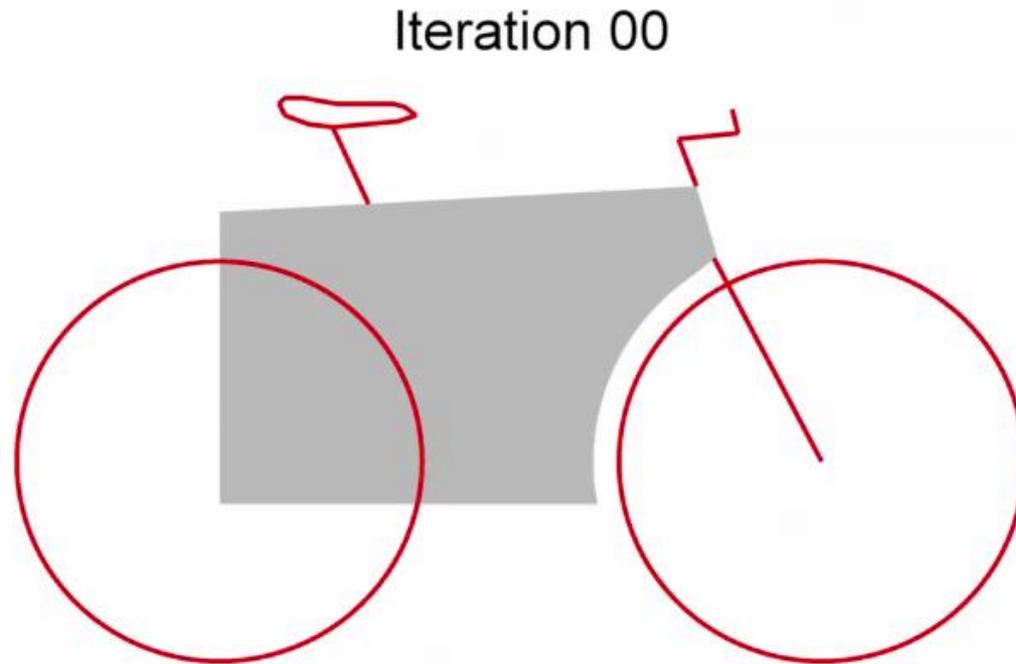
CANNONDALE CAPO
(URBAN COMMUTER BIKE)



BIKE DOMAIN AND LOADS

6) ADDITIVE MANUF. OF OPT. STRUCTS.

- INTRODUCTION TO DENSITY-BASED TOPOLOGY OPTIMIZATION



6) ADDITIVE MANUF. OF OPT. STRUCTS.

- DENSITY-BASED (NESTED) FORMULATION:
 - USING A DENSITY FILTER¹
 - MODIFIED SIMP²³⁴

$$\min_{\boldsymbol{\rho}} J(\boldsymbol{\rho}, \mathbf{u}(\boldsymbol{\rho}))$$

$$\text{s.t. } \bar{\boldsymbol{\rho}} = \mathbf{H}\boldsymbol{\rho}$$

$$\sum_i^{N_e} \bar{\rho}_i v_i - (f)(V_0) \leq 0$$

$$g_i(\boldsymbol{\rho}, \mathbf{u}(\boldsymbol{\rho})) \leq 0 \quad i = 1 \dots N_e$$

$$0 \leq \rho_j \leq 1 \quad j = 1 \dots N_e$$

$$E_k(\bar{\rho}_k) = E_{min} + \bar{\rho}_k^p (E_0 - E_{min}) \quad k = 1 \dots N_e$$

$$\text{with } \mathbf{K}(\bar{\boldsymbol{\rho}}) \mathbf{u} = \mathbf{f}$$

FILTERING

VOLUME
CONSTRAINT

1 = SOLID
0 = VOID

MOD-SIMP

1) BOURDIN B (2001) "FILTERS IN TOPOLOGY OPTIMIZATION." INTERNATIONAL JOURNAL FOR NUMERICAL METHODS IN ENGINEERING, 50(9):2143-2158

2) BENDSOE MP (1989) "OPTIMAL SHAPE DESIGN AS A MATERIAL DISTRIBUTION PROBLEM." STRUCTURAL AND MULTIDISCIPLINARY OPTIMIZATION 1(4):193-202

3) ZHOU M, ROZVANY G (1991) "THE COC ALGORITHM, PART II: TOPOLOGICAL, GEOMETRICAL AND GENERALIZED SHAPE OPTIMIZATION." COMP METH APPL MECH ENGRG 89:309-336

4) SIGMUND O (2007) "MORPHOLOGY-BASED BLACK AND WHITE FILTERS FOR TOPOLOGY OPTIMIZATION." STRUCTURAL AND MULTIDISCIPLINARY OPTIMIZATION, 33(4-5):401-424.

6) ADDITIVE MANUF. OF OPT. STRUCTS.

- DENSITY-BASED (NESTED) FORMULATION:
 - USING A DENSITY FILTER¹
 - MODIFIED SIMP²³⁴

$$\begin{aligned} \min_{\boldsymbol{\rho}} \quad & J(\boldsymbol{\rho}, \mathbf{u}(\boldsymbol{\rho})) \\ \text{s.t.} \quad & \bar{\boldsymbol{\rho}} = \mathbf{H}\boldsymbol{\rho} \end{aligned}$$

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$$\text{with } \mathbf{K}(\bar{\boldsymbol{\rho}}) \mathbf{u} = \mathbf{f}$$

P=1
VARIABLE THICKNESS
SHEET PROBLEM
(CONVEX)

1) BOURDIN B (2001) "FILTERS IN TOPOLOGY OPTIMIZATION." INTERNATIONAL JOURNAL FOR NUMERICAL METHODS IN ENGINEERING, 50(9):2143-2158

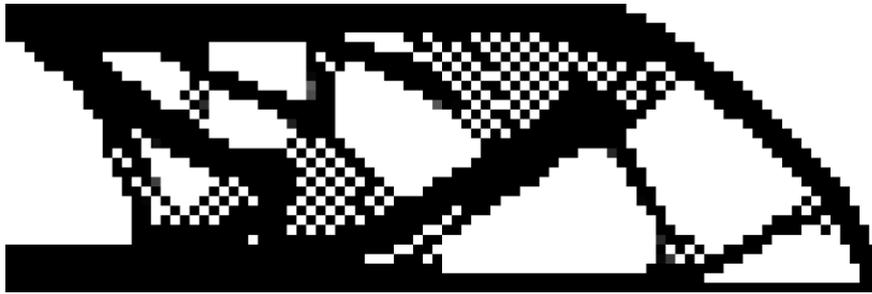
2) BENDSOE MP (1989) "OPTIMAL SHAPE DESIGN AS A MATERIAL DISTRIBUTION PROBLEM." STRUCTURAL AND MULTIDISCIPLINARY OPTIMIZATION 1(4):193-202

3) ZHOU M, ROZVANY G (1991) "THE COC ALGORITHM, PART II: TOPOLOGICAL, GEOMETRICAL AND GENERALIZED SHAPE OPTIMIZATION." COMP METH APPL MECH ENGRG 89:309-336

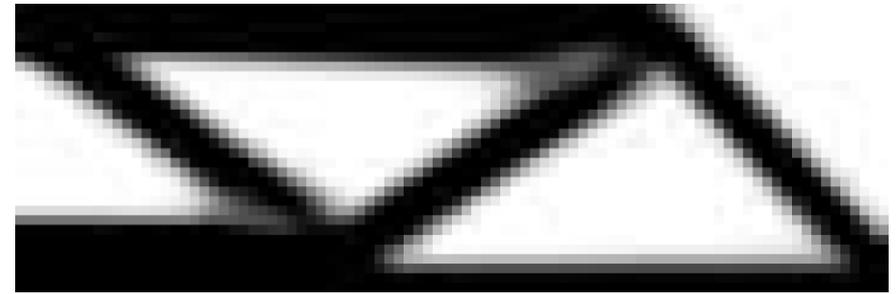
4) SIGMUND O (2007) "MORPHOLOGY-BASED BLACK AND WHITE FILTERS FOR TOPOLOGY OPTIMIZATION." STRUCTURAL AND MULTIDISCIPLINARY OPTIMIZATION, 33(4-5):401-424.

6) ADDITIVE MANUF. OF OPT. STRUCTS.

- FILTERS IN DENSITY-BASED FORMULATION:
 - SENSITIVITY FILTER (1-FIELD)
 - DENSITY FILTER (2-FIELDS) USED IN THIS WORK
 - PROJECTION FILTER (3-FIELDS)



UNFILTERED
(CHECKERBOARD)



FILTERED

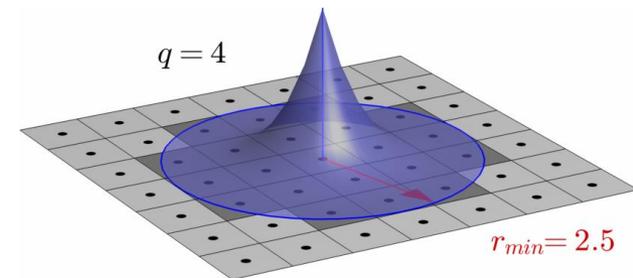
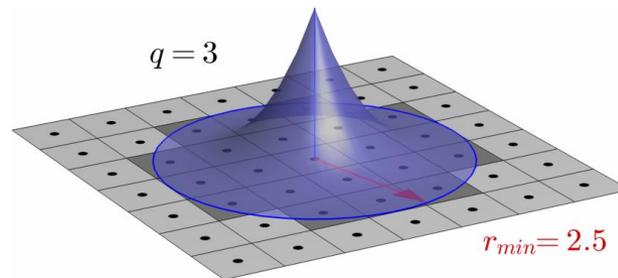
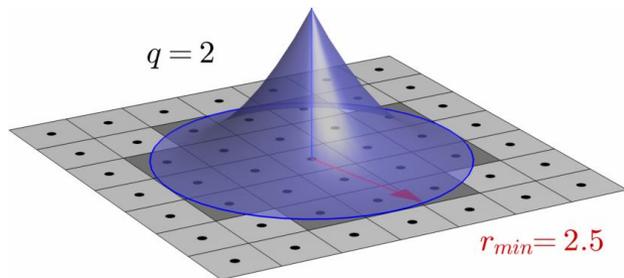
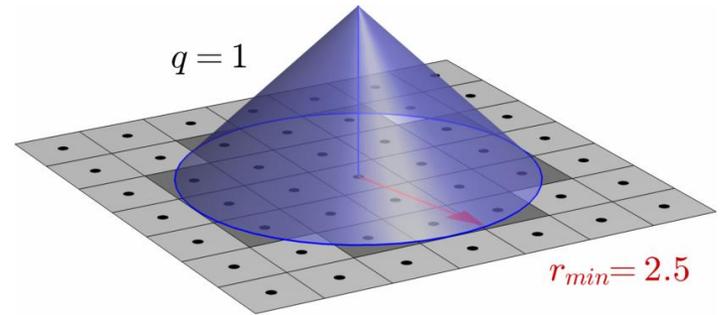
6) ADDITIVE MANUF. OF OPT. STRUCTS.

- CONVOLUTION (BLURRING) OF THE DENSITY FIELD

$$\bar{\rho} = \mathbf{H}\rho$$

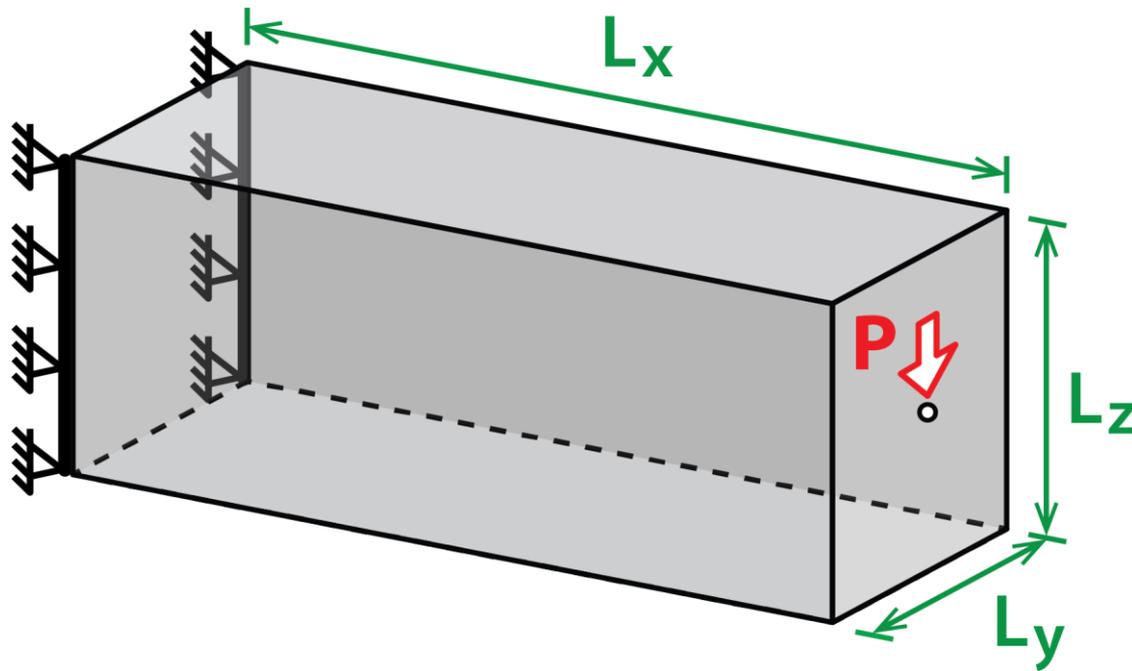
with
$$\mathbf{H}_{ij} = \frac{h(i, j) v_j}{\sum_k^{N_e} h(i, k) v_k}$$

$$h(i, j) = \begin{cases} [r_{min} - \text{dist}(i, j)]^q & \text{for } r_{min} - \text{dist}(i, j) > 0 \\ 0 & \text{otherwise} \end{cases}$$



6) ADDITIVE MANUF. OF OPT. STRUCTS.

- EDGE-SUPPORTED CANTILEVER BEAM
 $L_x=3$, $L_y=L_z=1$, $Q=1$, $R=5$ AND VOLFRAC=10%

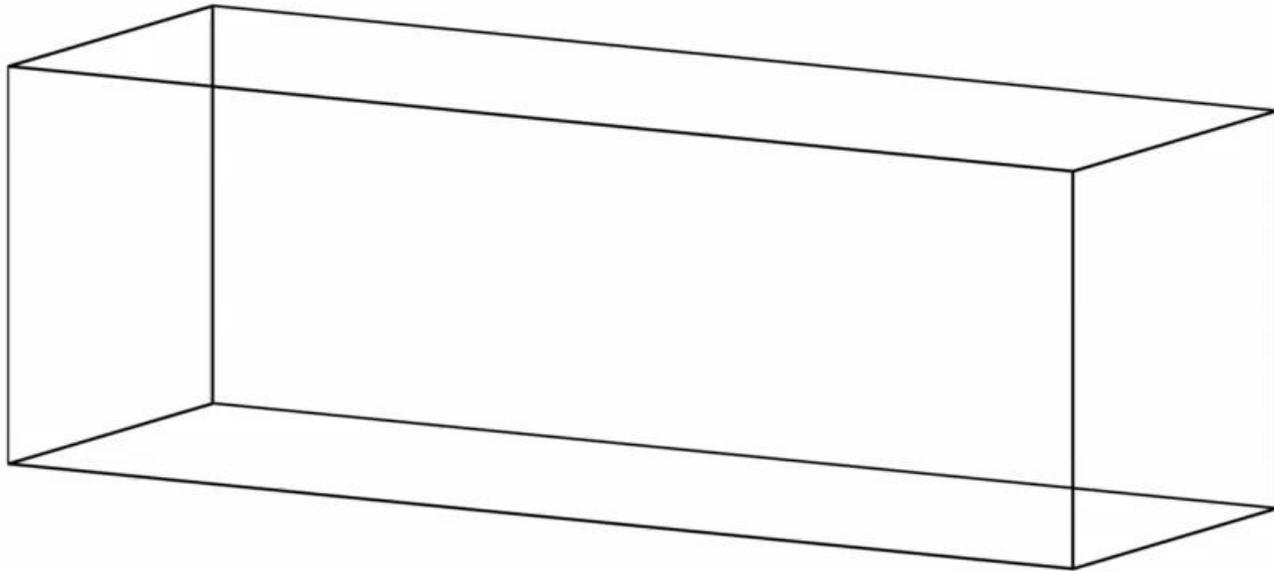


559,872 DVs FOR $\frac{1}{2}$
(1,119,744 TOTAL)

6) ADDITIVE MANUF. OF OPT. STRUCTS.

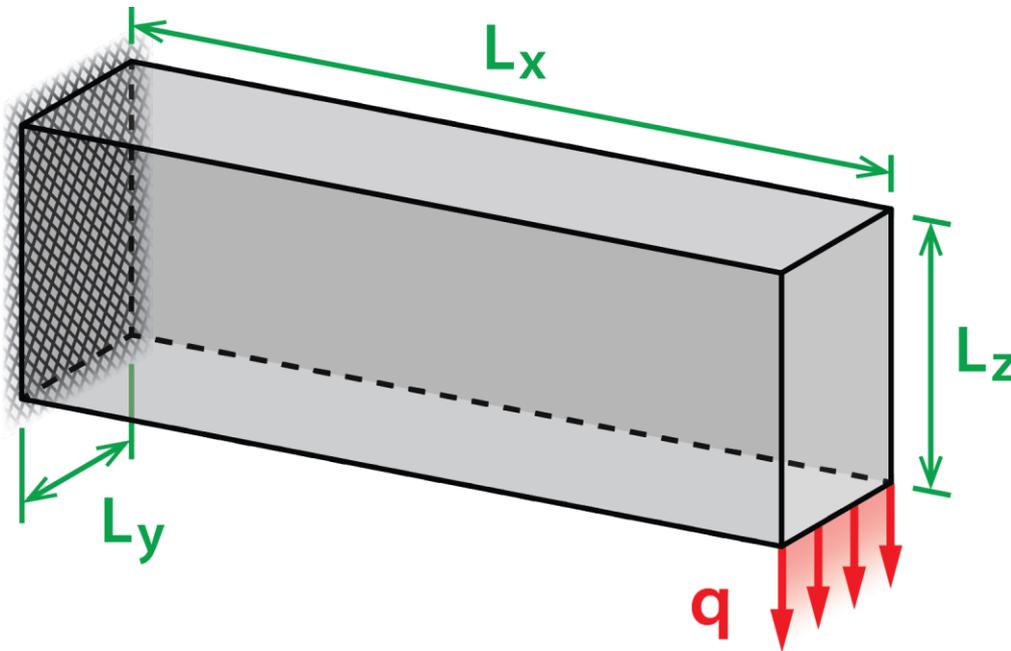
- EDGE-SUPPORTED CANTILEVER BEAM
 $L_x=3$, $L_y=L_z=1$, $Q=1$, $R=5$ AND VOLFRAC=10%

Iteration 000 Penal = 3.00



6) ADDITIVE MANUF. OF OPT. STRUCTS.

- EDGE-LOADED CANTILEVER BEAM
 $L_x=3$, $L_y=L_z=1$
VOLFRAC=10%, $R=6$, $Q=1$ AND $P=3$

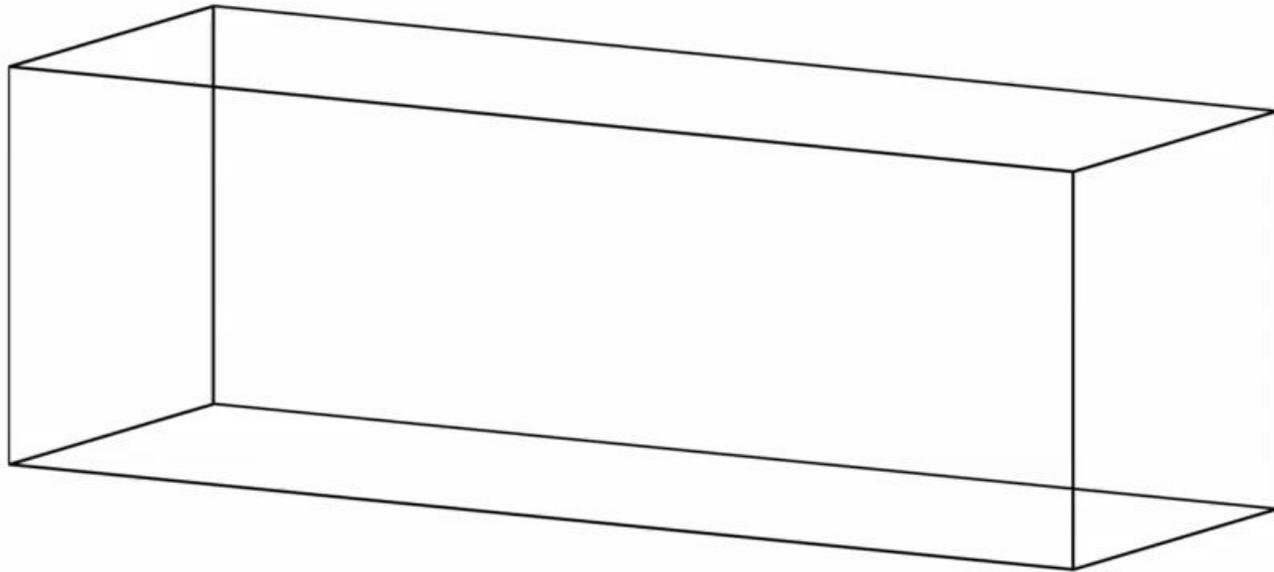


559,872 DVs FOR $\frac{1}{2}$
(1,119,744 TOTAL)

6) ADDITIVE MANUF. OF OPT. STRUCTS.

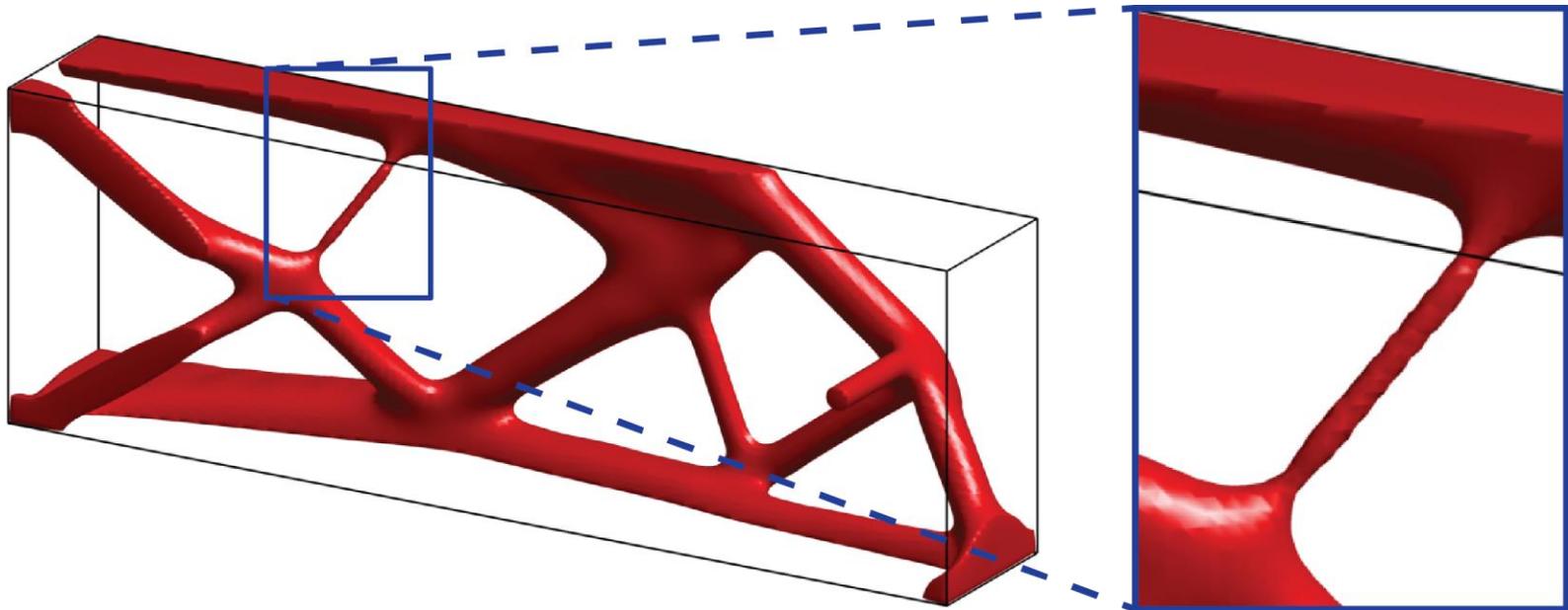
- EDGE-LOADED CANTILEVER BEAM
 $L_x=3$, $L_y=L_z=1$, $VOLFRAC=10\%$, $R=6$, $Q=1$ AND $P=3$

Iteration 000 Penal = 3.00



6) ADDITIVE MANUF. OF OPT. STRUCTS.

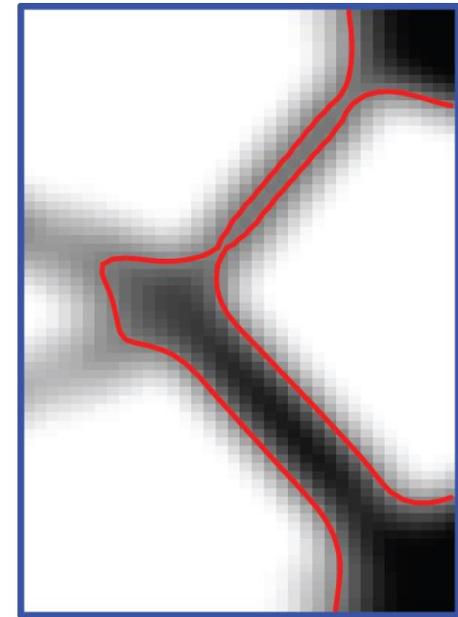
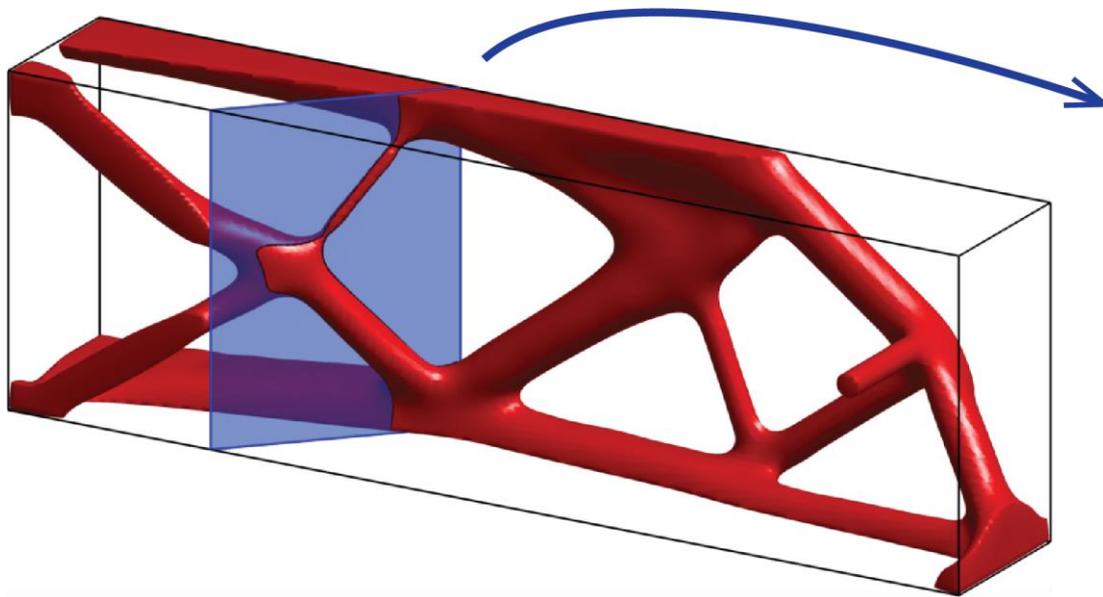
- EDGE-LOADED CANTILEVER
 $L_x=3$, $L_y=L_z=1$
VOLFRAC=10%, $R=6$, $Q=1$ AND $P=3$



559,872 DVs FOR $\frac{1}{2}$
(1,119,744 TOTAL)

6) ADDITIVE MANUF. OF OPT. STRUCTS.

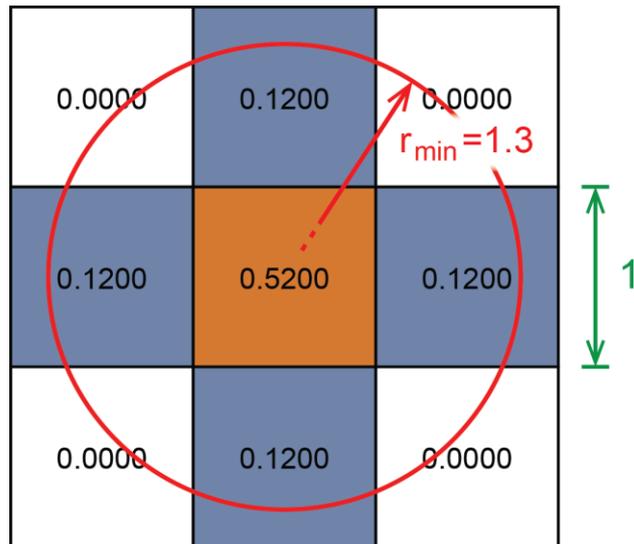
- EDGE-LOADED CANTILEVER
 $L_x=3$, $L_y=L_z=1$
VOLFRAC=10%, $R=6$, $Q=1$ AND $P=3$



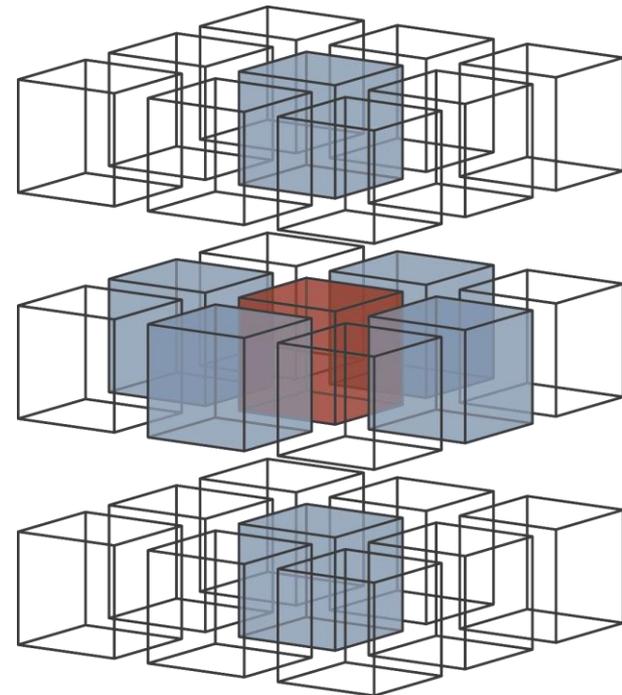
559,872 DVs FOR $\frac{1}{2}$
(1,119,744 TOTAL)

6) ADDITIVE MANUF. OF OPT. STRUCTS.

- FILTER'S WEIGHTS FOR A REGULAR MESH
 $R_{MIN}=1.3$, $Q=1$ AND ELEM SIZE IS $L=1$



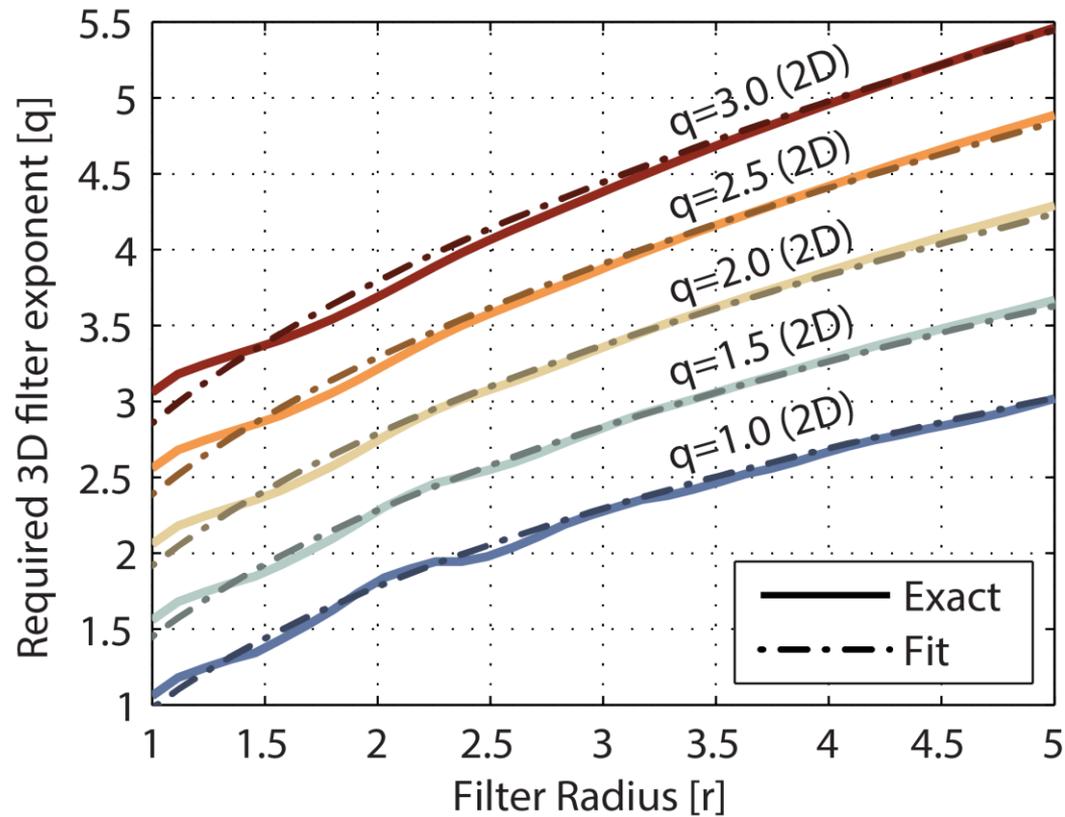
TWO-DIMENSIONS



THREE-DIMENSIONS
($H_{ii} = 0.4194$)

6) ADDITIVE MANUF. OF OPT. STRUCTS.

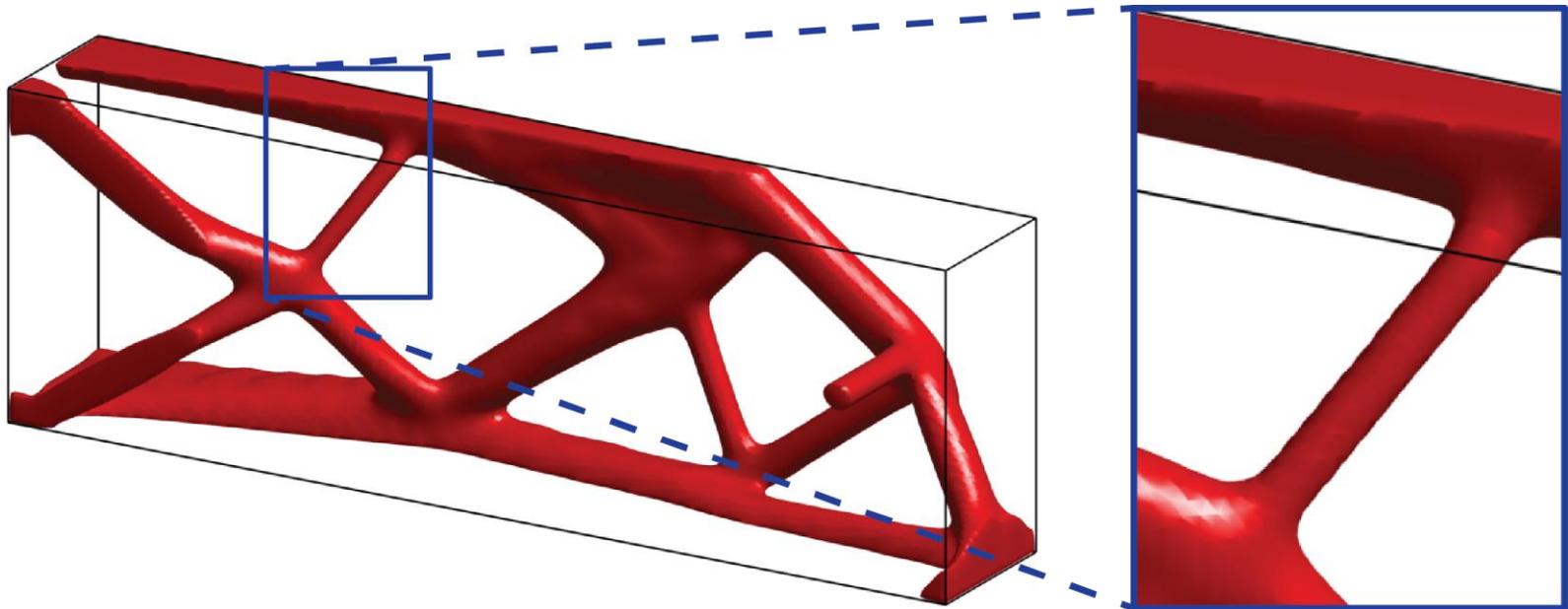
IDEA: WHAT EXPONENT Q MAKES $H_{ii}^{(2D)} = H_{ii}^{(3D)}$?



$$q^{(3D)} = \log(r_{min}) + \frac{17}{20}q^{(2D)} + \frac{4}{57}q^{(2D)}r_{min} + \frac{4}{87}r_{min}$$

6) ADDITIVE MANUF. OF OPT. STRUCTS.

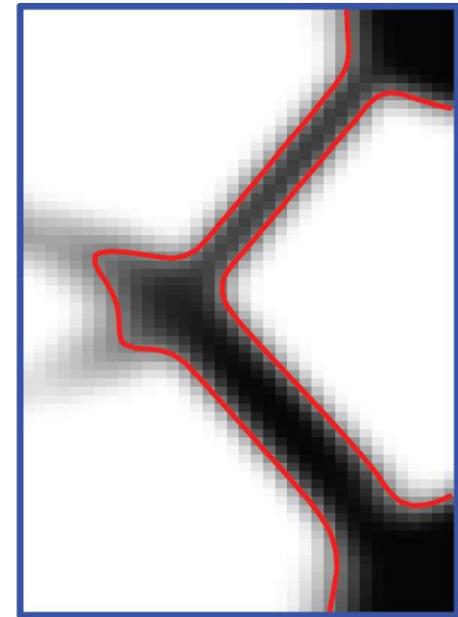
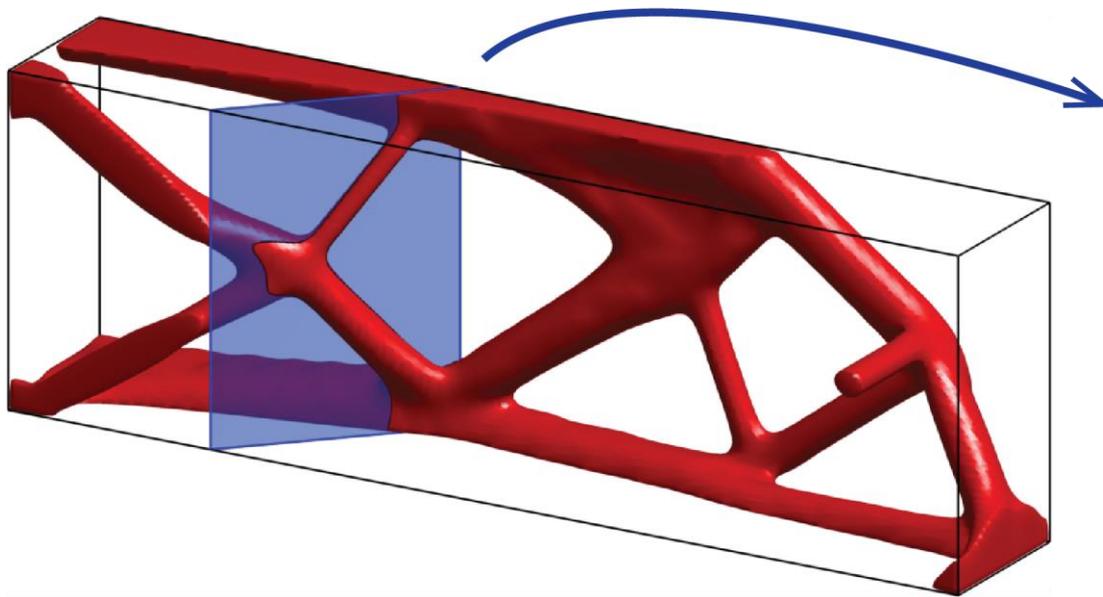
- EDGE-LOADED CANTILEVER
 $L_x=3$, $L_y=L_z=1$
VOLFRAC=10%, $R=6$, $Q=3$ AND $P=3$



559,872 DVs FOR $\frac{1}{2}$
(1,119,744 TOTAL)

6) ADDITIVE MANUF. OF OPT. STRUCTS.

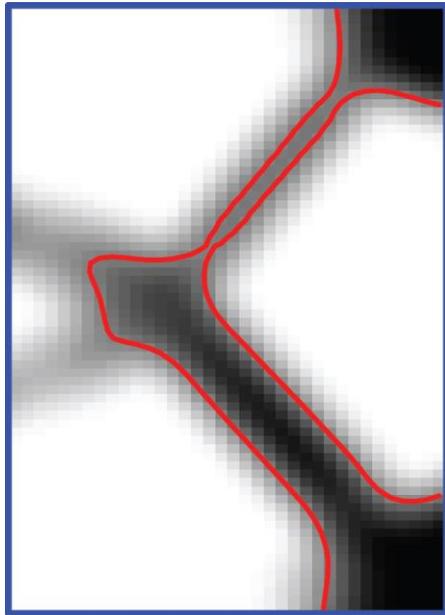
- EDGE-LOADED CANTILEVER
 $L_x=3$, $L_y=L_z=1$
VOLFRAC=10%, $R=6$, $Q=3$ AND $P=3$



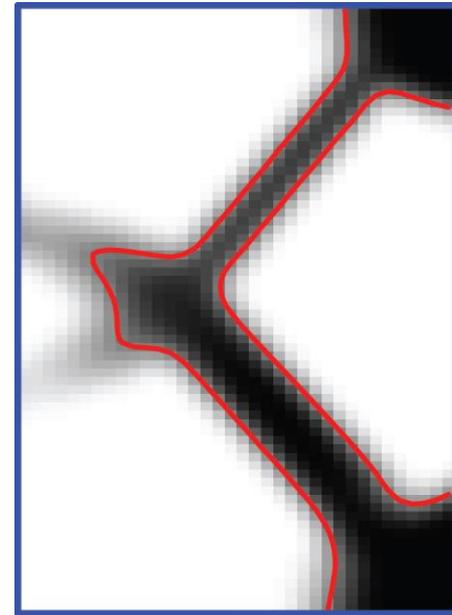
559,872 DVs FOR $\frac{1}{2}$
(1,119,744 TOTAL)

6) ADDITIVE MANUF. OF OPT. STRUCTS.

- EDGE-LOADED CANTILEVER
DENSITY FILTER: $R=6$



LINEAR DENSITY FILTER

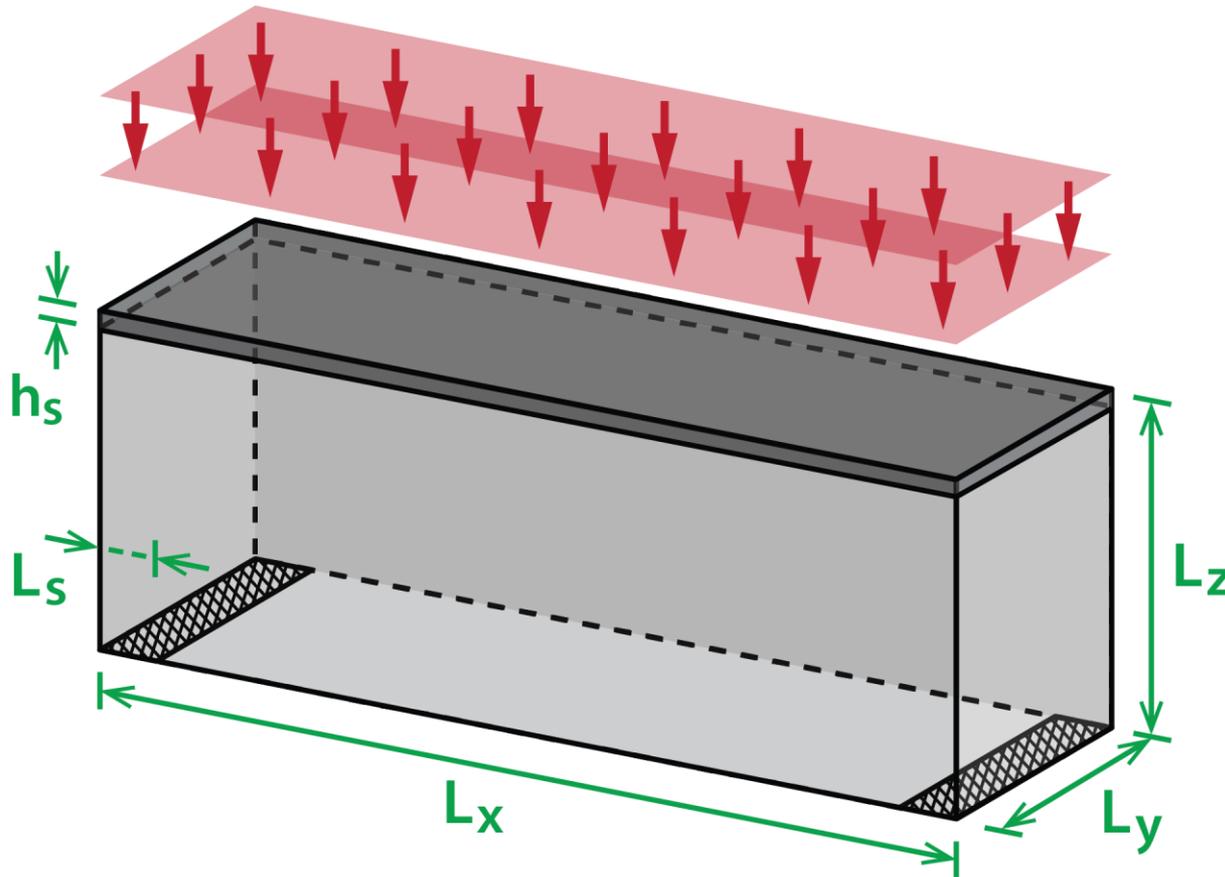


CUBIC DENSITY FILTER

6) ADDITIVE MANUF. OF OPT. STRUCTS.

- BRIDGE PROBLEM

$L_x = XXX$, $L_y = L_z = YYY$, $Q = ZZZ$, $R = 5$ AND
 $VOLFRAC = 10\%$

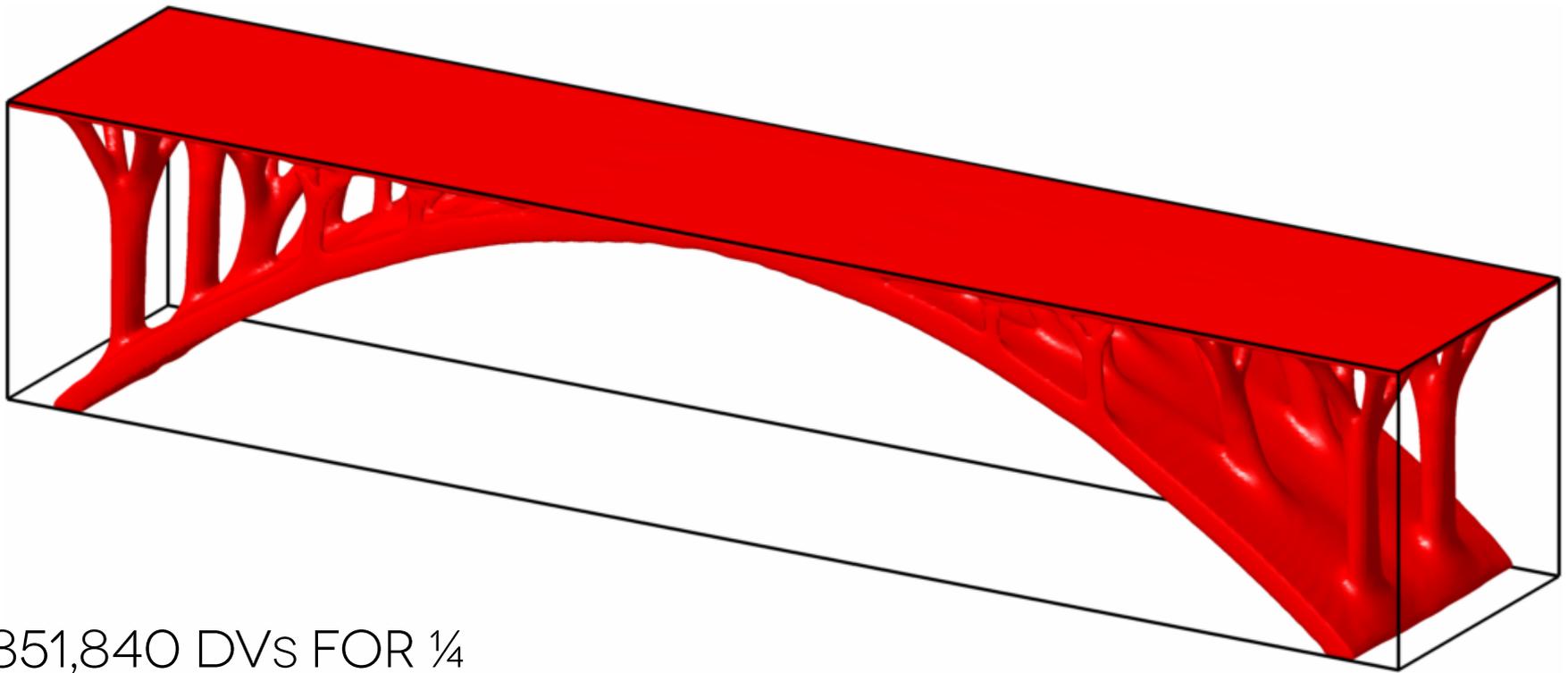


6) ADDITIVE MANUF. OF OPT. STRUCTS.

- BRIDGE PROBLEM

$L_x=25$, $L_y=L_z=5$

$VOLFRAC=10\%$, $R=5$, $Q=3$ AND $P=3$



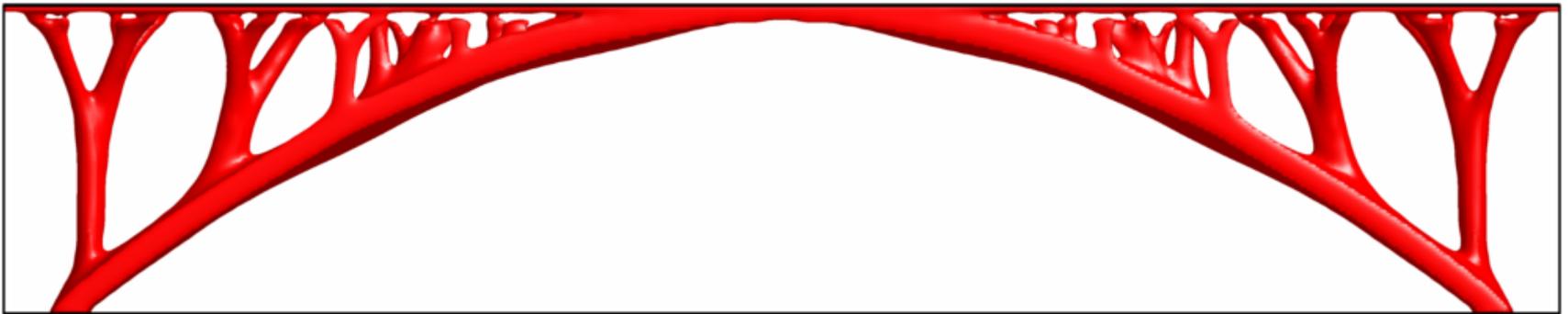
851,840 DVs FOR $\frac{1}{4}$
(3,407,360 TOTAL)

6) ADDITIVE MANUF. OF OPT. STRUCTS.

- BRIDGE PROBLEM

$L_x=25$, $L_y=L_z=5$

$VOLFRAC=10\%$, $R=5$, $Q=3$ AND $P=3$



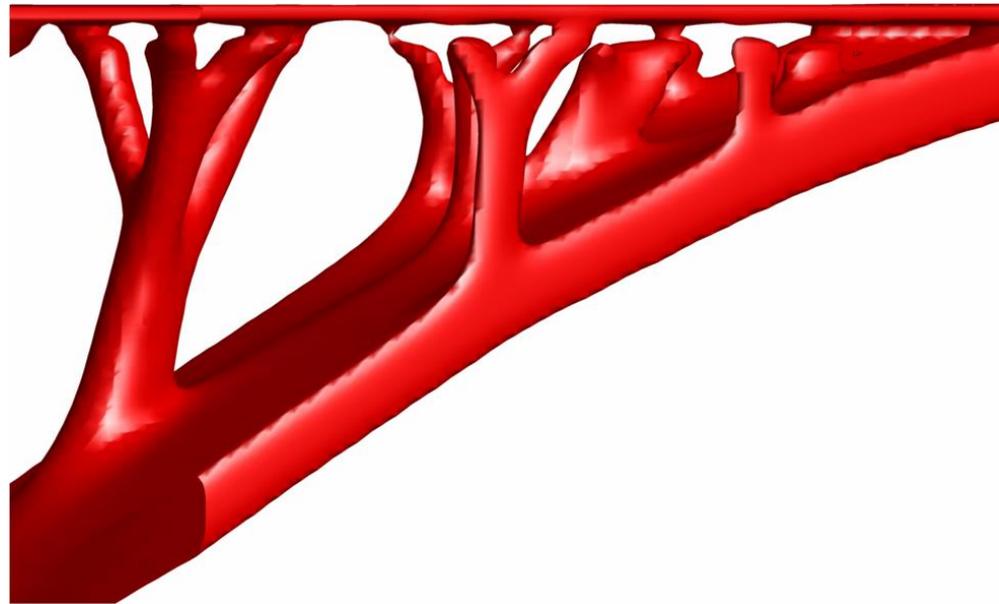
851,840 DVs FOR $\frac{1}{4}$
(3,407,360 TOTAL)

6) ADDITIVE MANUF. OF OPT. STRUCTS.

- BRIDGE PROBLEM

$L_x=25$, $L_y=L_z=5$

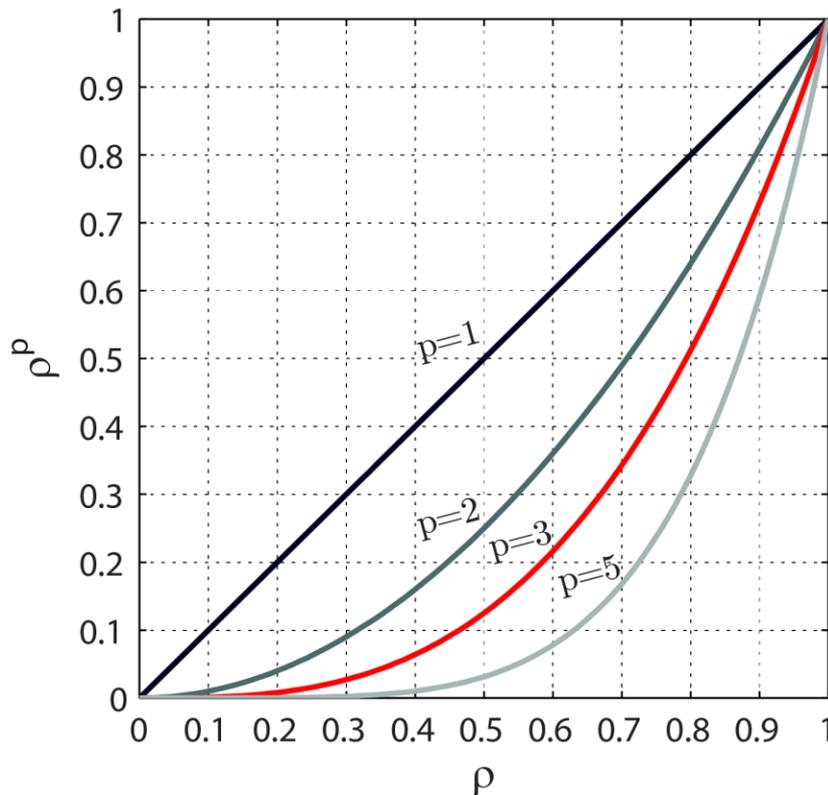
$VOLFRAC=10\%$, $R=5$, $Q=3$ AND $P=3$



851,840 DVs FOR $\frac{1}{4}$
(3,407,360 TOTAL)

6) ADDITIVE MANUF. OF OPT. STRUCTS.

- SIMP'S POWER-LAW:



SIMP:

$$E_i(\rho_i) = \rho_i^p E_0$$

$$0 \lesssim \rho_{min} \leq \rho_j \leq 1$$

MODIFIED SIMP:

$$E_k(\rho_k) = E_{min} + \rho_k^p (E_0 - E_{min})$$

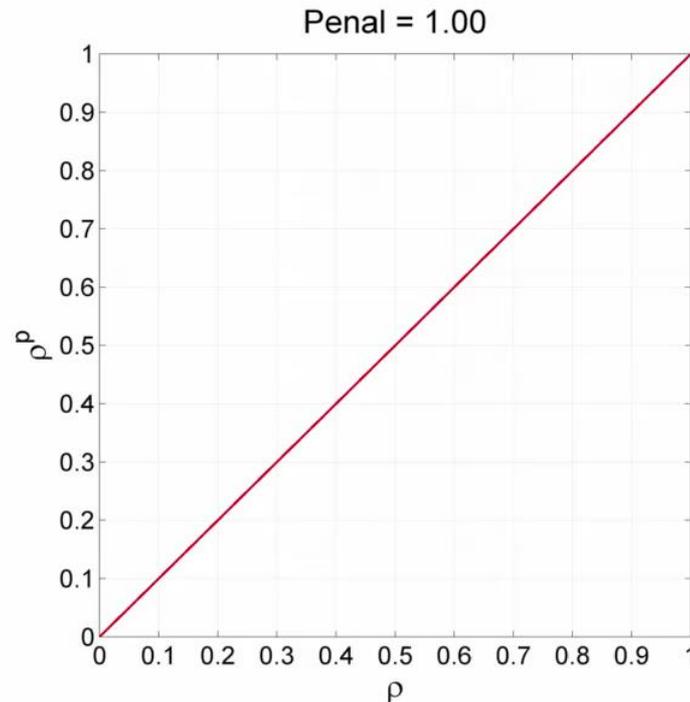
$$0 \leq \rho_j \leq 1$$

2) BENDSOE MP (1989) "OPTIMAL SHAPE DESIGN AS A MATERIAL DISTRIBUTION PROBLEM." STRUCTURAL AND MULTIDISCIPLINARY OPTIMIZATION 1(4):193-202

3) ZHOU M, ROZVANY G (1991) "THE COC ALGORITHM, PART II: TOPOLOGICAL, GEOMETRICAL AND GENERALIZED SHAPE OPTIMIZATION." COMP METH APPL MECH ENGRG 89:309-336

6) ADDITIVE MANUF. OF OPT. STRUCTS.

- CONTINUATION OF “P” PARAMETER



ALLAIRE G, FRANCFORT G (1993) "A NUMERICAL ALGORITHM FOR TOPOLOGY AND SHAPE OPTIMIZATION." IN TOPOLOGY DESIGN OF STRUCTURES, SPRINGER

ALLAIRE G, KOHN R (1993) "TOPOLOGY OPTIMIZATION AND OPTIMAL SHAPE DESIGN USING HOMOGENIZATION." IN TOPOLOGY DESIGN OF STRUCTURES, SPRINGER

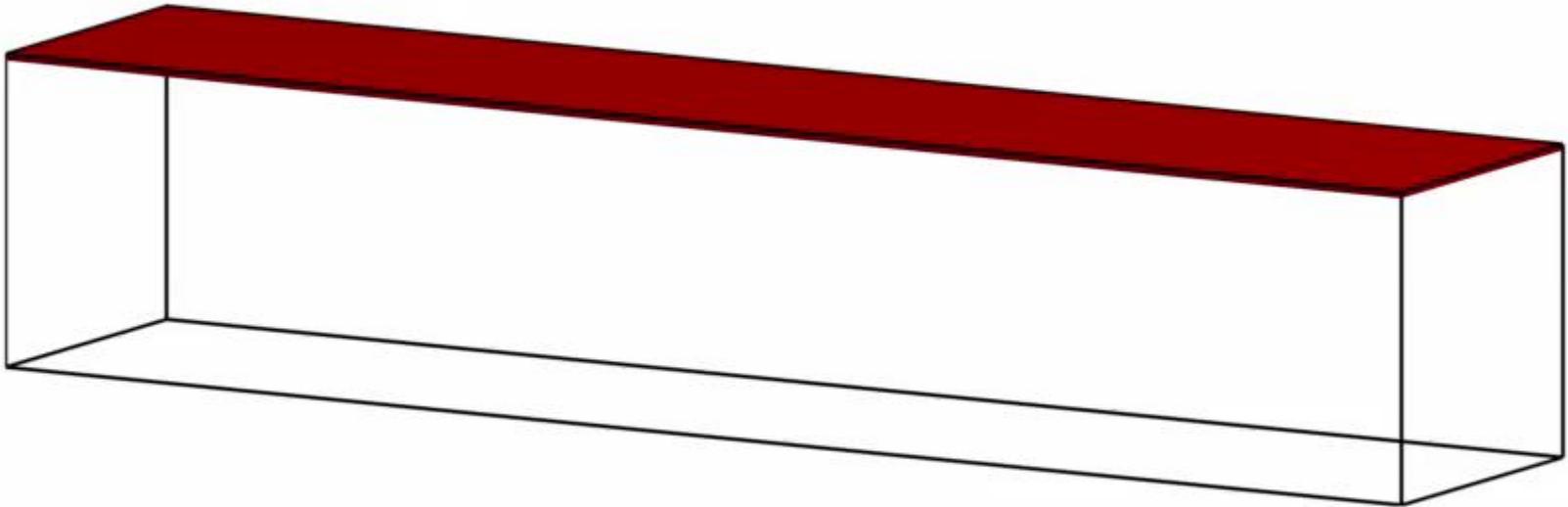
SIGMUND O, PETERSSON J (1998) "NUMERICAL INSTABILITIES IN TOPOLOGY OPTIMIZATION" STRUCTURAL OPTIMIZATION, 16(1):68–75

6) ADDITIVE MANUF. OF OPT. STRUCTS.

- BRIDGE PROBLEM

$L_x=25$, $L_y=L_z=5$, $VOLFRAC=10\%$, $R=5$, $Q=3$ AND $P=[CONT]$

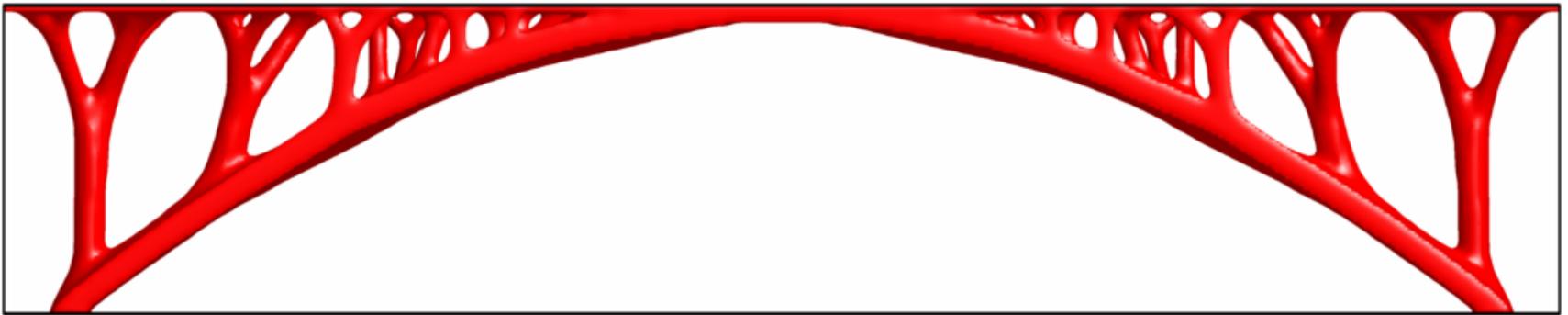
Iteration 000 Penal = 2.00



6) ADDITIVE MANUF. OF OPT. STRUCTS.

- BRIDGE PROBLEM

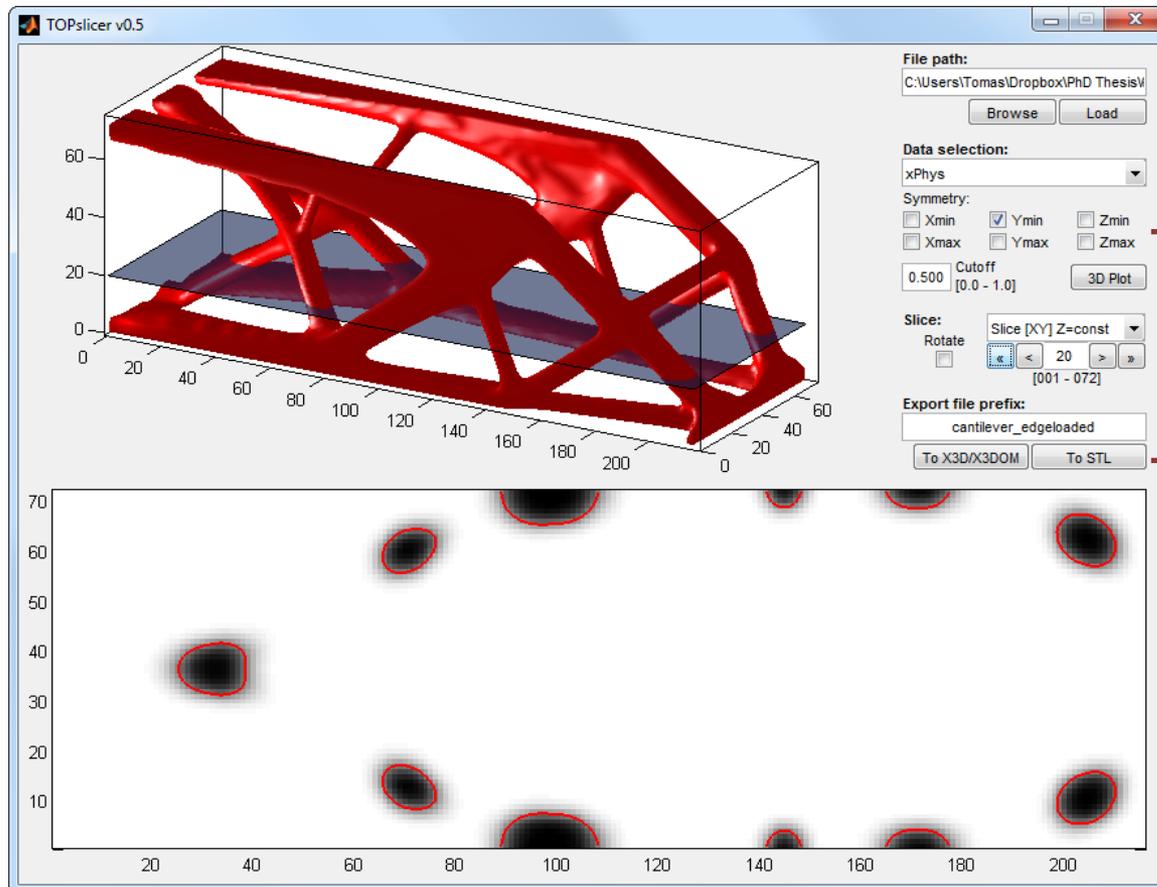
$L_x=25$, $L_y=L_z=5$, $VOLFRAC=10\%$, $R=5$, $Q=3$ AND $P=[CONT]$



851,840 DVs FOR $\frac{1}{4}$
(3,407,360 TOTAL)

6) ADDITIVE MANUF. OF OPT. STRUCTS.

- TOPSLICER: AN INSPECTOR/EXPORTER OF 3D DENSITY-BASED TOPOLOGIES

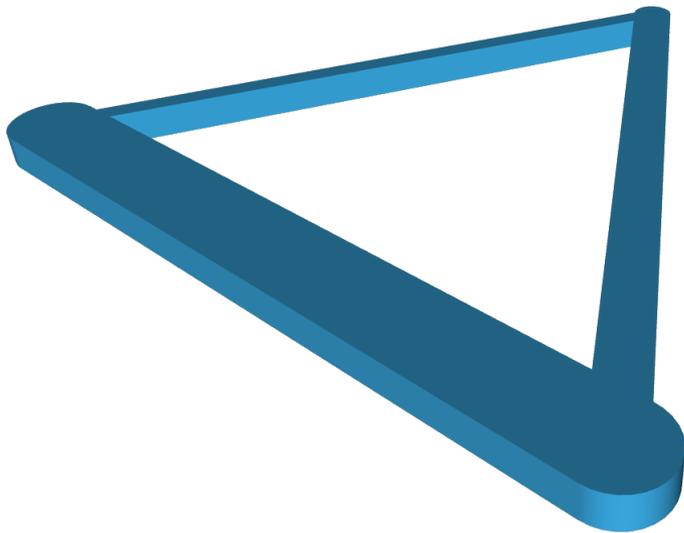


RESTORE SYMMETRY

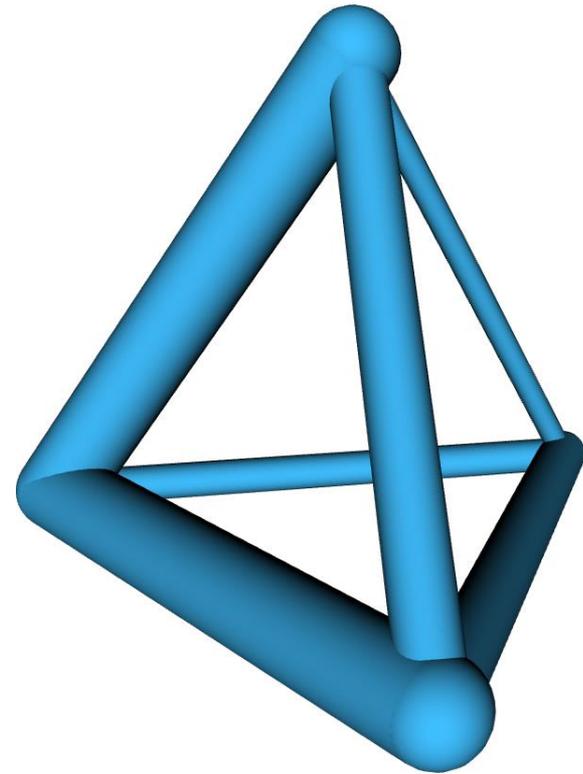
EXPORT TO X3D OR STL

6) ADDITIVE MANUF. OF OPT. STRUCTS.

- MANUFACTURING OF GROUND STRUCTURES



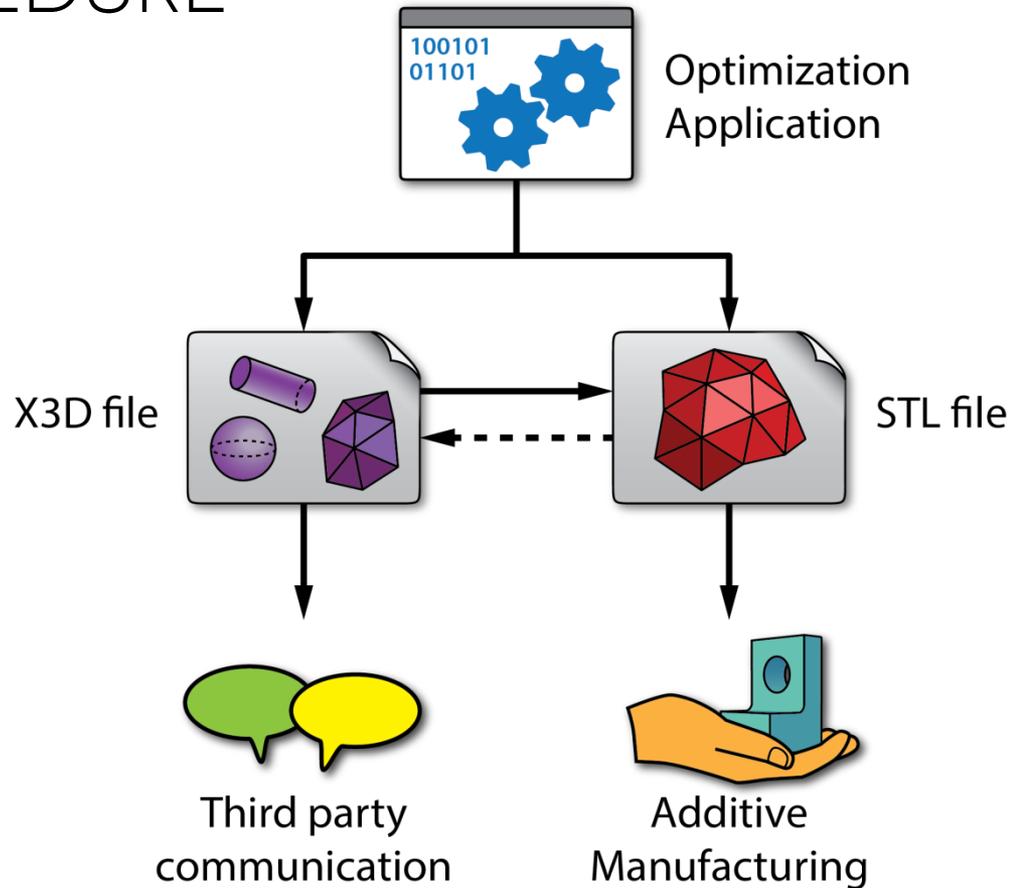
2D GROUND STRUCTURES



3D GROUND STRUCTURES

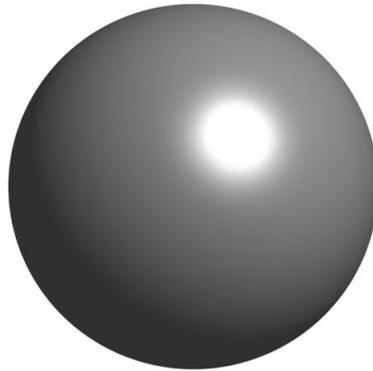
6) ADDITIVE MANUF. OF OPT. STRUCTS.

- PROCEDURE

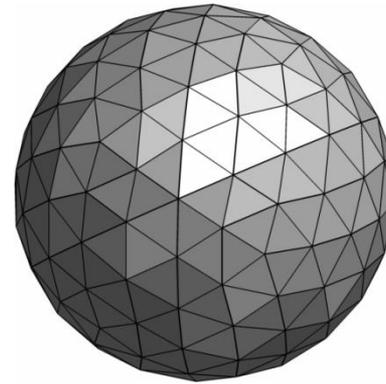
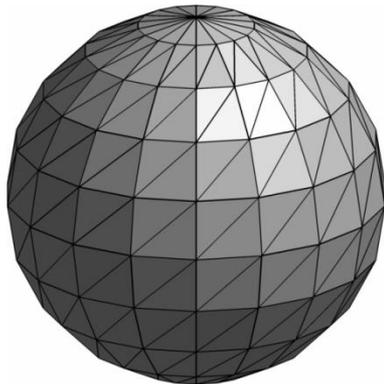


6) ADDITIVE MANUF. OF OPT. STRUCTS.

- X3D SUPPORTS IMPLICIT 3D PRIMITIVES

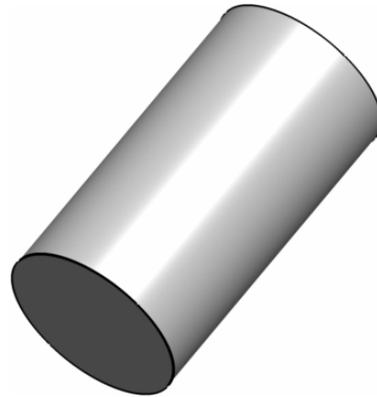


- STL ONLY SUPPORTS DISCRETIZED (TESSELLATED) SOLIDS

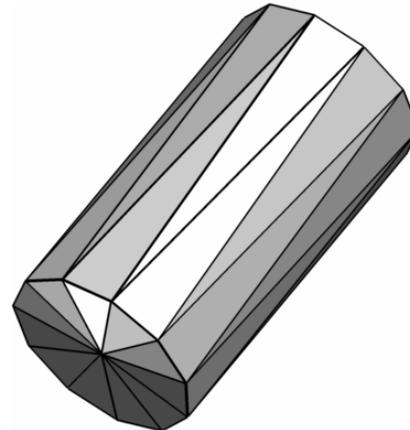
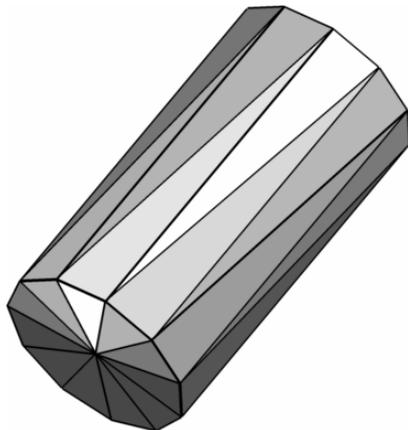


6) ADDITIVE MANUF. OF OPT. STRUCTS.

- X3D SUPPORTS IMPLICIT 3D PRIMITIVES

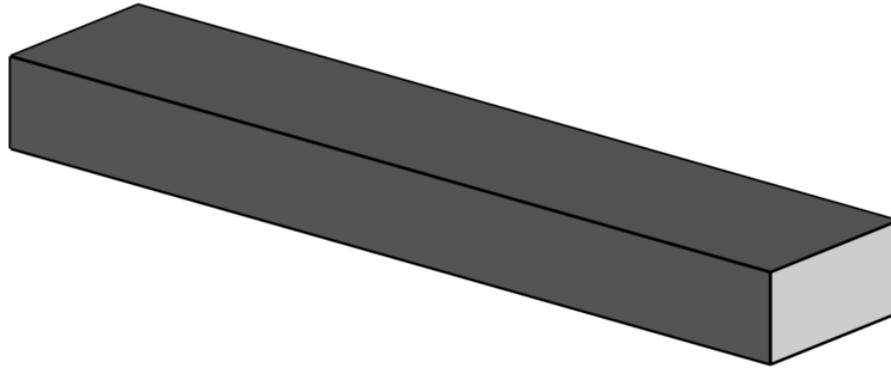


- STL ONLY SUPPORTS DISCRETIZED (TESSELLATED) SOLIDS

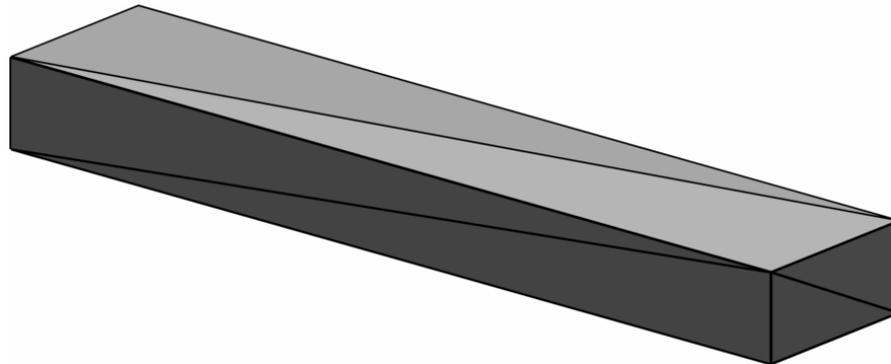


6) ADDITIVE MANUF. OF OPT. STRUCTS.

- X3D SUPPORTS IMPLICIT 3D PRIMITIVES

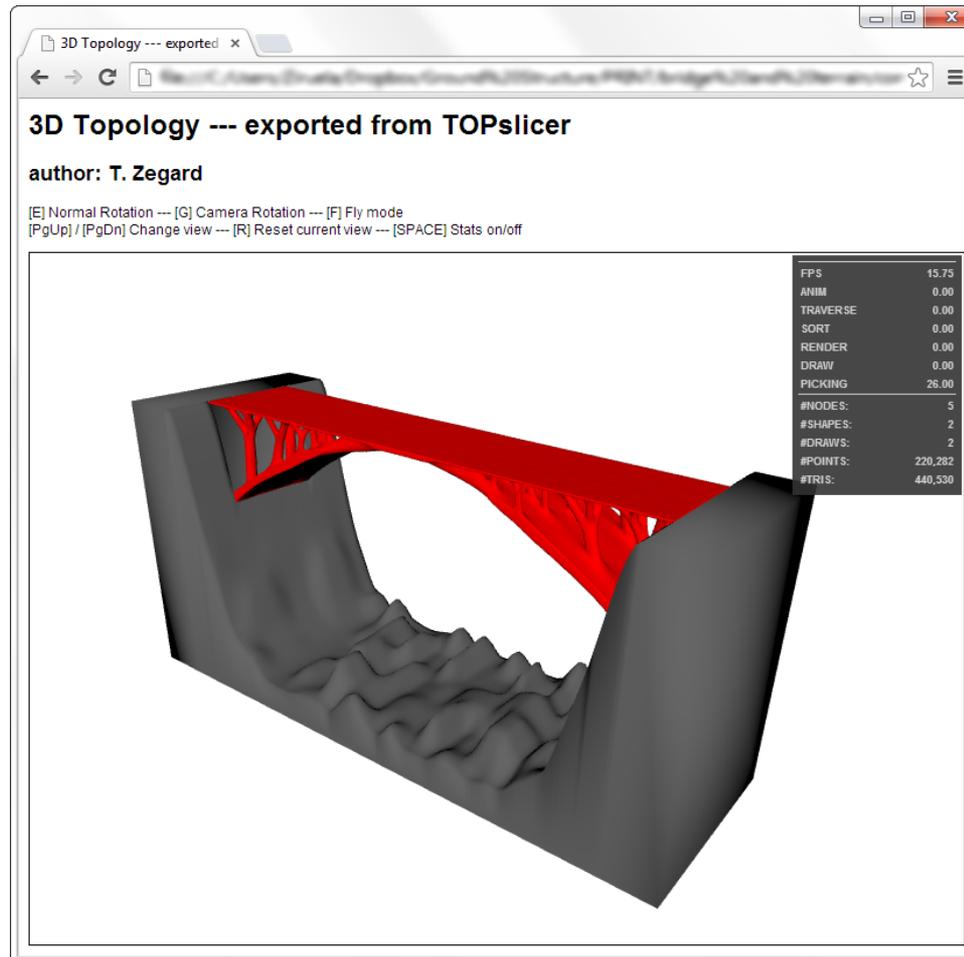


- STL ONLY SUPPORTS DISCRETIZED (TESSELLATED) SOLIDS



6) ADDITIVE MANUF. OF OPT. STRUCTS.

- **X3D**: ROYALTY-FREE FORMAT FOR REPRESENTING 3D COMPUTER GRAPHICS. MANAGED BY THE WEB3D CONSORTIUM.

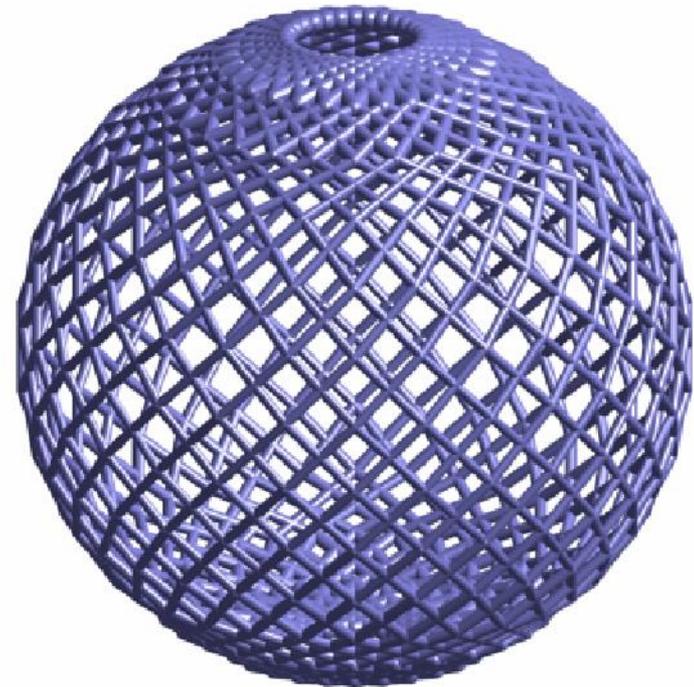
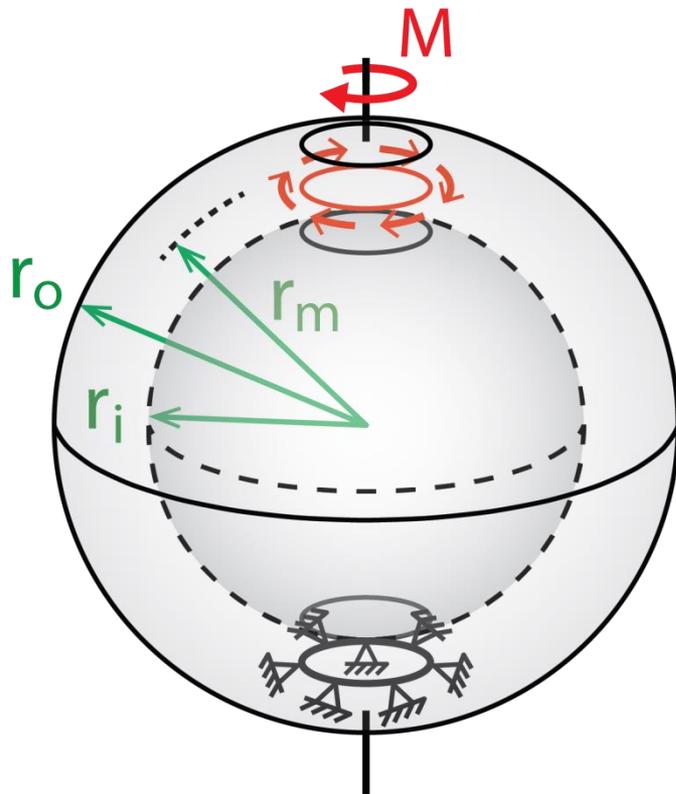


6) ADDITIVE MANUF. OF OPT. STRUCTS.

- SHOW AND TELL:
- COLOR CODE
 - WHITE — 3D GROUND STRUCTURES
 - BLUE — 2D GROUND STRUCTURES
 - RED — 3D DENSITY METHOD
 - BLACK — APPLICATION-ORIENTED
- MANUFACTURED USING:
 - FDM: FUSED DEPOSITION MODELING
 - SLS: SELECTIVE LASER SINTERING

6) ADDITIVE MANUF. OF OPT. STRUCTS.

- SHOW AND TELL: **TORSION BALL**



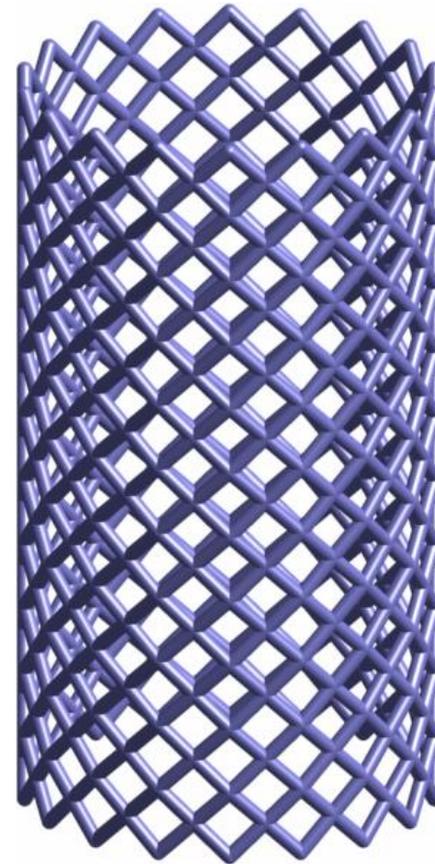
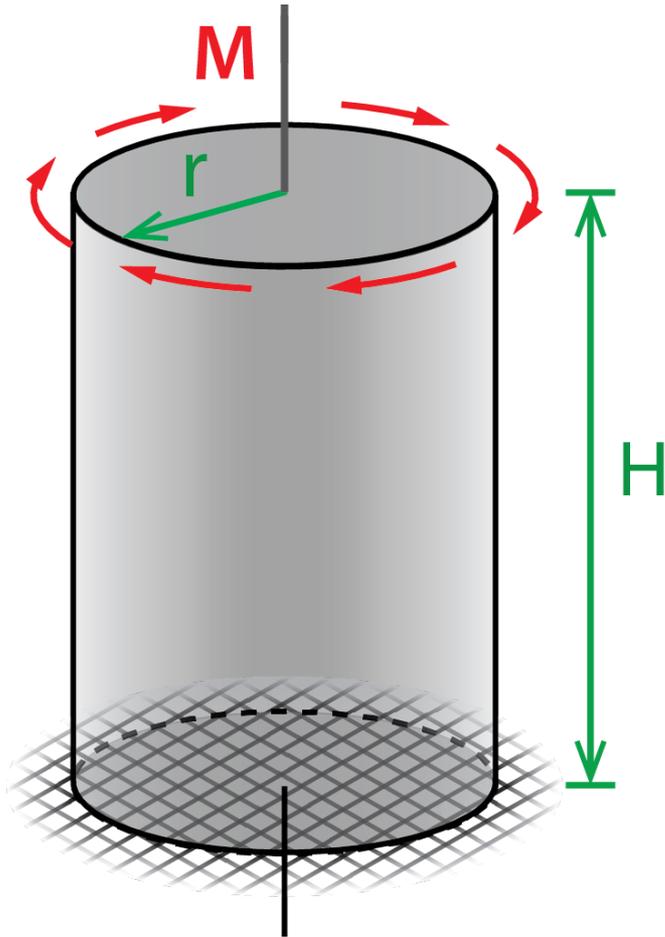
6) ADDITIVE MANUF. OF OPT. STRUCTS.

- SHOW AND TELL: **TORSION BALL**



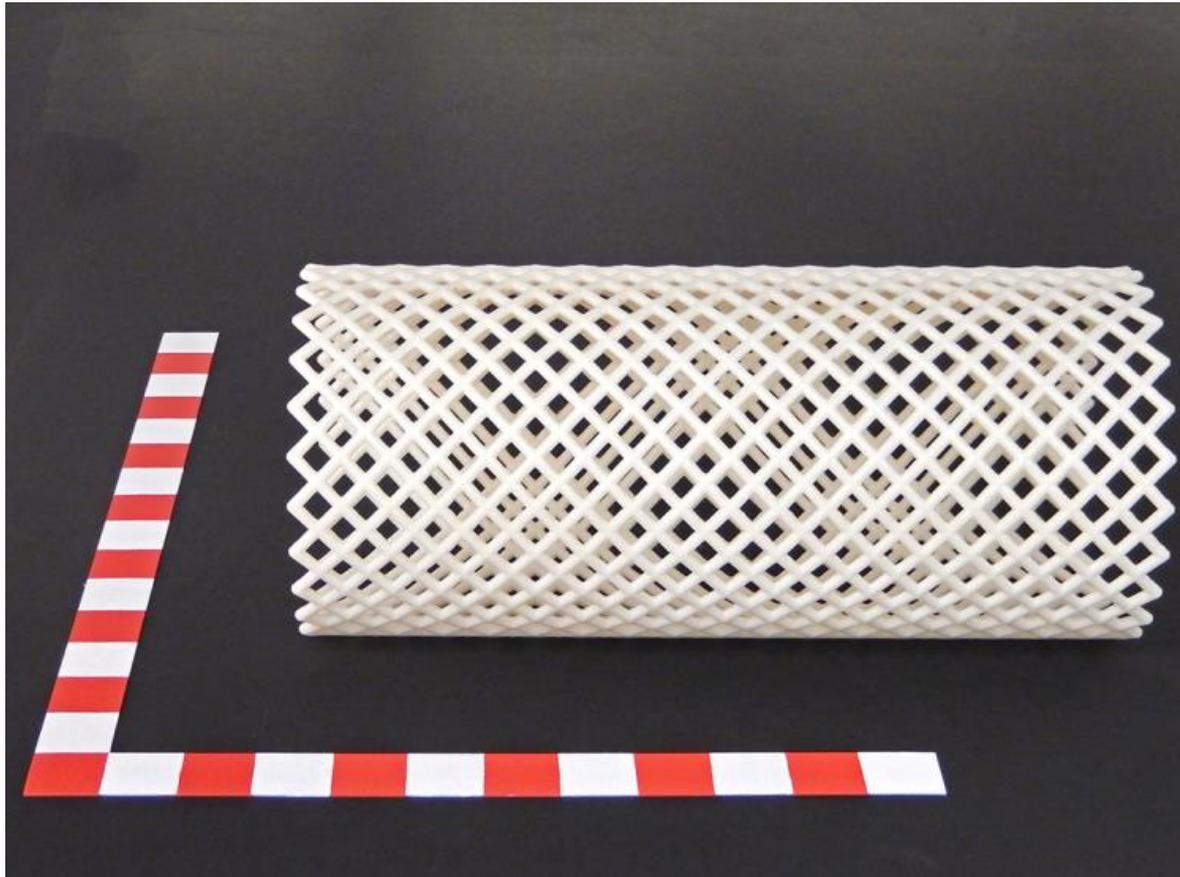
6) ADDITIVE MANUF. OF OPT. STRUCTS.

- SHOW AND TELL: **TORSION CYLINDER**



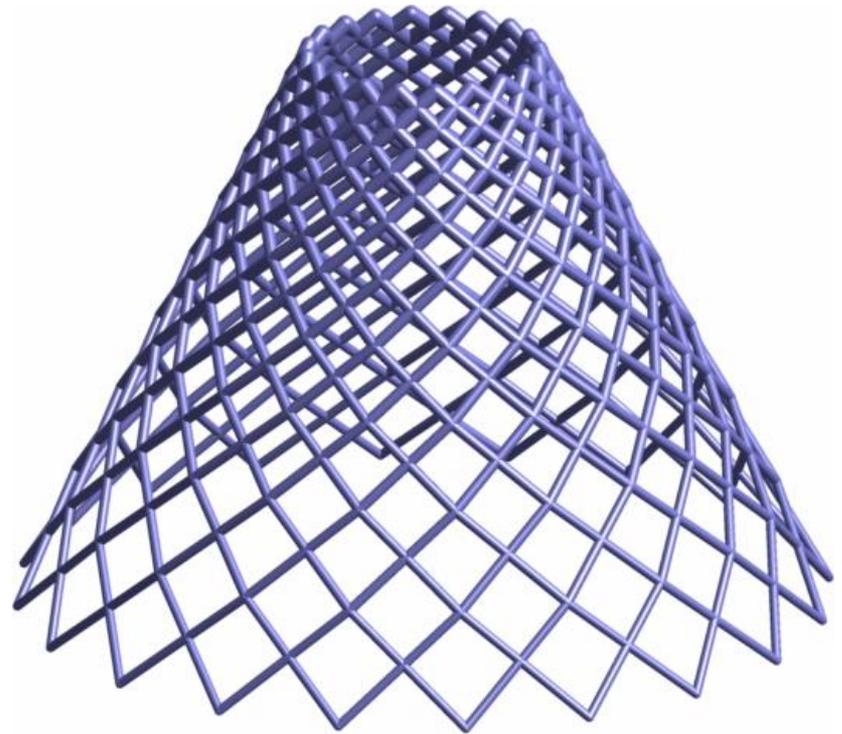
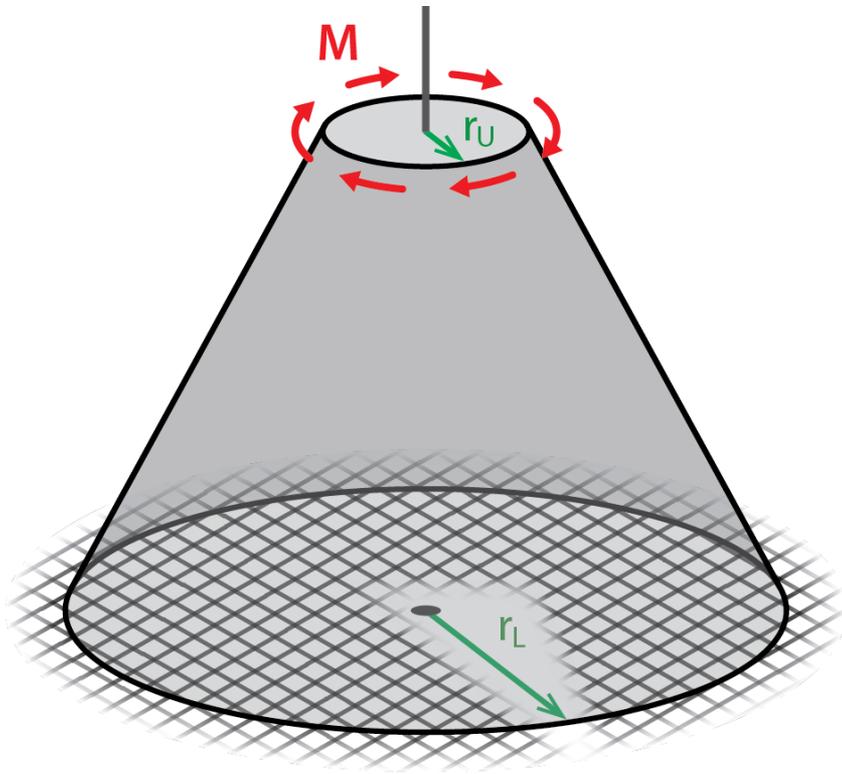
6) ADDITIVE MANUF. OF OPT. STRUCTS.

- SHOW AND TELL: TORSION CYLINDER



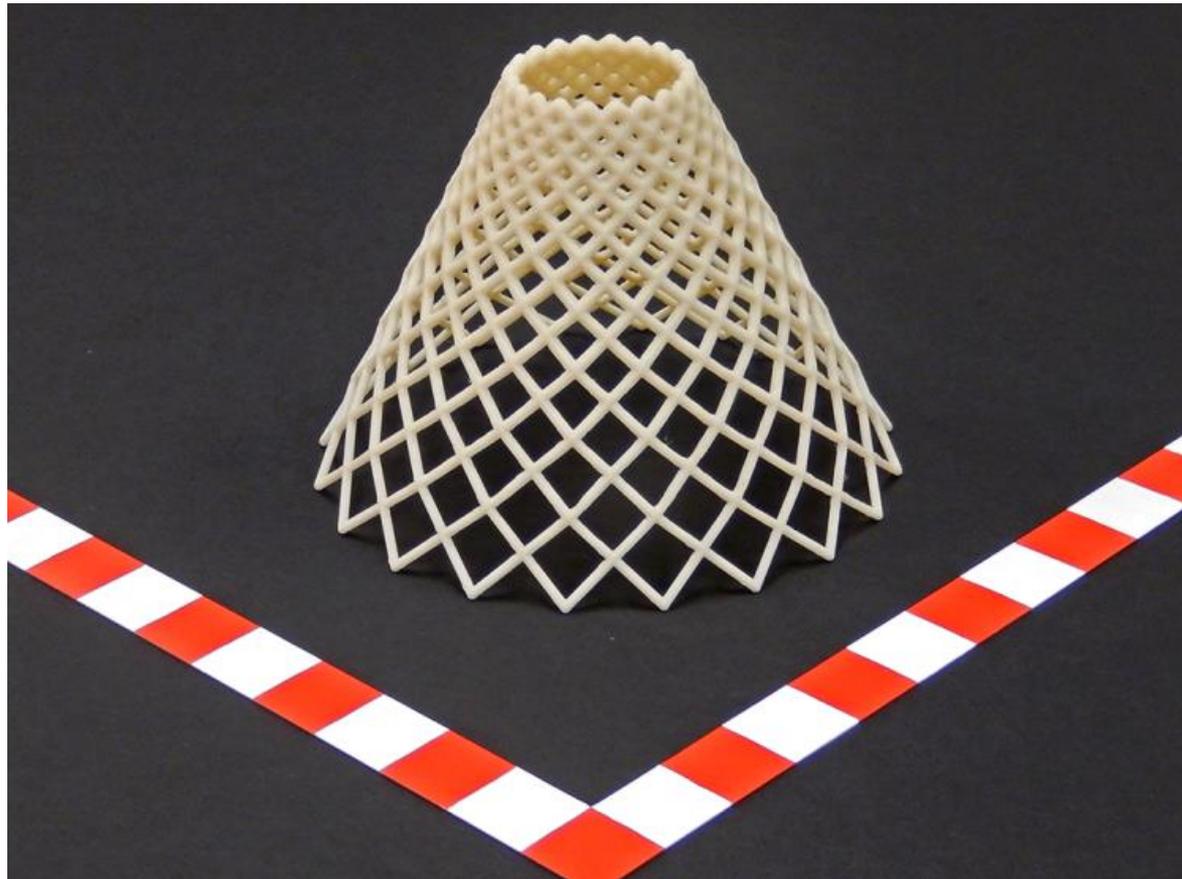
6) ADDITIVE MANUF. OF OPT. STRUCTS.

- SHOW AND TELL: **TORSION CONE**



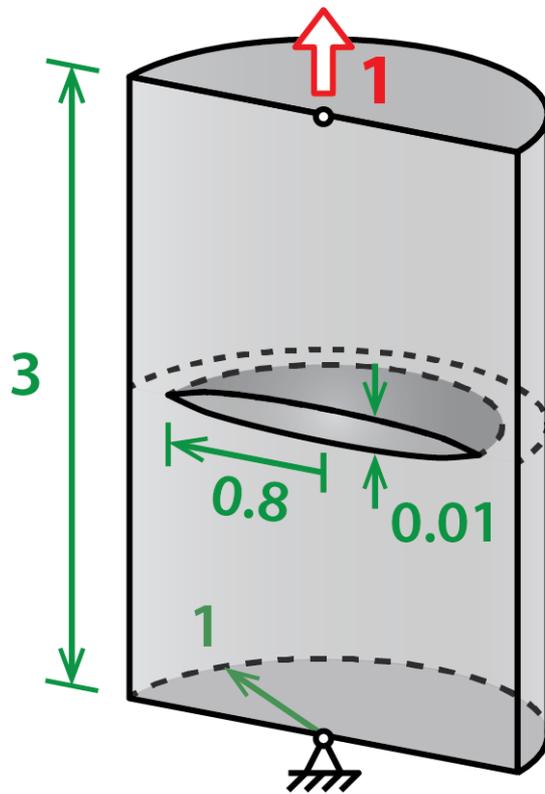
6) ADDITIVE MANUF. OF OPT. STRUCTS.

- SHOW AND TELL: **TORSION CONE**

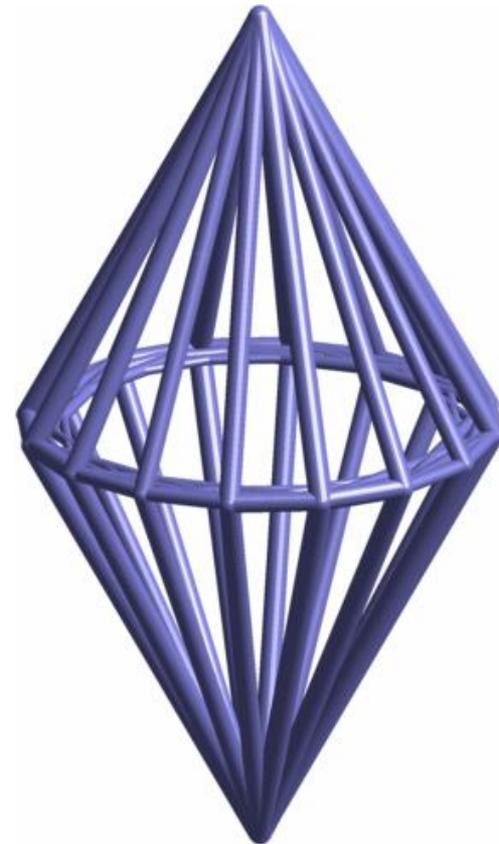


6) ADDITIVE MANUF. OF OPT. STRUCTS.

- SHOW AND TELL: **DIAMOND**

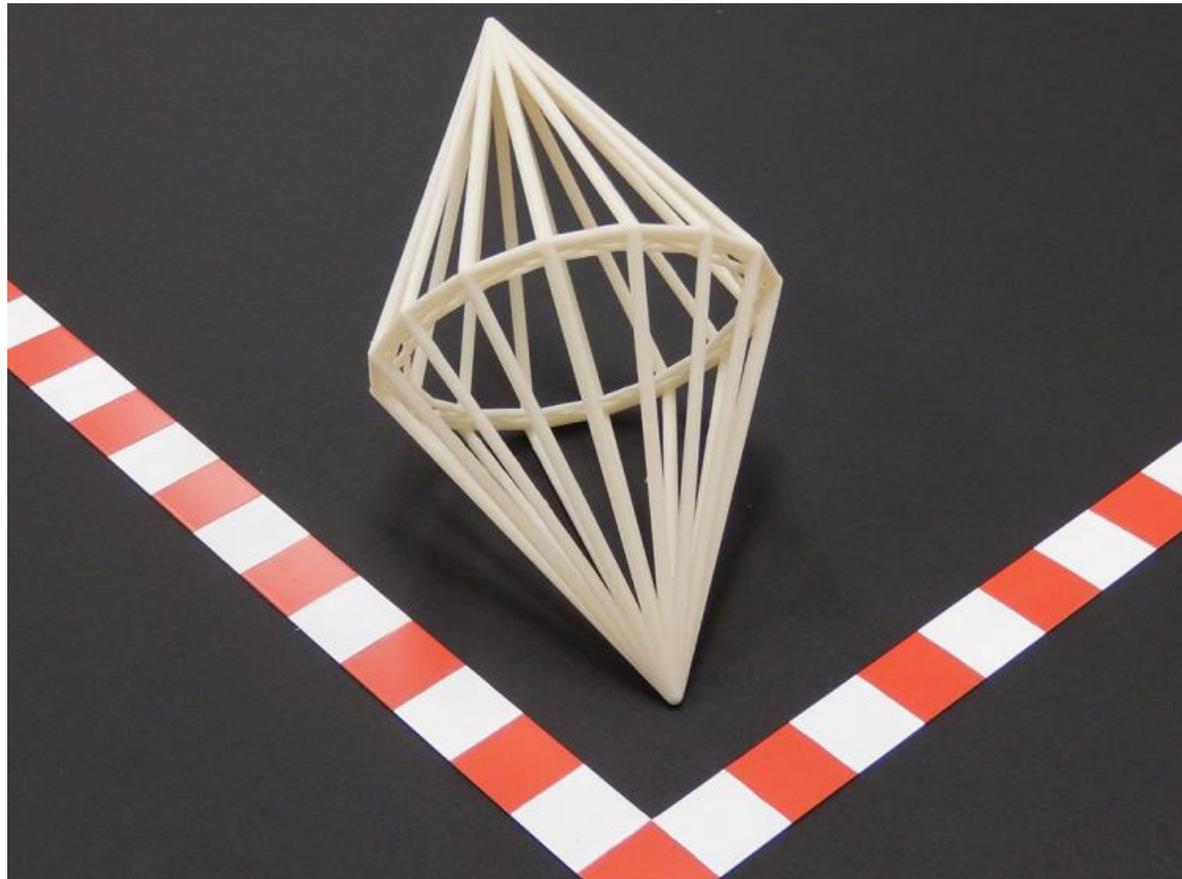


NOTE: HALF-DOMAIN



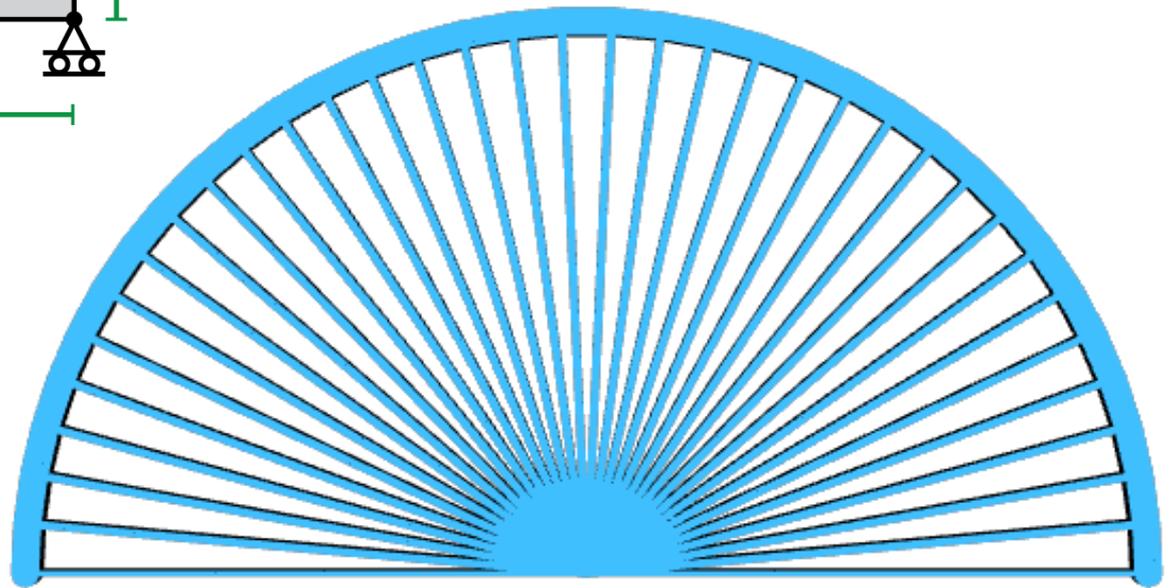
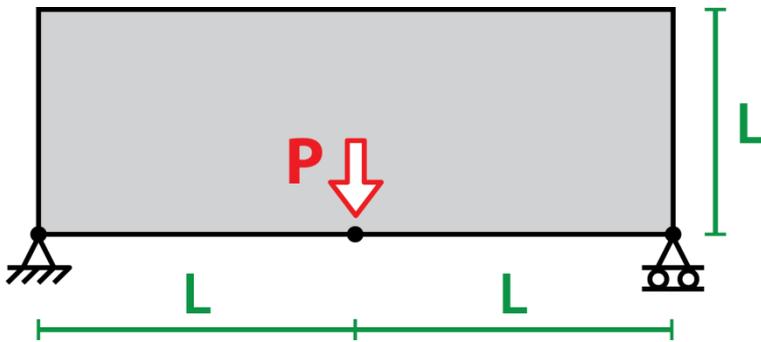
6) ADDITIVE MANUF. OF OPT. STRUCTS.

- SHOW AND TELL: DIAMOND



6) ADDITIVE MANUF. OF OPT. STRUCTS.

- SHOW AND TELL: PINWHEEL



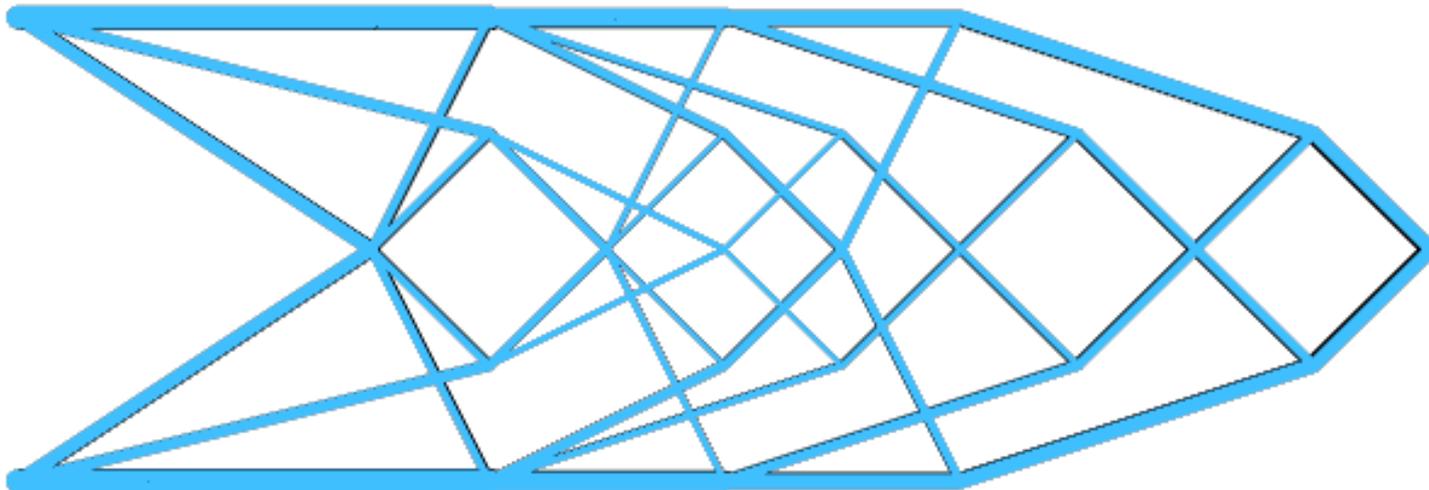
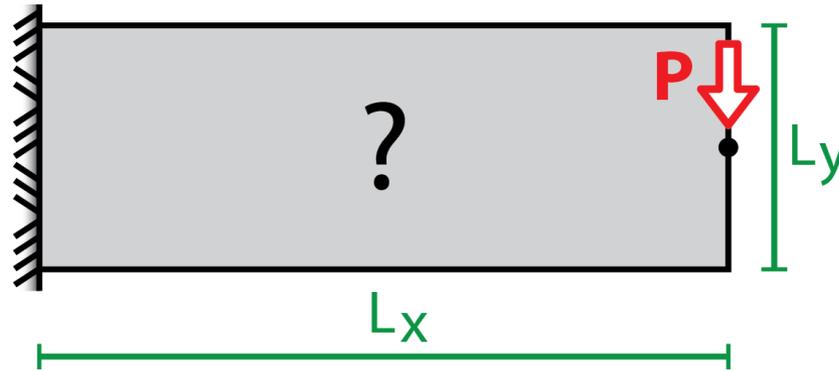
6) ADDITIVE MANUF. OF OPT. STRUCTS.

- SHOW AND TELL: PINWHEEL



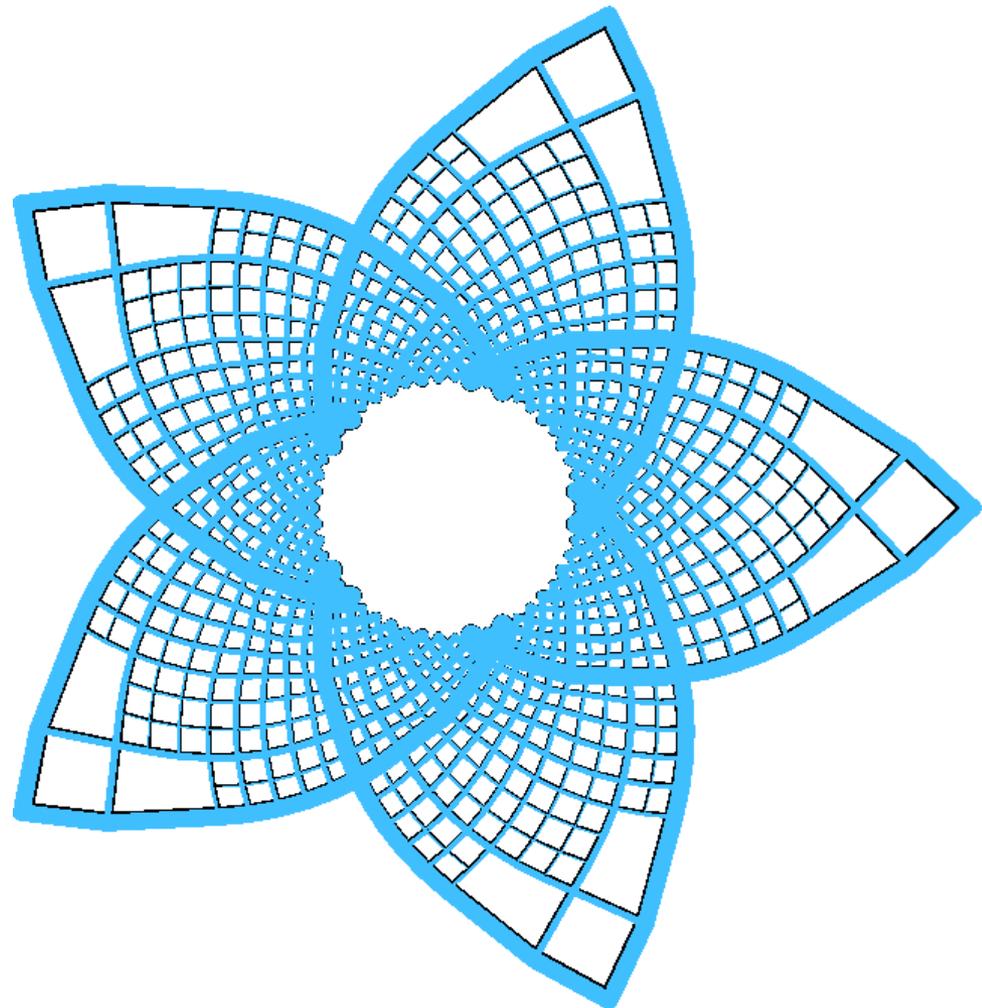
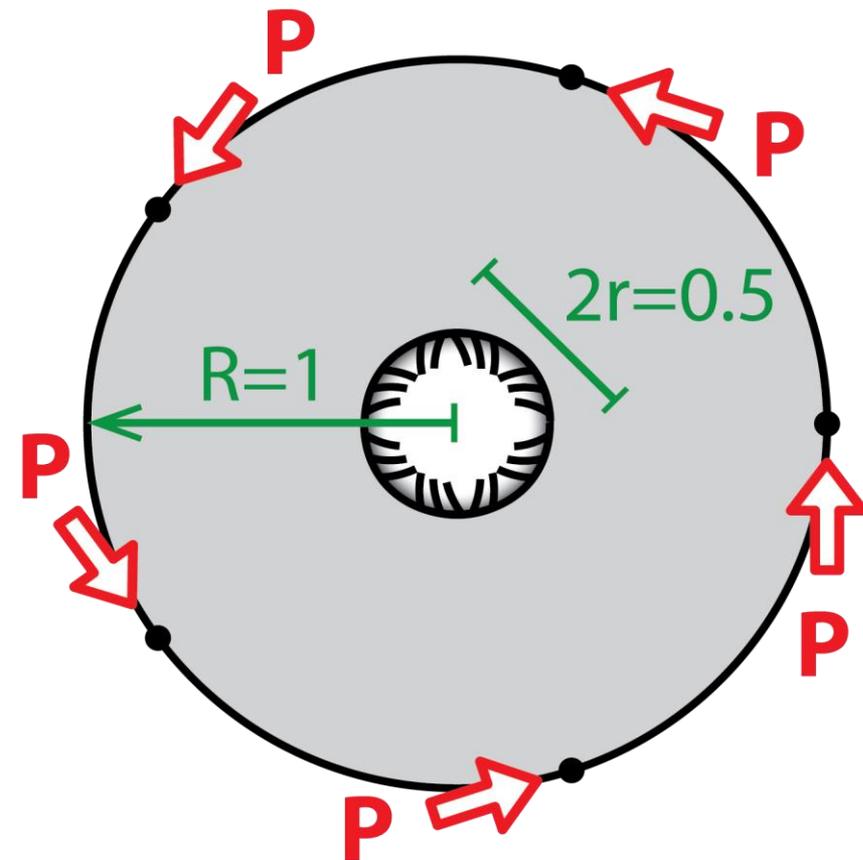
6) ADDITIVE MANUF. OF OPT. STRUCTS.

- SHOW AND TELL: CANTILEVER



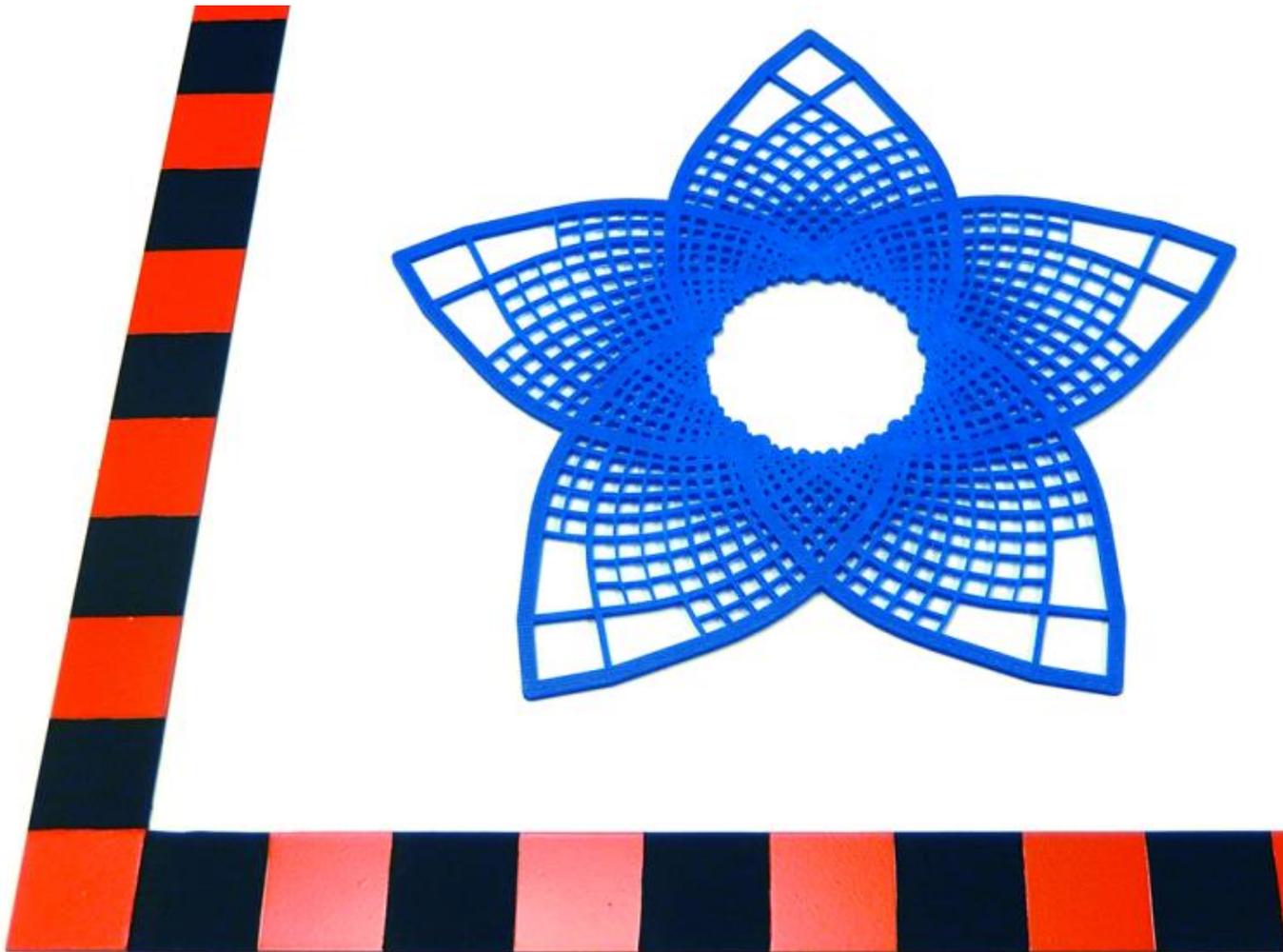
6) ADDITIVE MANUF. OF OPT. STRUCTS.

- SHOW AND TELL: FLOWER



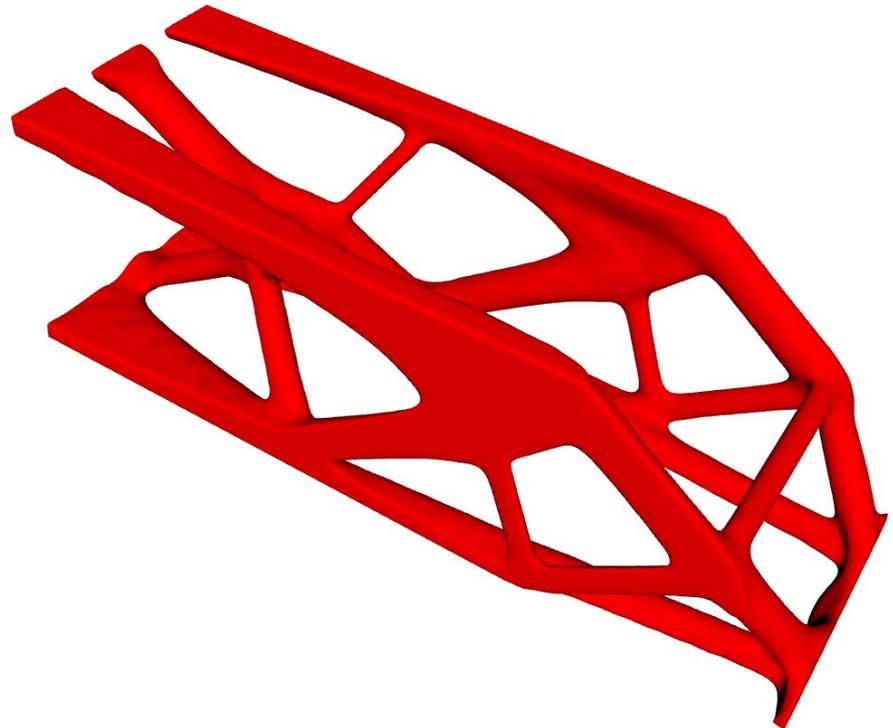
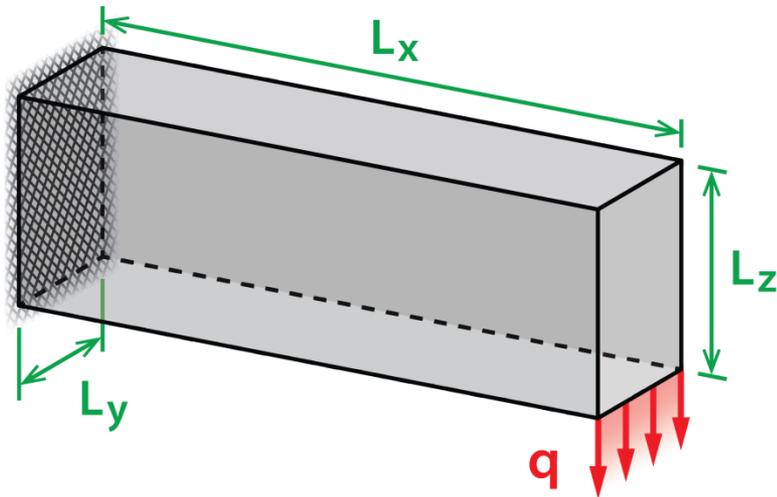
6) ADDITIVE MANUF. OF OPT. STRUCTS.

- SHOW AND TELL: FLOWER



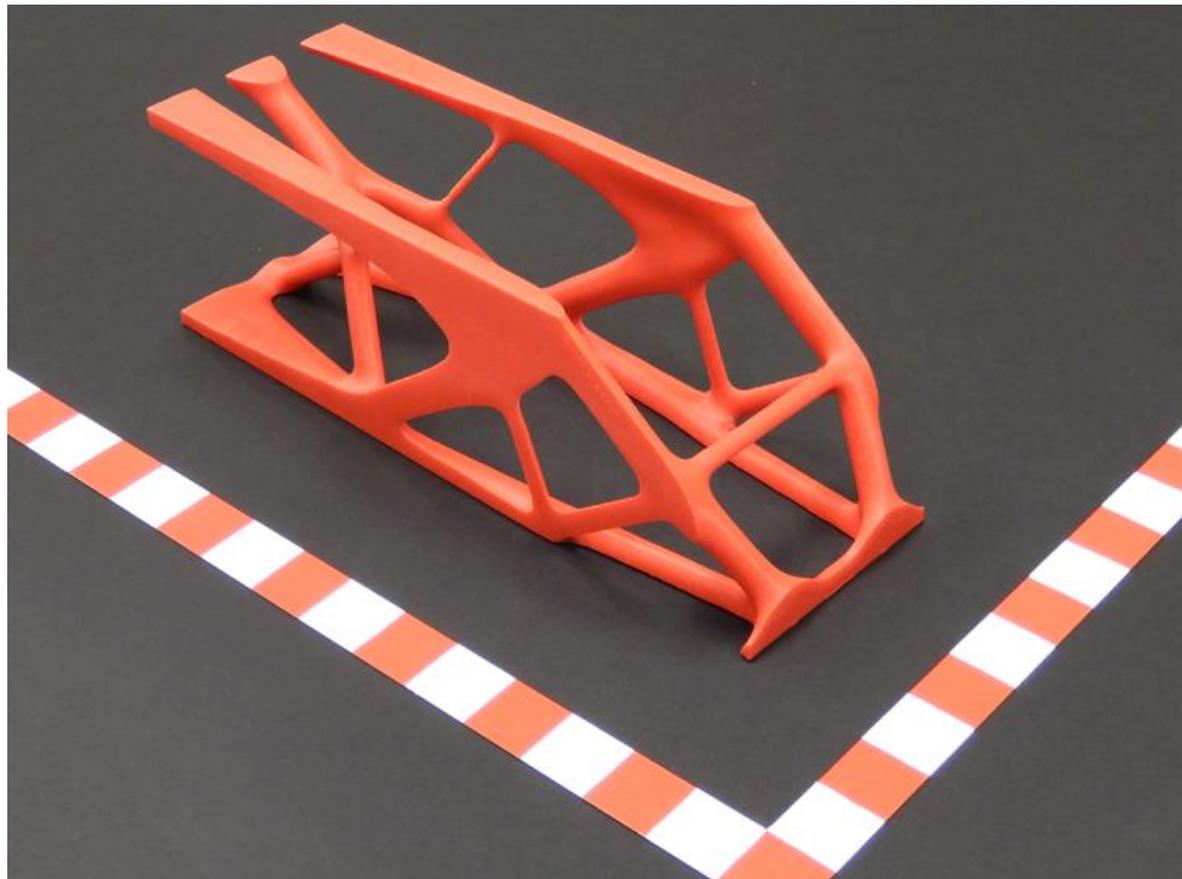
6) ADDITIVE MANUF. OF OPT. STRUCTS.

- SHOW AND TELL:
EDGE-LOADED 3D CANTILEVER (NO FIX)



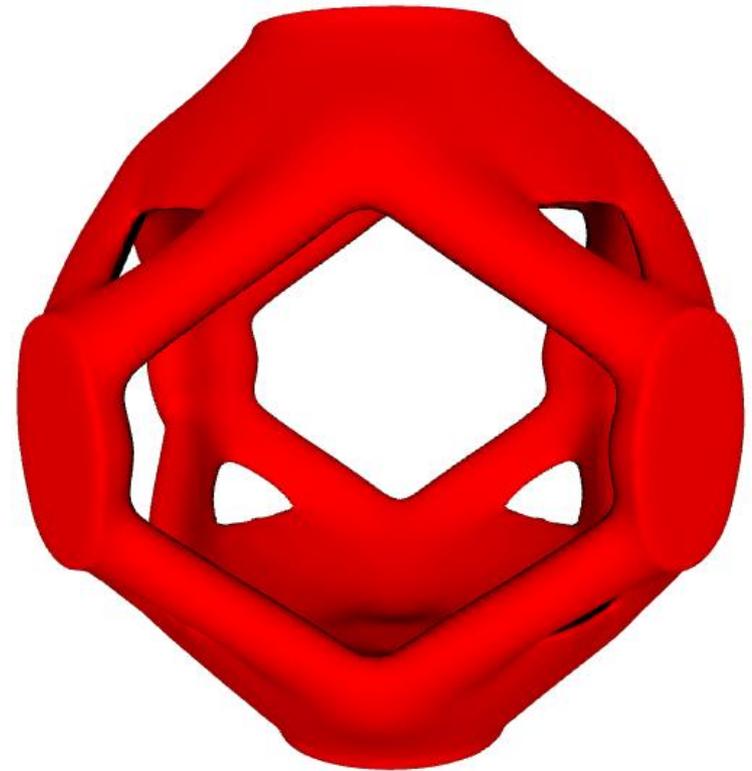
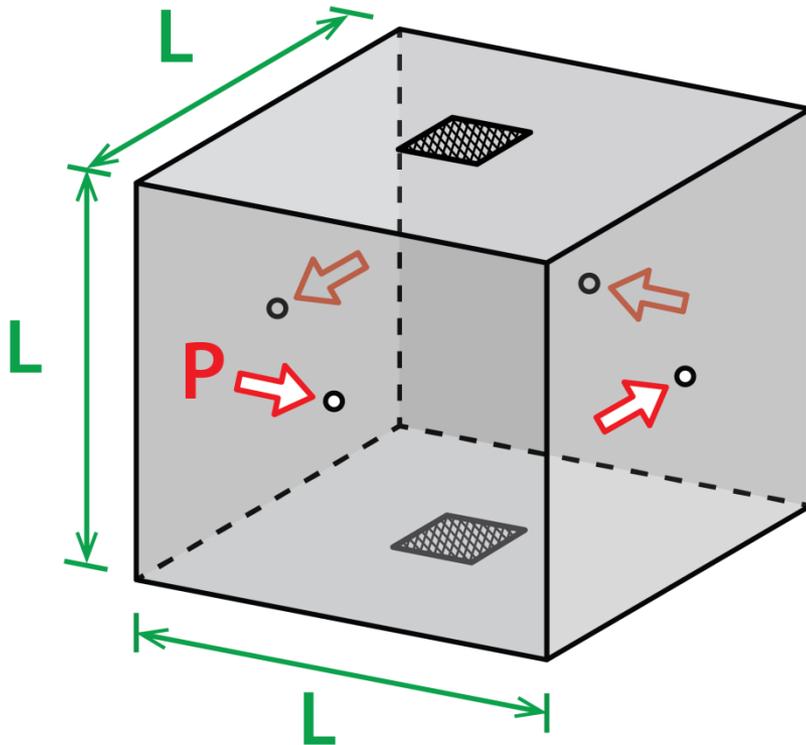
6) ADDITIVE MANUF. OF OPT. STRUCTS.

- SHOW AND TELL:
EDGE-LOADED 3D CANTILEVER (NO FIX)



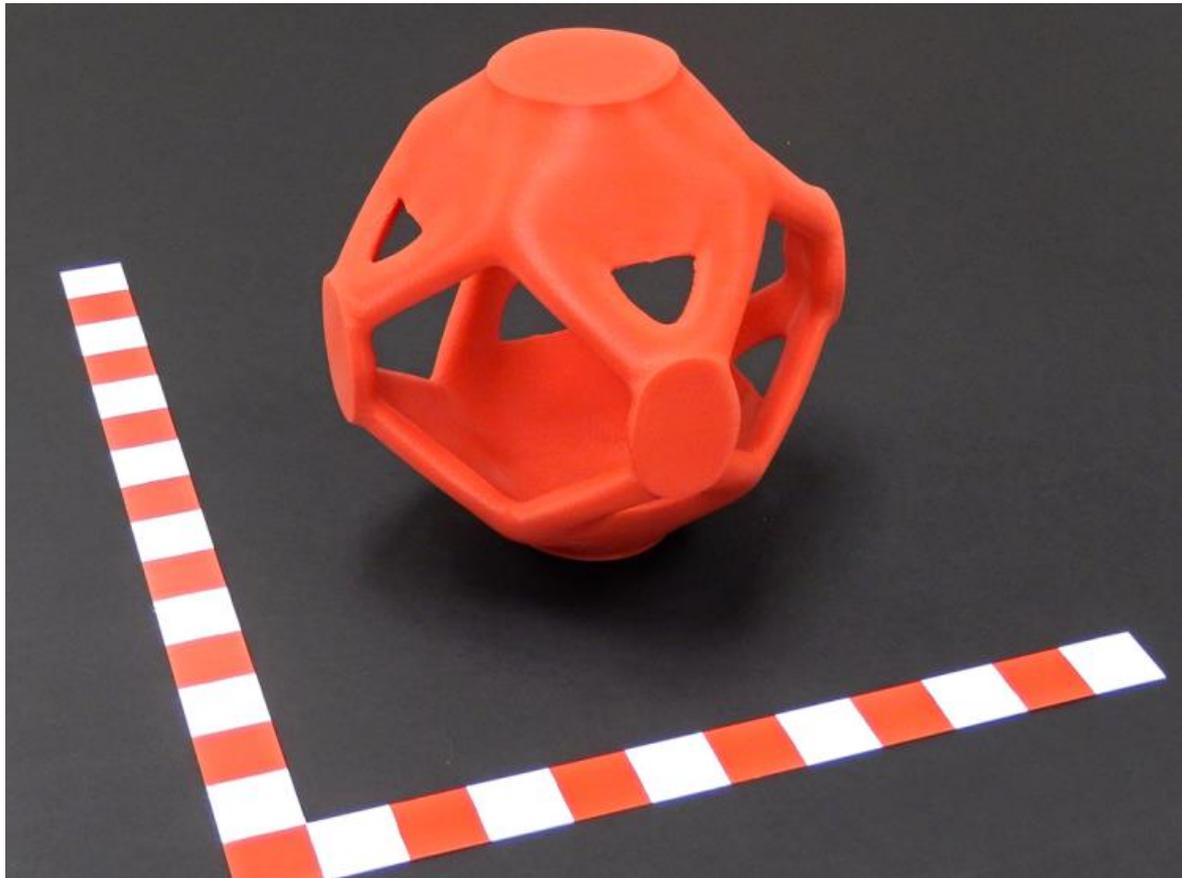
6) ADDITIVE MANUF. OF OPT. STRUCTS.

- SHOW AND TELL: SHEAR BOX



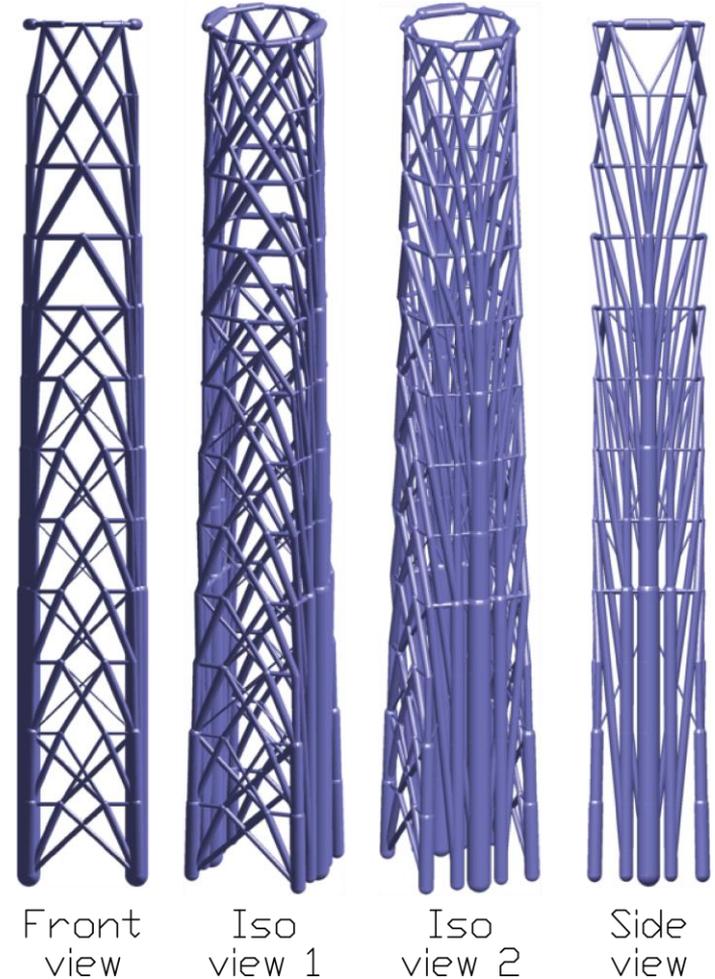
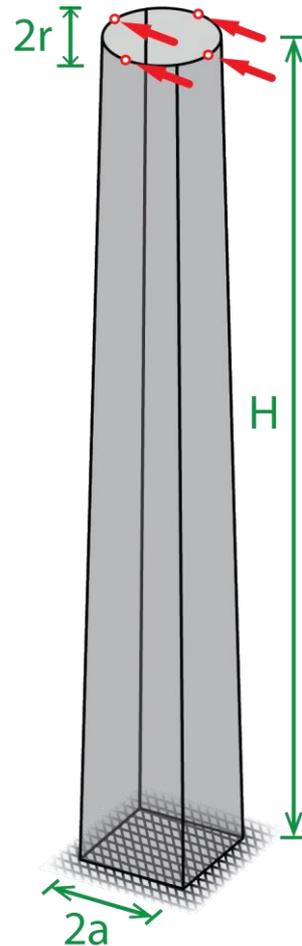
6) ADDITIVE MANUF. OF OPT. STRUCTS.

- SHOW AND TELL: SHEAR BOX



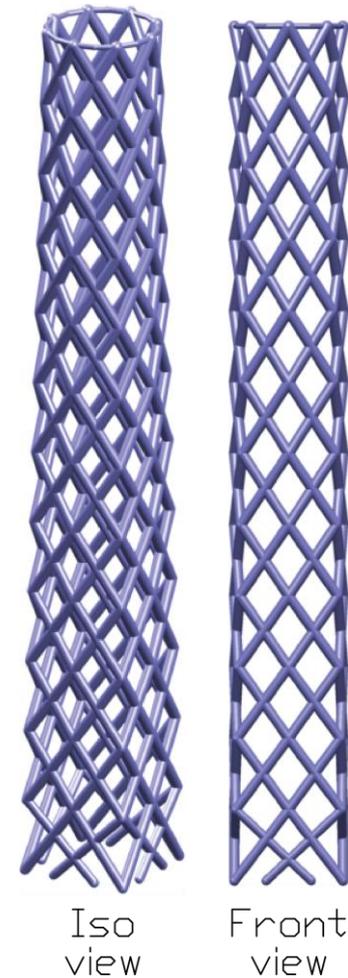
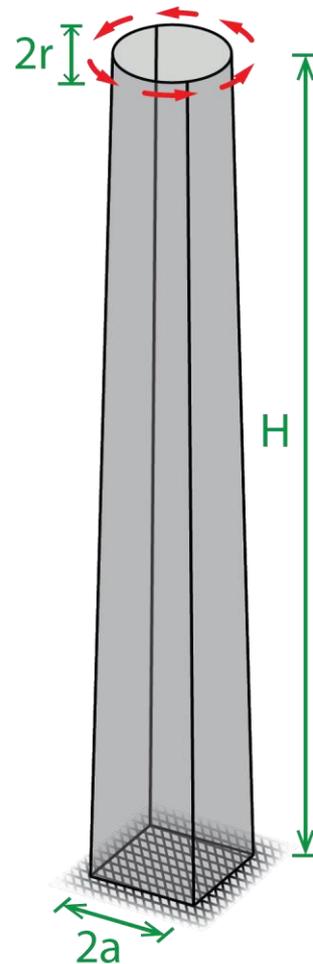
6) ADDITIVE MANUF. OF OPT. STRUCTS.

- APPLICATION-ORIENTED: **LOTTE TOWER**



6) ADDITIVE MANUF. OF OPT. STRUCTS.

- APPLICATION-ORIENTED: **LOTTE TOWER**



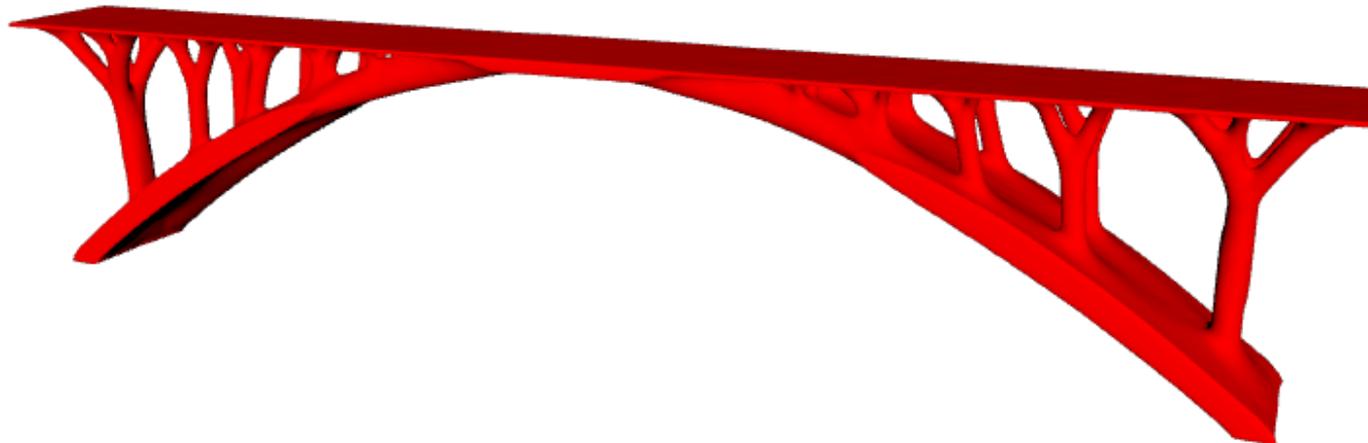
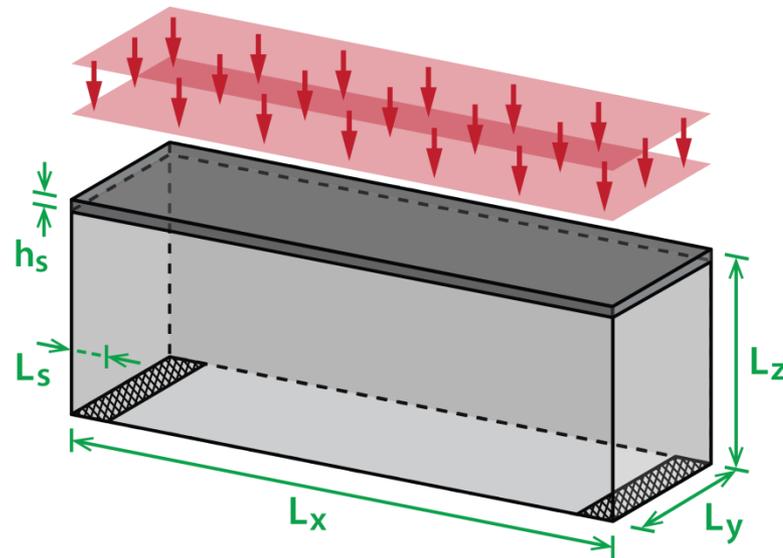
6) ADDITIVE MANUF. OF OPT. STRUCTS.

- APPLICATION-ORIENTED: **LOTTE TOWER**



6) ADDITIVE MANUF. OF OPT. STRUCTS.

- APPLICATION-ORIENTED: BRIDGE



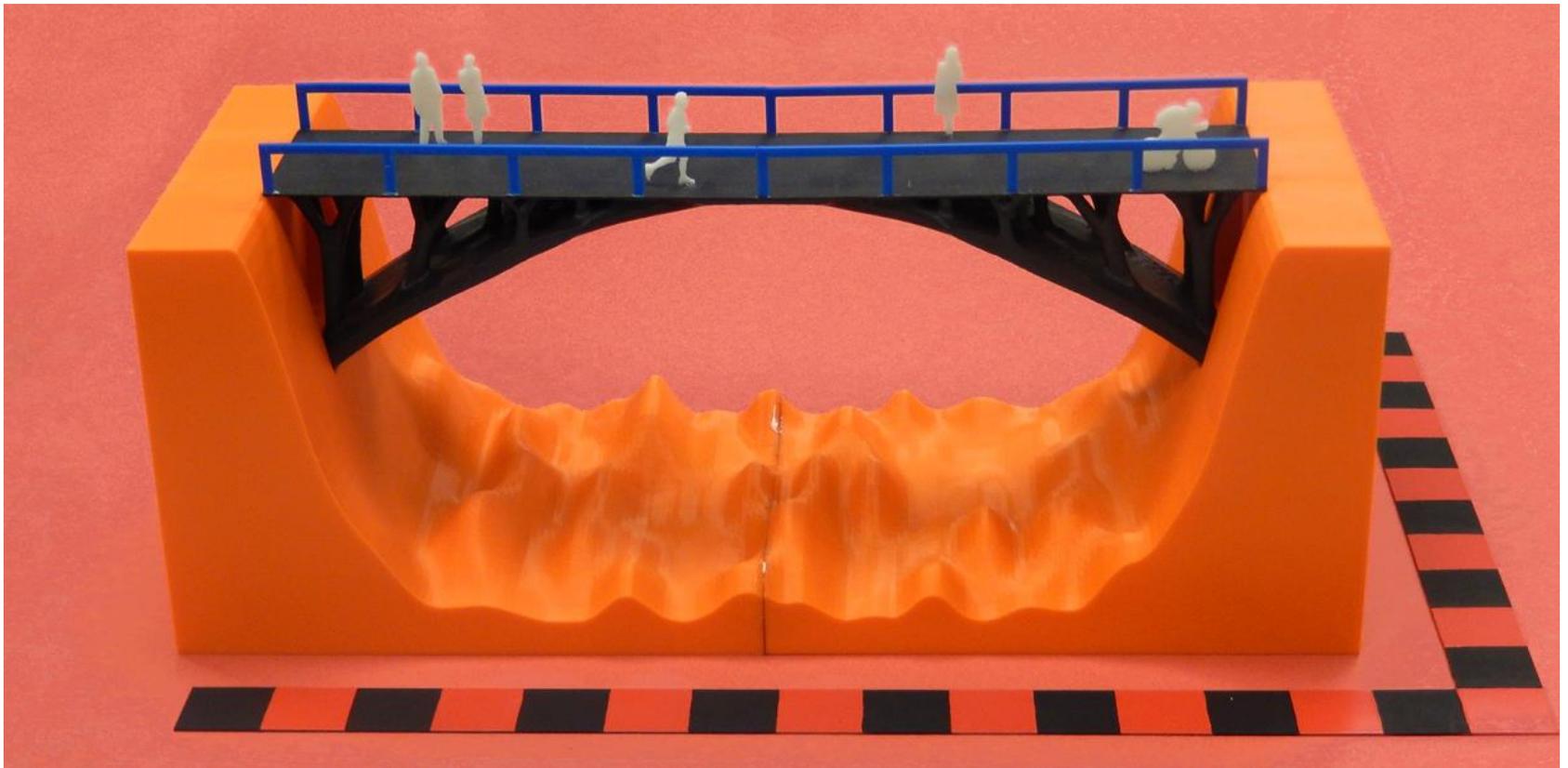
6) ADDITIVE MANUF. OF OPT. STRUCTS.

- APPLICATION-ORIENTED: BRIDGE



6) ADDITIVE MANUF. OF OPT. STRUCTS.

- APPLICATION-ORIENTED: BRIDGE



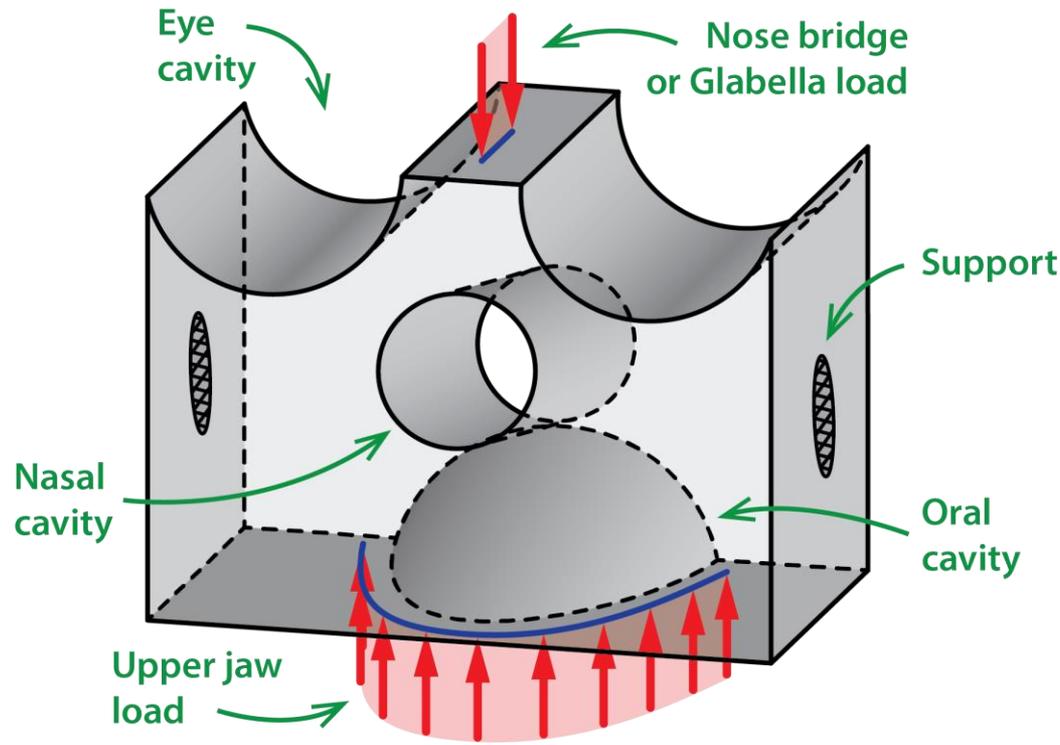
6) ADDITIVE MANUF. OF OPT. STRUCTS.

- APPLICATION-ORIENTED: **BRIDGE**
ACHIEVING LARGE SCALES



6) ADDITIVE MANUF. OF OPT. STRUCTS.

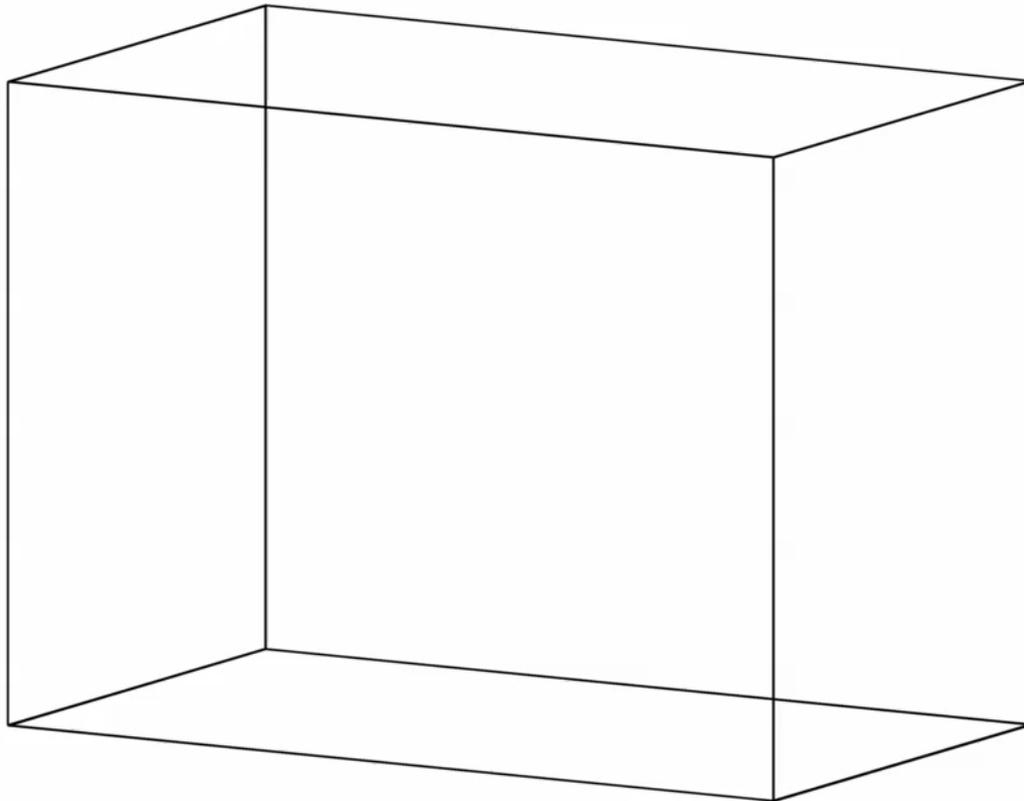
- APPLICATION-ORIENTED:
CRANIOFACIAL RECONSTRUCTION



6) ADDITIVE MANUF. OF OPT. STRUCTS.

- APPLICATION-ORIENTED:
CRANIOFACIAL RECONSTRUCTION

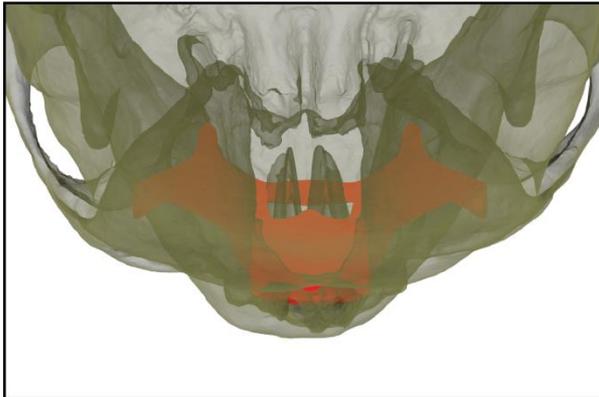
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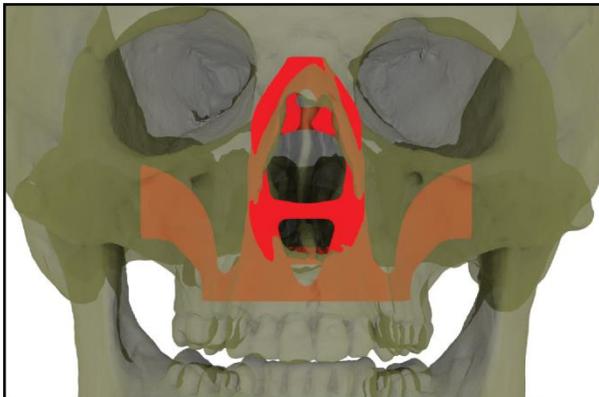
6) ADDITIVE MANUF. OF OPT. STRUCTS.

- APPLICATION-ORIENTED:
CRANIOFACIAL RECONSTRUCTION

Top view



Iso view



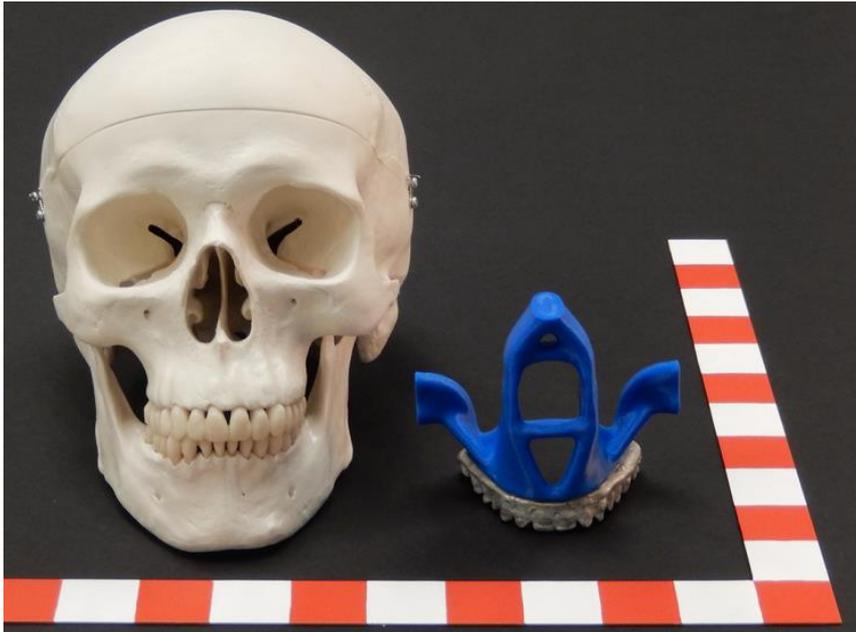
Front view



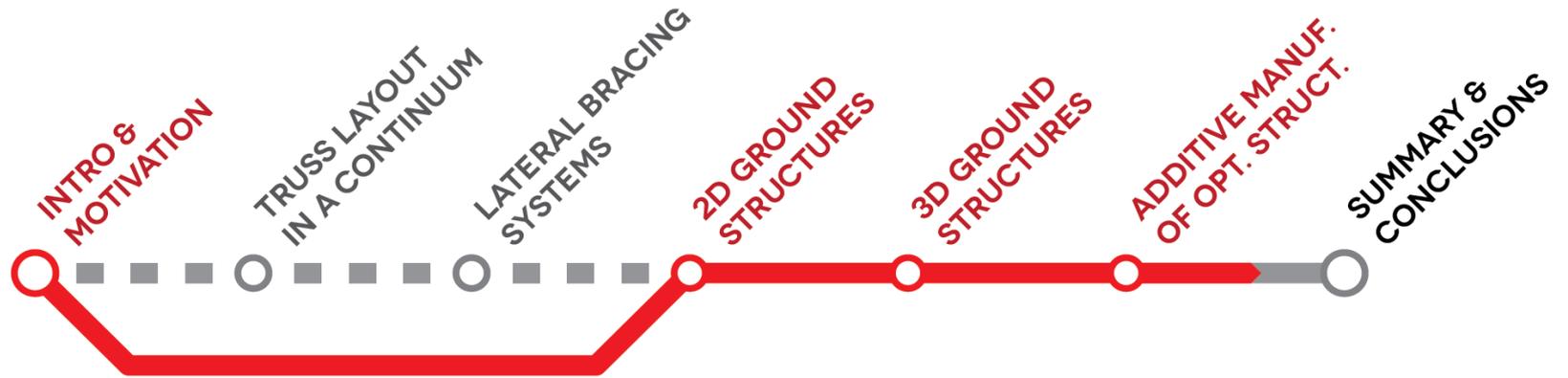
Side view

6) ADDITIVE MANUF. OF OPT. STRUCTS.

- APPLICATION-ORIENTED:
CRANIOFACIAL RECONSTRUCTION



ROADMAP



7) SUMMARY AND CONCLUSIONS

- OPTIMIZATION:
 1. ESSENTIAL FOR SUSTAINABILITY
 2. CAN BE INCORPORATED INTO DESIGN TODAY
 3. GIVE A DESIGN, AND I WILL TRY TO MAKE IT BETTER
 4. DIFFERENT METHODS FOR DIFFERENT PROBLEMS
 5. YES, WE CAN MANUFACTURE THIS
 6. DESIGN GUIDED BY FUNCTIONALITY AND NOT JUST BEAUTY

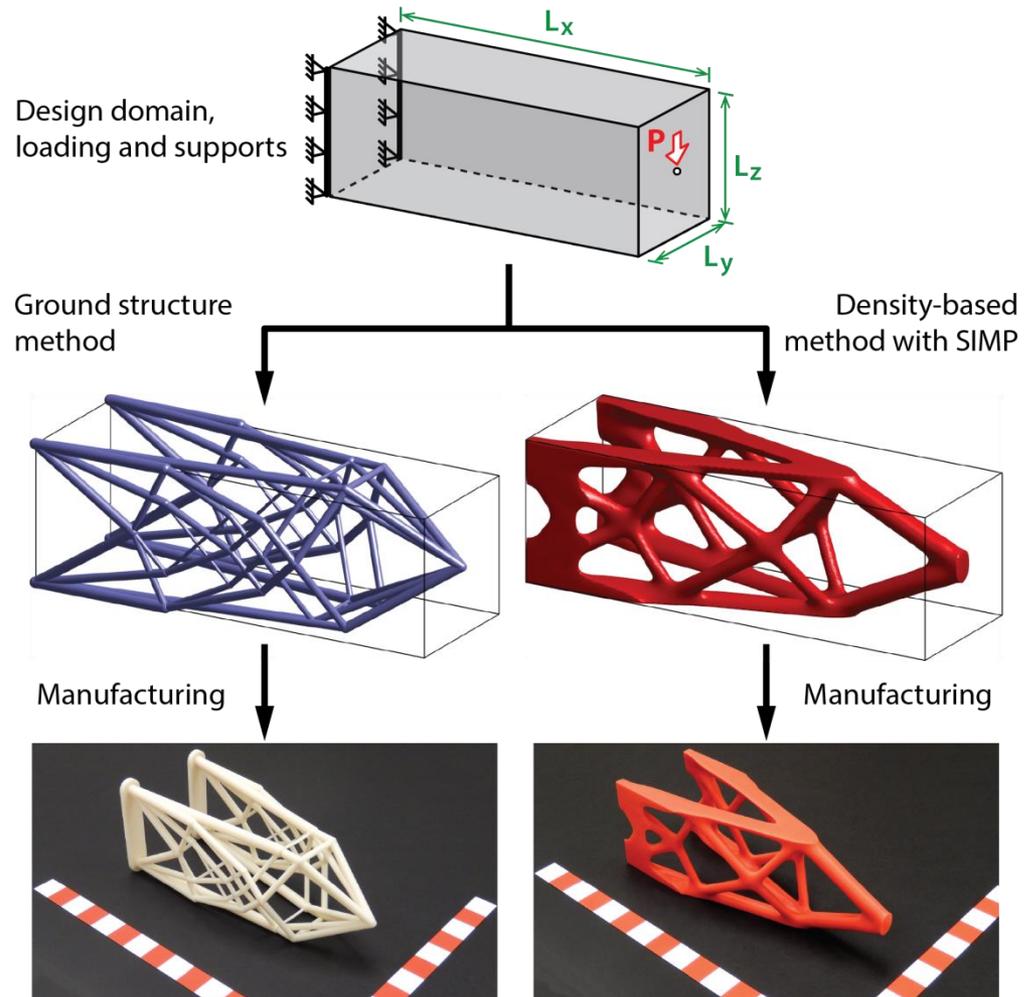
7) SUMMARY AND CONCLUSIONS



MUSEUMS AND RECONSTRUCTION (

7) SUMMARY AND CONCLUSIONS

- INTEGRATED DESIGN PROCESS:
START TO FINISH



AKNOWLEDGEMENTS

- ADEILDO SOARES RAMOS
- GLAUCIO H. PAULINO
- LCCV @ UFAL
- CEE @ ILLINOIS

THE END

